



Reservoir Pressure Response

8-July-2010

10841
Exhibit No. _____
Worldwide Court Reporters, Inc.

Outline

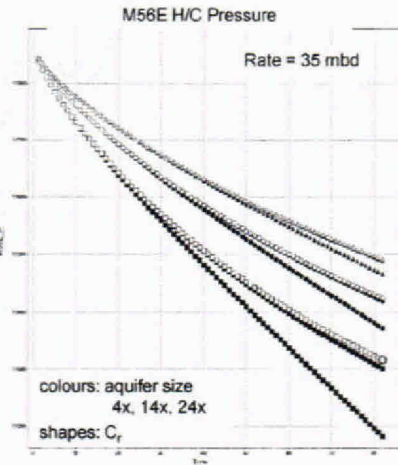


- Modelling used preliminary slab model
 - Structural model incomplete Wed. evening
 - PIE used to cross-check
- Fixed Parameters:
 - M110 Size (45 mmrb)
- Sensitivity Parameters:
 - Aquifer: **3.8x**, 13.7x, 24x (larger aquifers with some K red'n)
 - Cr: **6, 12, 18** μ sips
 - Oil Rate: 35, 50, 60 mbd
 - Skin: 0, 10, 20
 - Xflow 0, ??, ?? rb/d (approximate, controlled with skin)

Depletion



- Aquifer Impact (referenced to 4x Aquifer, 6 μ sips, @35 mbd)
 - No Aquifer: -800 psi
 - 13.7x Aquifer +120 psi
 - 24x Aquifer +130 psi
- Compressibility
 - 12 μ sips +200 psi
 - 18 μ sips +300 psi
- S.I. BHP Range (M56E, @5 hrs)
 - Near well: 7,900 - **11,030** - 11,120
 - Reservoir: 9,360 - **11,360** - 11,590
 - Recommend: new "most likely": 3.8x aquifer, 12 μ sips, 35 mbd

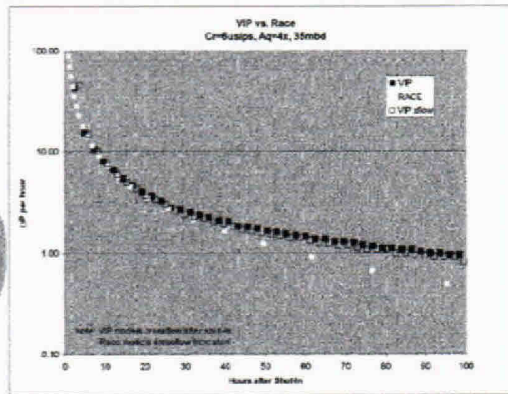


note: values reflect additional 15 days of depletion

Post Shut-In Behaviour



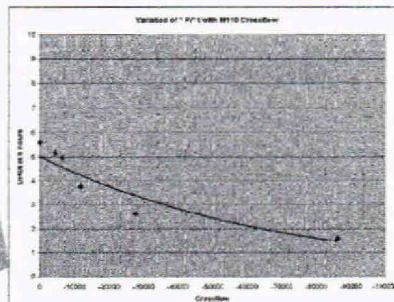
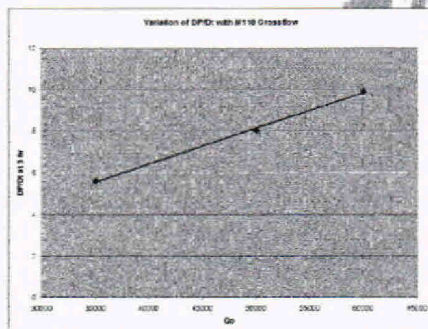
- Bottomhole pressure changes very rapidly for first 3 hours
 - $\Delta P/\Delta t > 30,000$ psi/hr
- Differences
 - Layer crossflow
 - 2 layers v. many
 - Solution method & timesteps
- Similar solutions during critical period ($5 < t < 100$ hrs)



Variation of DP/Dt with Parameters: Q_o & Xflo



$\Delta P/\Delta t$ of ~5 - 10 psi/hour for rates between 35 & 60 mbd at 5 hours of shut-in



$\Delta P/\Delta t$ of ~1-3 psi/hour for crossflow between 0 & 30 mbd at 5 hours of shut-in

$\Delta P/\Delta t$ at 5 hours



- Insensitive to:
 - Aquifer (1 psi/hr)
 - Compressibility (1 psi/hr)

- Largest sensitivities:
 - Crossflow
 - Average production rate
 - Sensitivity to $Q_o > X_{fio}$

DRAFT



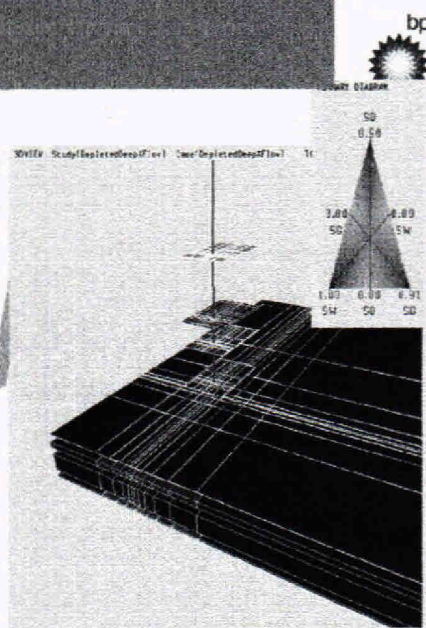
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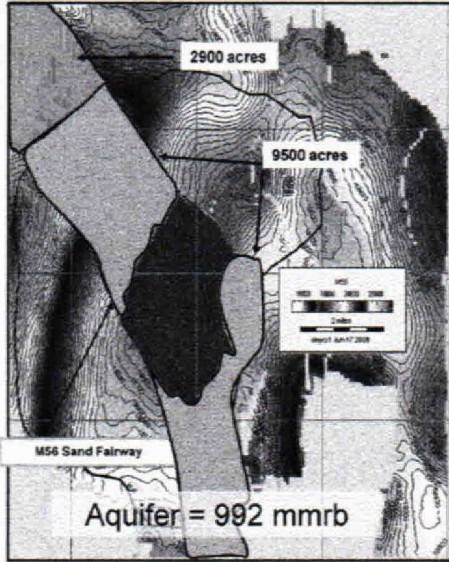
TREX 010841.0007

Input Data

- Data provided by GoMx Reservoir Team
- Rock Properties
 - Developed from MC252 logs
 - Permeability
 - 275 mD in main M56E sand
 - 397 mD in M56A gas/oil sand (only 2.5')
 - 86 – 110 mD in other oil sands
 - Compressibility:
 - Cr: 6×10^{-6} psia⁻¹
 - Cw: 3×10^{-6} psia⁻¹
 - Cf: $\sim 13 \times 10^{-6}$ psia⁻¹
 - Fluid properties generated by EoS; volatile, near critical fluid
- tubing performance matched to GAP / Prosper work of T. Liao, A. Chitale & M Gokdemir



