

I. What are proper assumptions for characterizing well performance?

--Tests performed and data from test (pressure vs time only)

II. . What analyses have been done that can characterize this performance?

--BP

--USGS

--DOE

III Outstanding questions

--Validity of Assumptions

--A path forward



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