Macondo RF –
Aquifer Size



Oil Accumulation
110 mmstb = 258 mmb

9500 acre Aquifer		
Net Sand Thickness, ft.	Porosity, %	Aquifer Size
44	13	1.5x
44	17	2.0x
66	17	2.9x

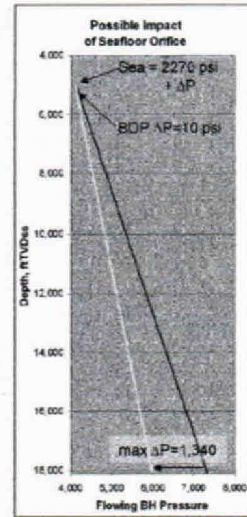
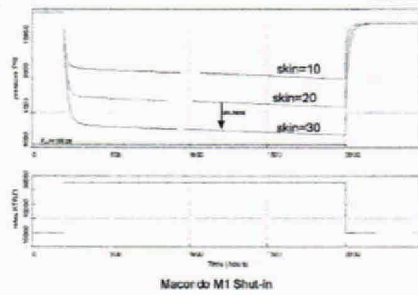
12400 acre Aquifer		
Net Sand Thickness, ft.	Porosity, %	Aquifer Size
44	13	1.9x
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Largest Aquifer Size – used as base case
(will minimise depletion)

Depletion Response @wellbore



- PIE gives similar results to VIP
 - Constant compressibility (too low)
 - Single phase
- P_{wf} drops ~8 psi/day (for 35mbd case)
- Lack of observed depletion could be due to fixed seafloor pressure and large orifice

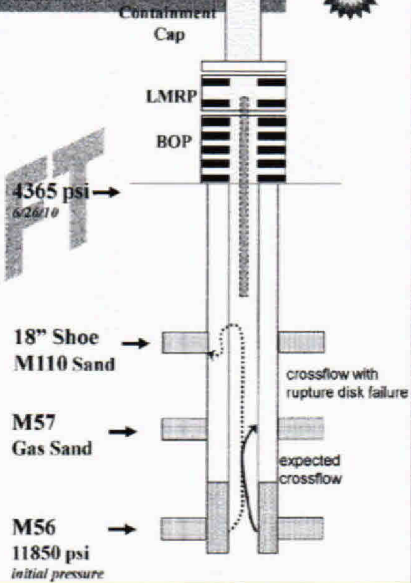


Conclusions

- Actual reservoir depletion dependent on:
 - Flowrate
 - Oil column size
 - Aquifer
- Limited depletion observed in wellhead could be controlled by non-reservoir mechanisms
 - Large orifice
 - Flowpath / choke between BOP & reservoir
 - Broken gauge
 - Crossflow
- Largest uncertainties: flowrate and pressure drop

2270 psi
initial

bp

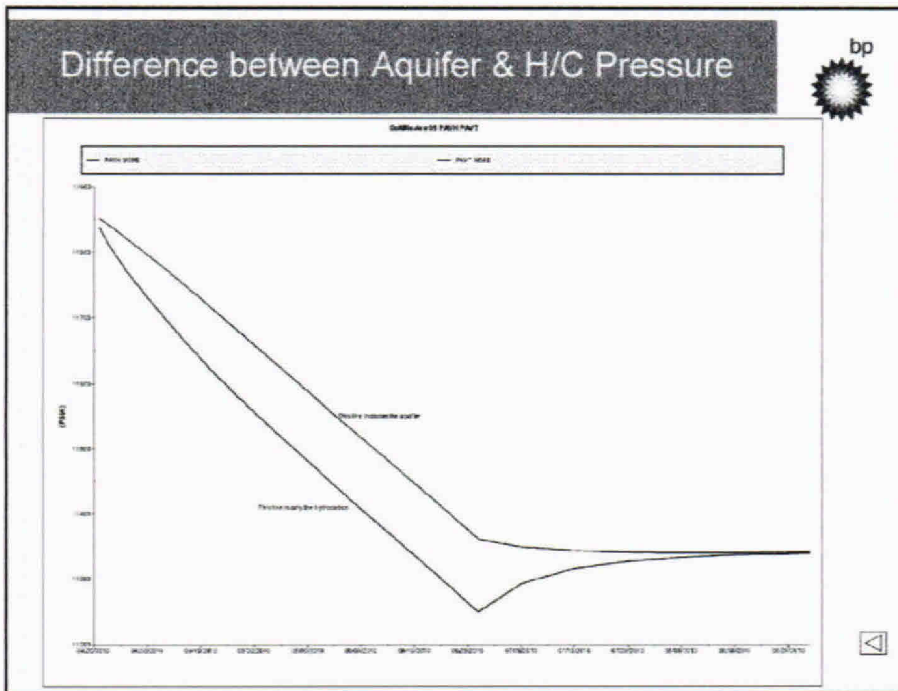


Back-Up



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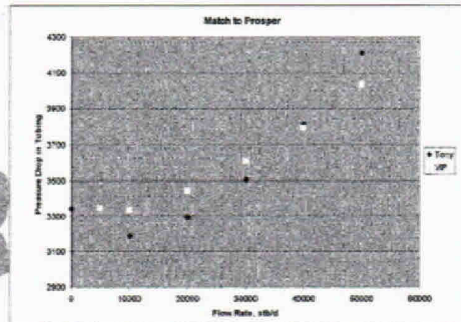
Difference between Aquifer & H/C Pressure



Match to "Tubing Performance"



- Flowpath is a major (principle?) source of THP uncertainty
- Various cases considered:
 - Annular flow
 - Casing flow
 - Annular + casing flow
- VIP wellbore modelling capability limited in comparison with Prosper / Gap
 - Matched lift with simple tubing string
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Influences on Observable Shut-In Pressure



At Shut-In

High Wellhead Pressure

- Limited crossflow
- Well integrity above 18" shoe
 - small leak into small zone
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Low Wellhead Pressure

- Integrity failure (crossflow into M110)
- Smaller aquifer
- Higher production (& lower skin)

After Shut-In

Rising THP

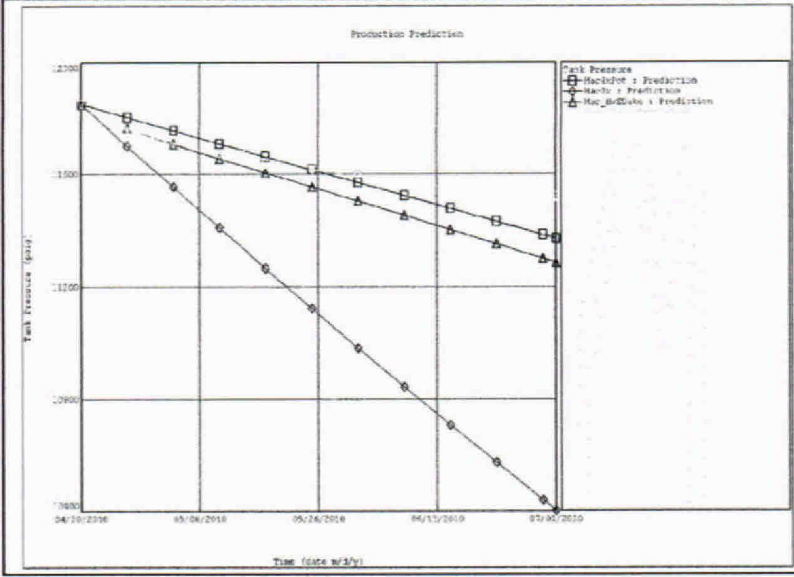
- Fluid Segregation
 - Only if $P_{thp} < 6,650$ psia
 - Increase would begin at low rates or at flow cessation
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 - Aquifer size will influence P_{final}
- Cessation of crossflow (pressure equilibration)

Falling THP

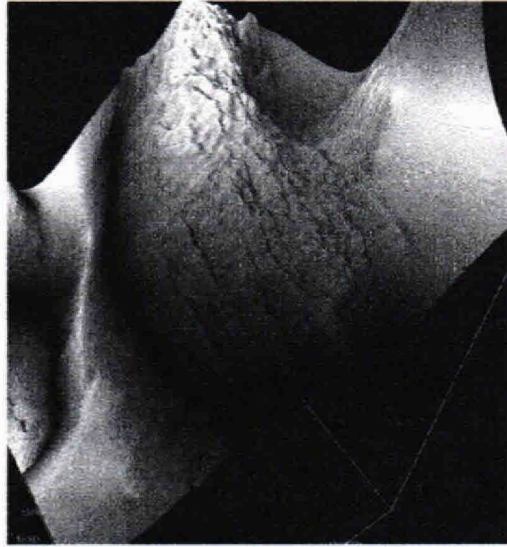
- Wellbore temperature equilibration (cooling)
- Large leak with limited inflow



MBal Results for Various Aquifers



Future Work: Add Structure



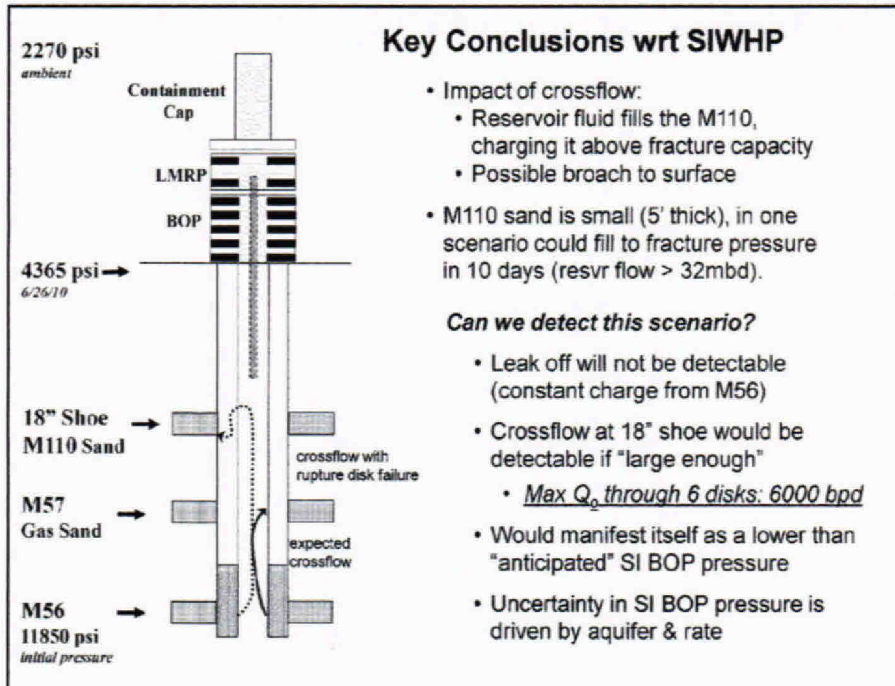
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TREX 010841.0017



Key Conclusions wrt SIWHP

- Impact of crossflow:
 - Reservoir fluid fills the M110, charging it above fracture capacity
 - Possible broach to surface
- M110 sand is small (5' thick), in one scenario could fill to fracture pressure in 10 days (resvr flow > 32mbd).

Can we detect this scenario?

- Leak off will not be detectable (constant charge from M56)
- Crossflow at 18" shoe would be detectable if "large enough"
 - Max Q_o through 6 disks: 6000 bpd
- Would manifest itself as a lower than "anticipated" SI BOP pressure
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Model Approach & Purpose



- Model constructed to address impact of crossflow of M57B & M56A gas sands during "top kill"
 - Response of observed pressures
 - GOR variation with time
- Requested to investigate whether depletion was consistent with known pressures below BOP
- Requested to avoid making any conclusions regarding likely rates
 - Role of flowrate investigation team

- Approach
 - Simple: tight timing, multiple unknowns
 - Single layer per reservoir (M57B to M56F, with intervening shales)
 - 10 x 12 x 17; no structure



Reservoir Pressure Response

8-July-2010

Outline

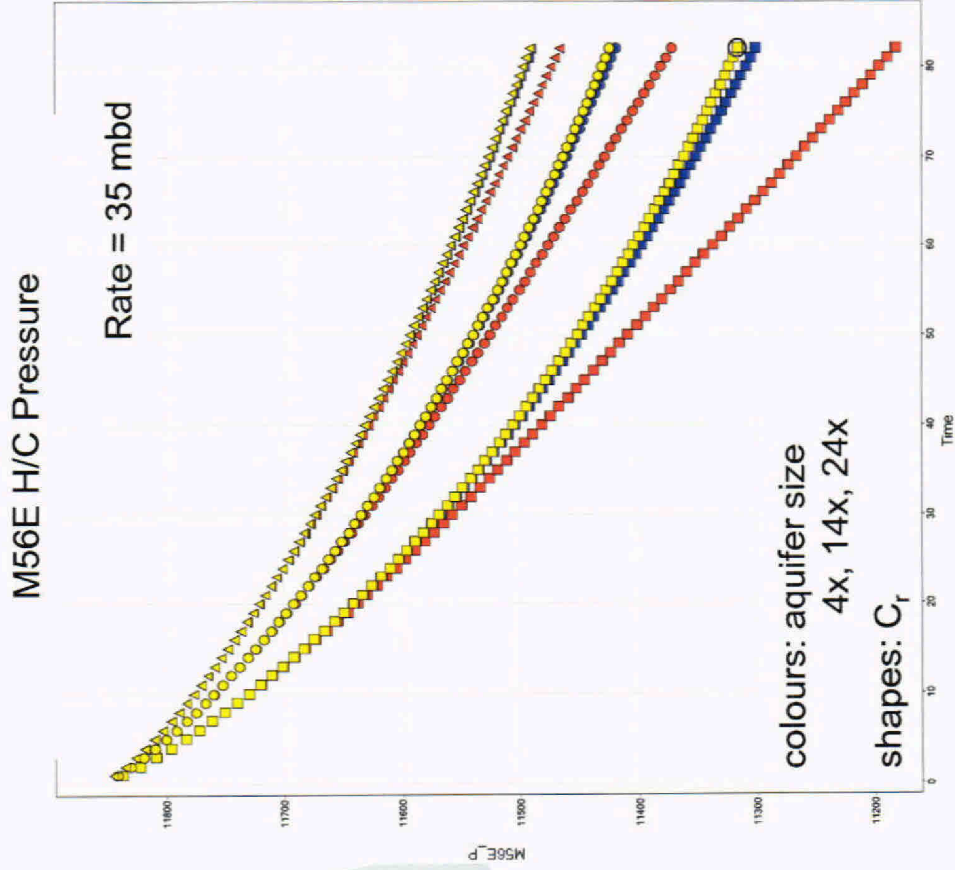


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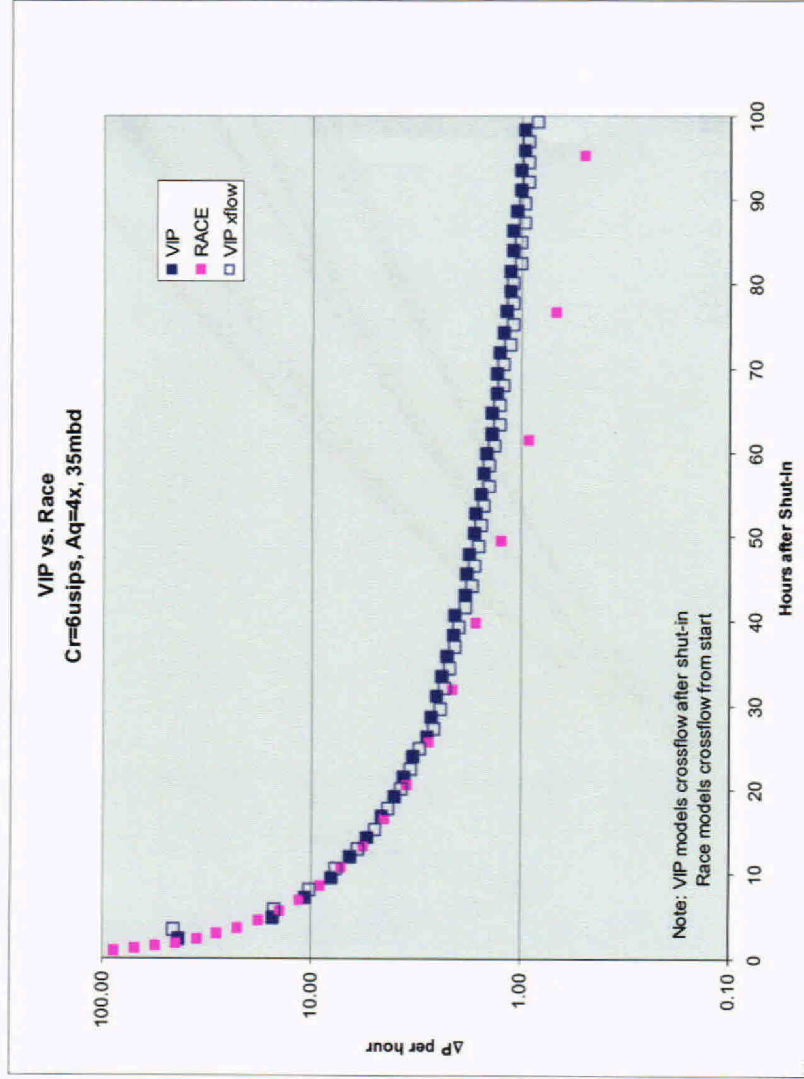
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Post Shut-In Behaviour



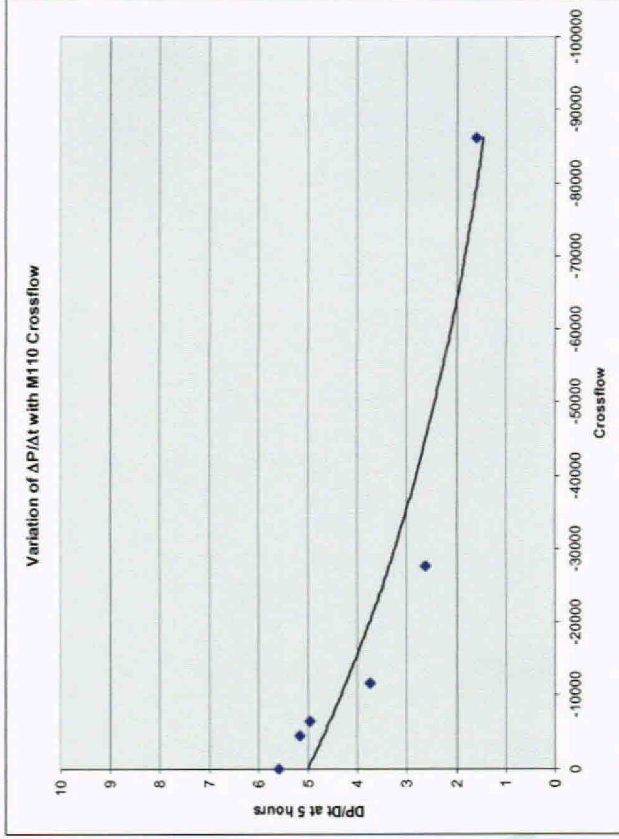
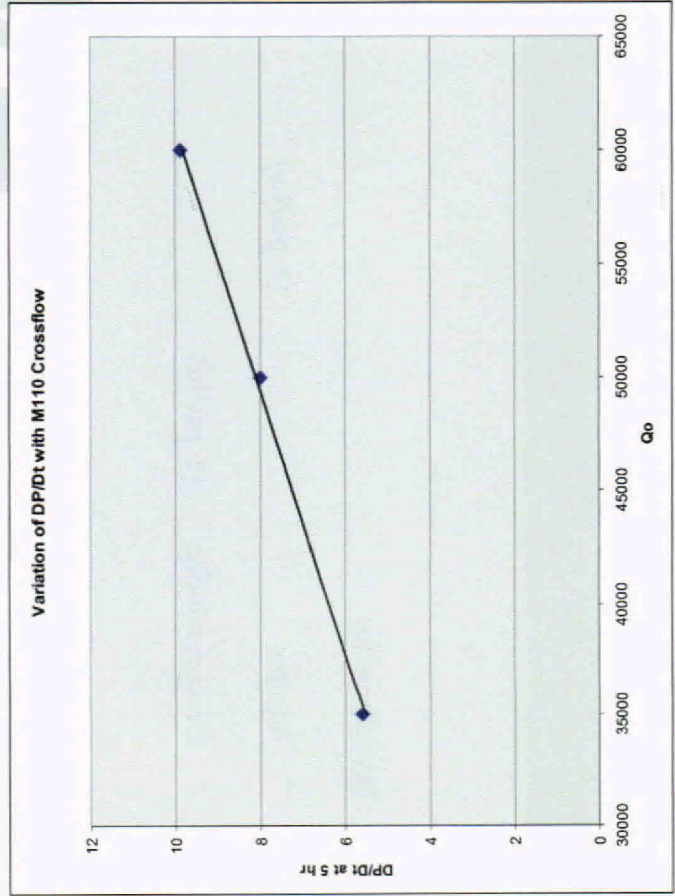
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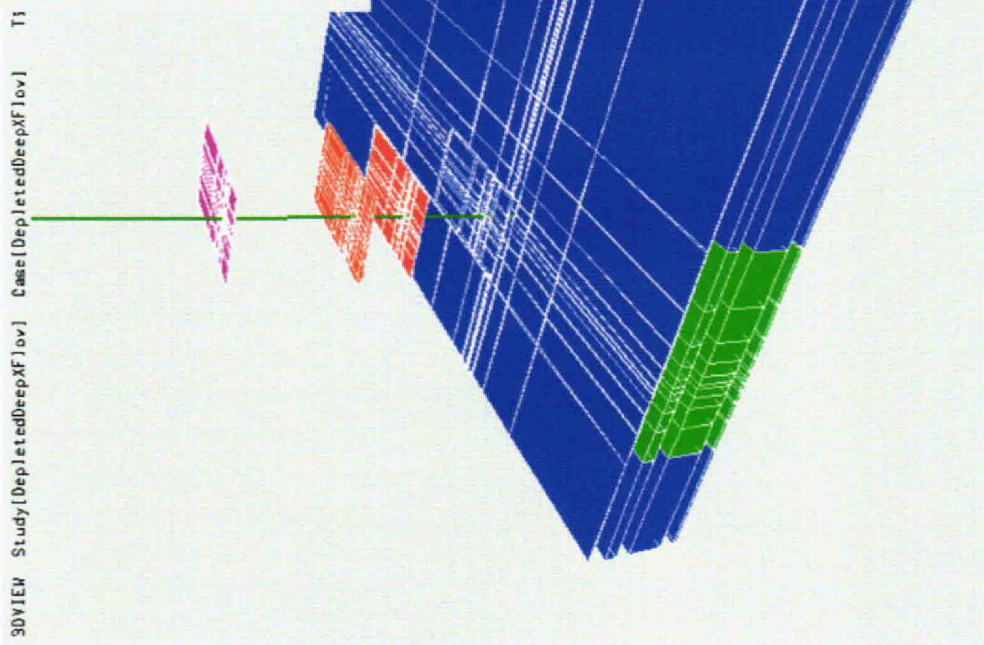
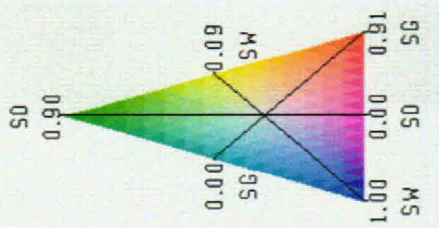
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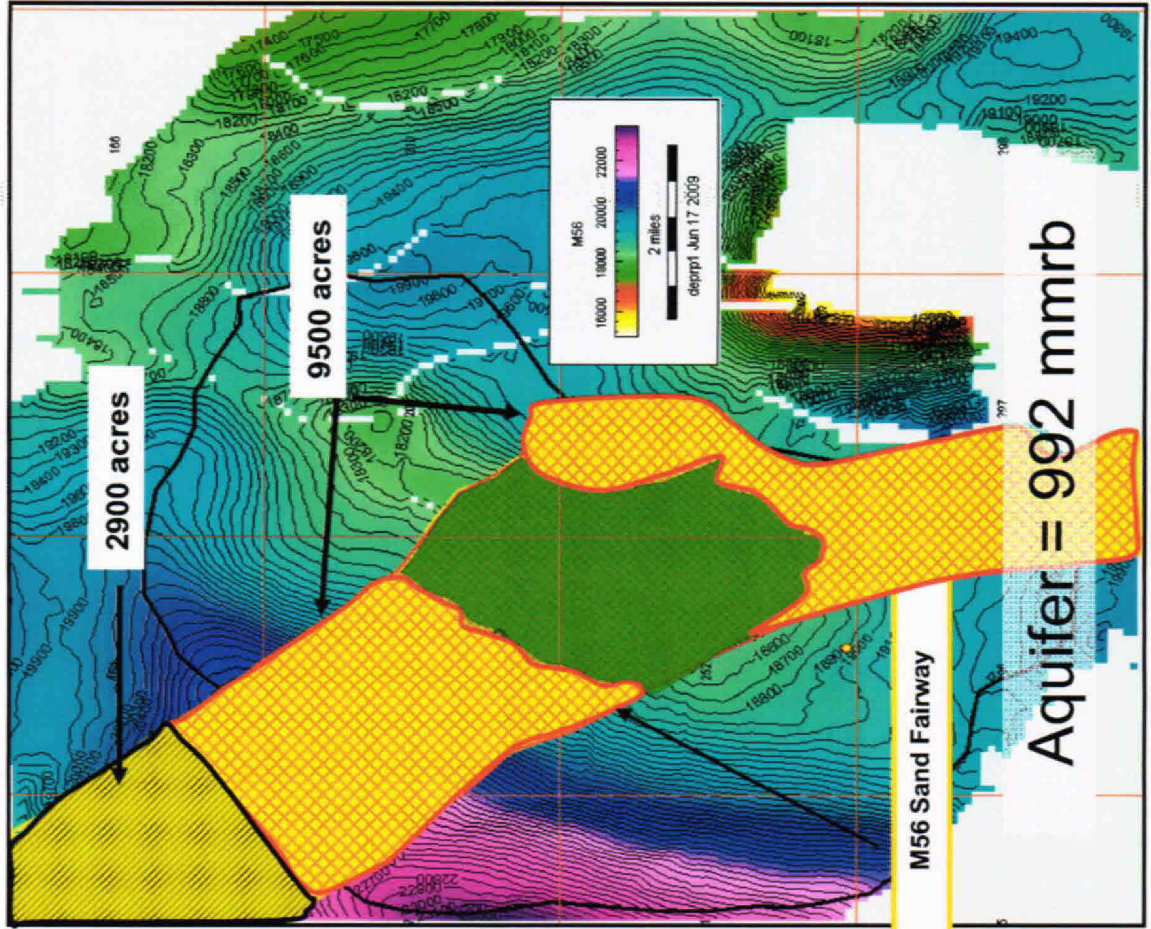


PRIMARY DIAGRAM



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Macondo RF –
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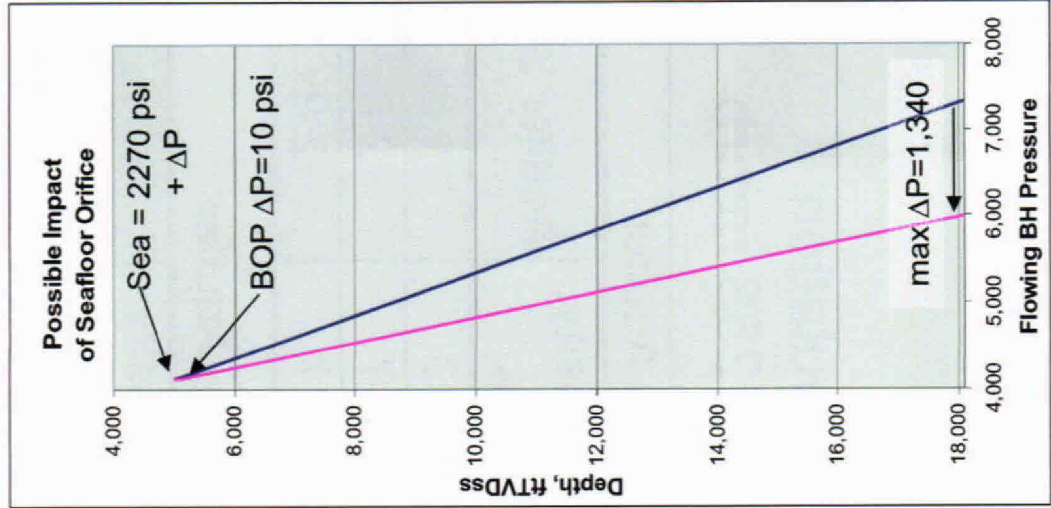
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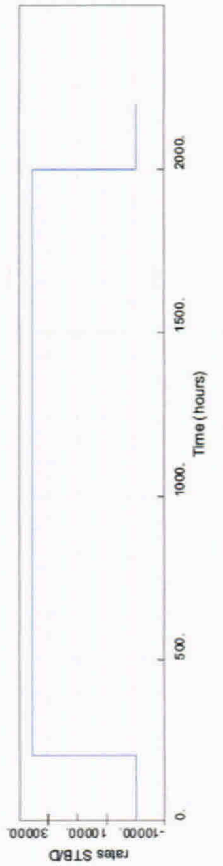
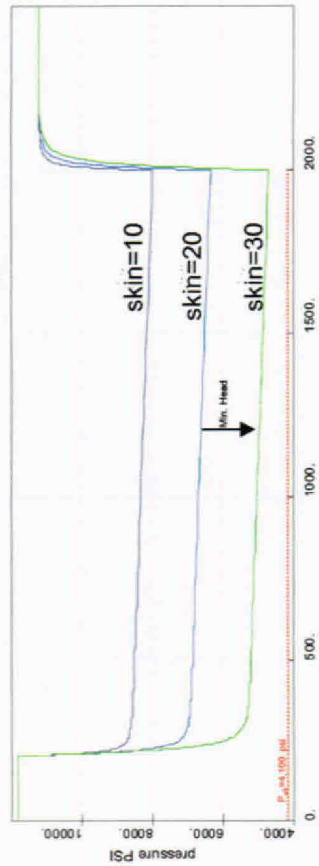
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2010/07/12-1800 : OIL



Macondo M1 Shut-In



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2270 psi
ambient

Containment

Cap

LMRP

BOP

4365 psi →
6/26/10

18" Shoe →
M110 Sand

M57 →
Gas Sand

M56 →
11850 psi
initial pressure

crossflow with
rupture disk failure

expected
crossflow

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bp



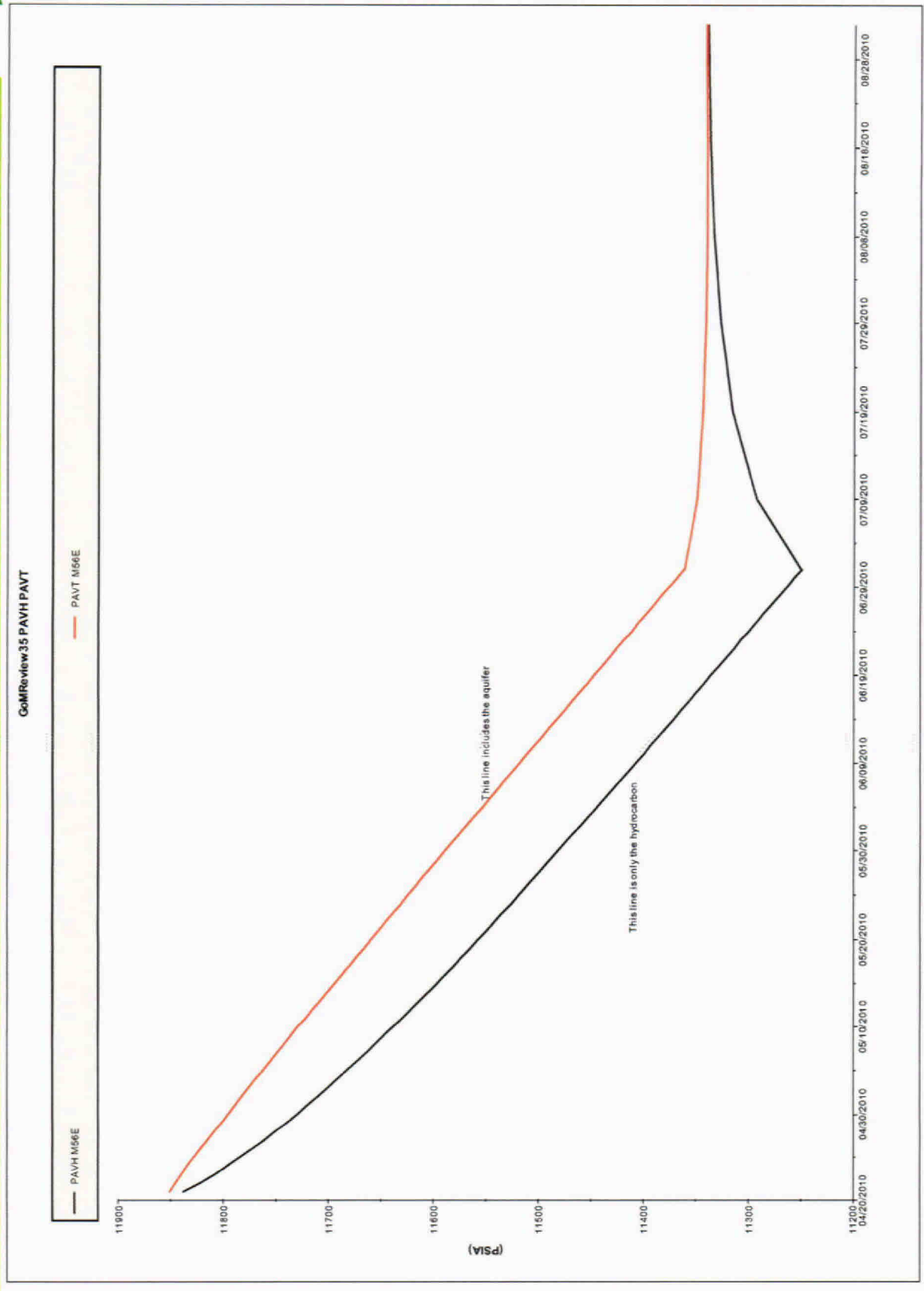
Back-Up

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Difference between Aquifer & H/C Pressure

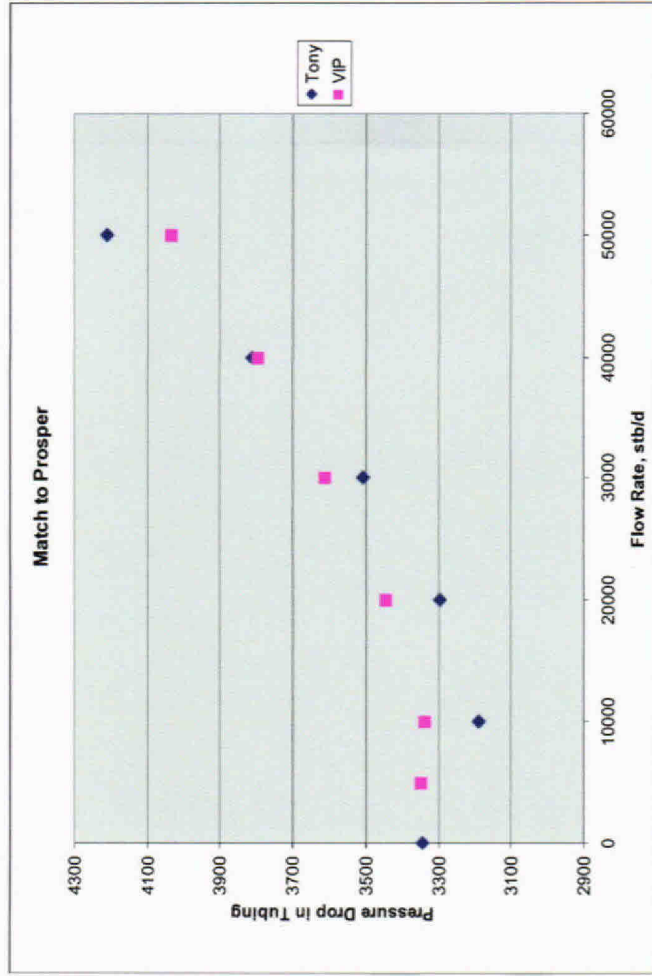


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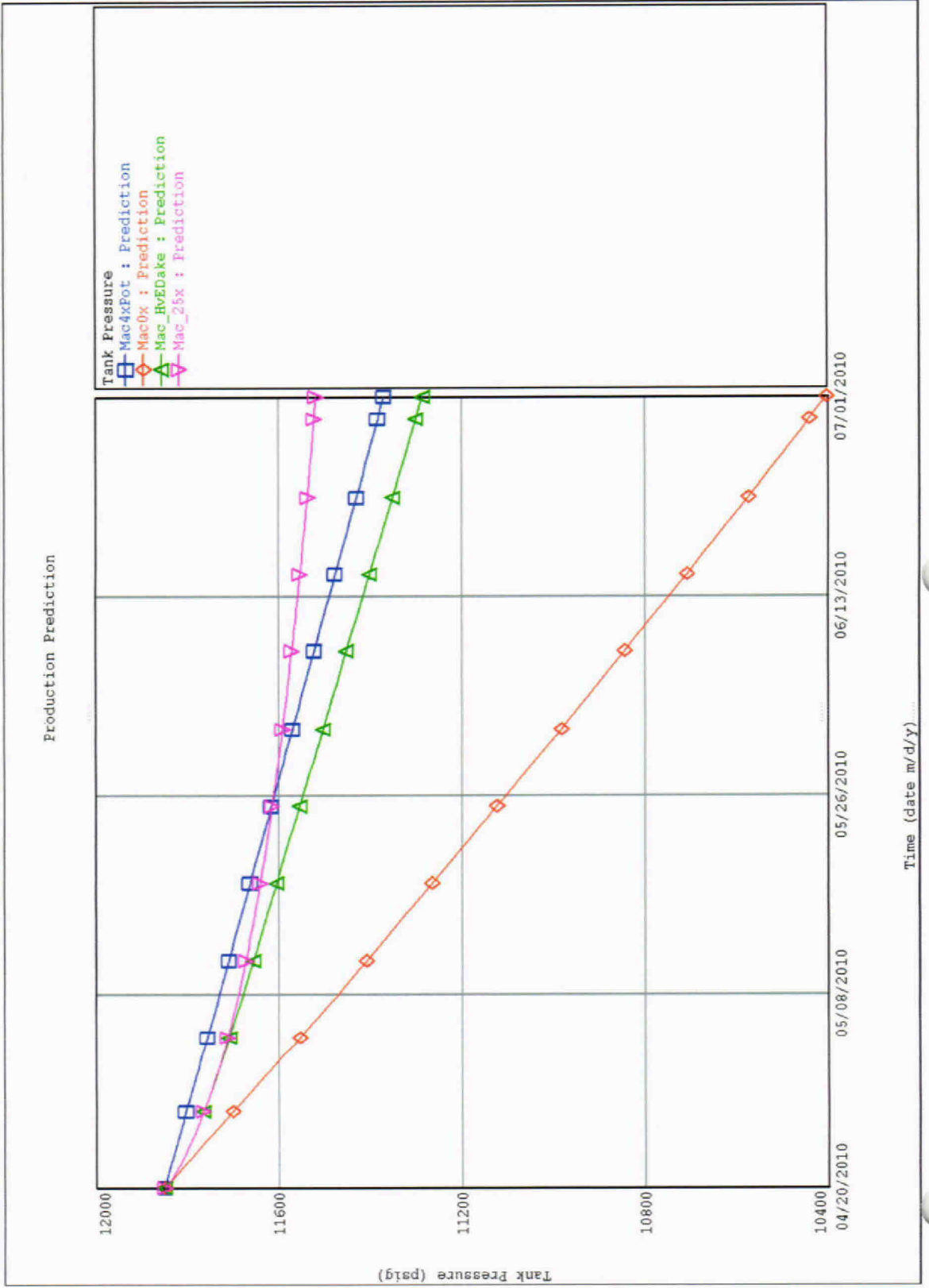
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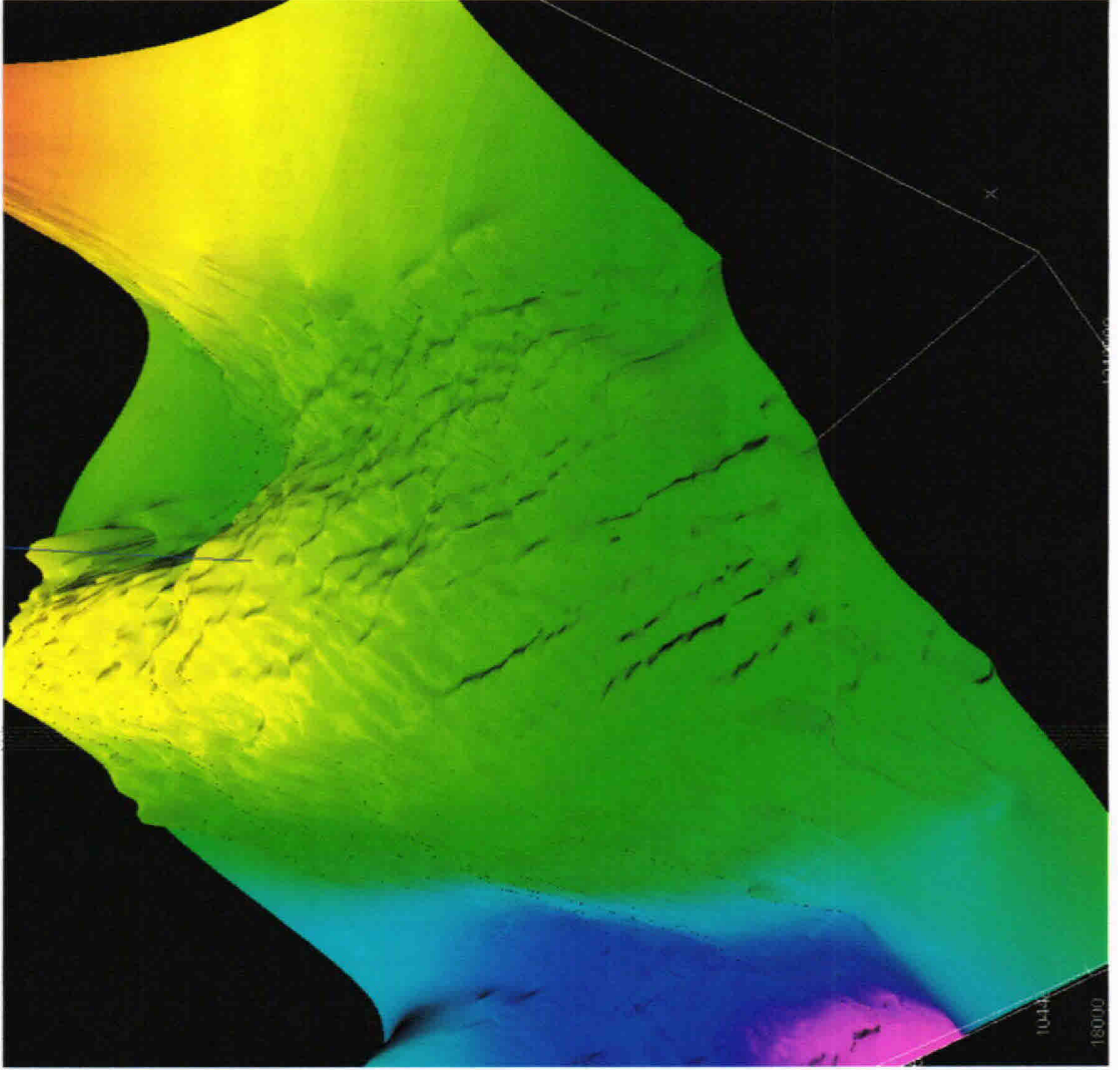


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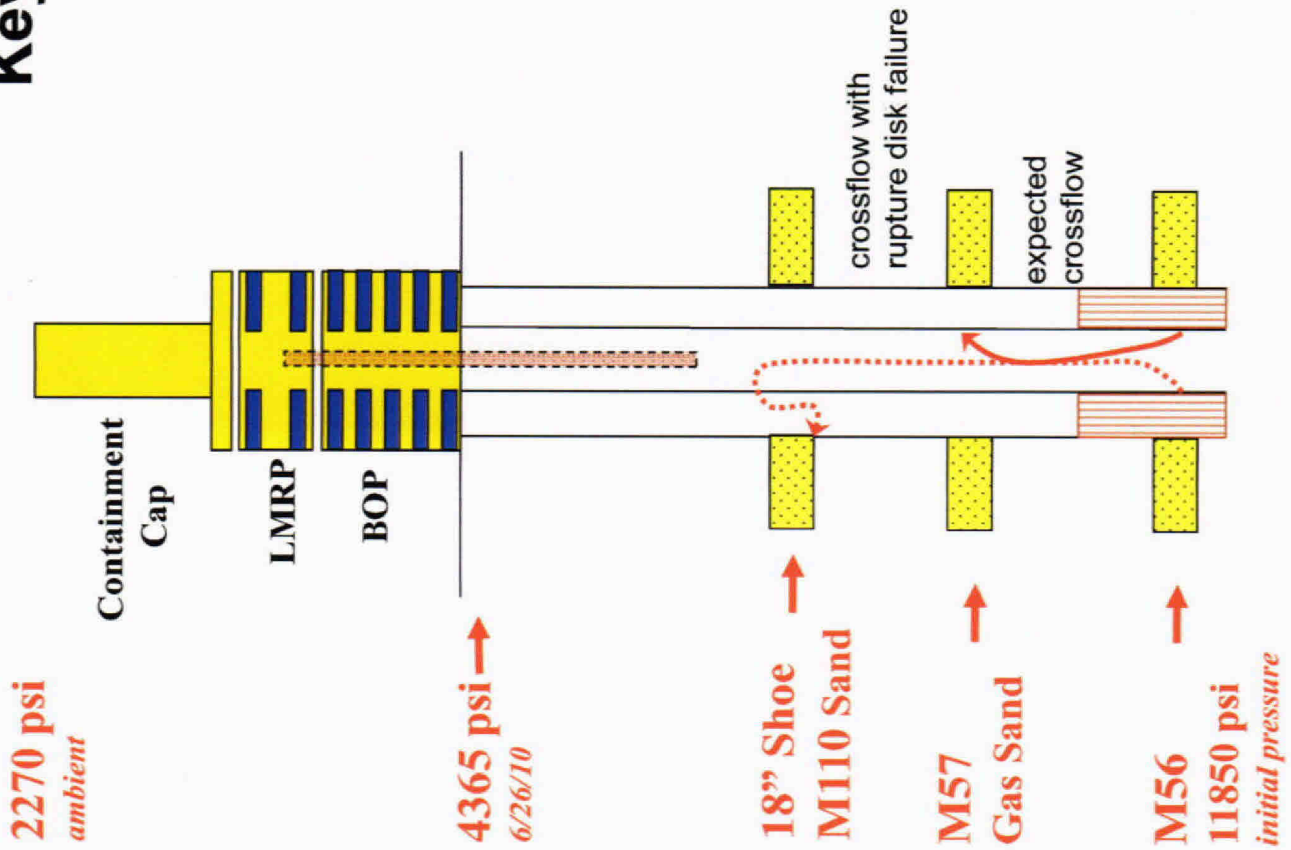
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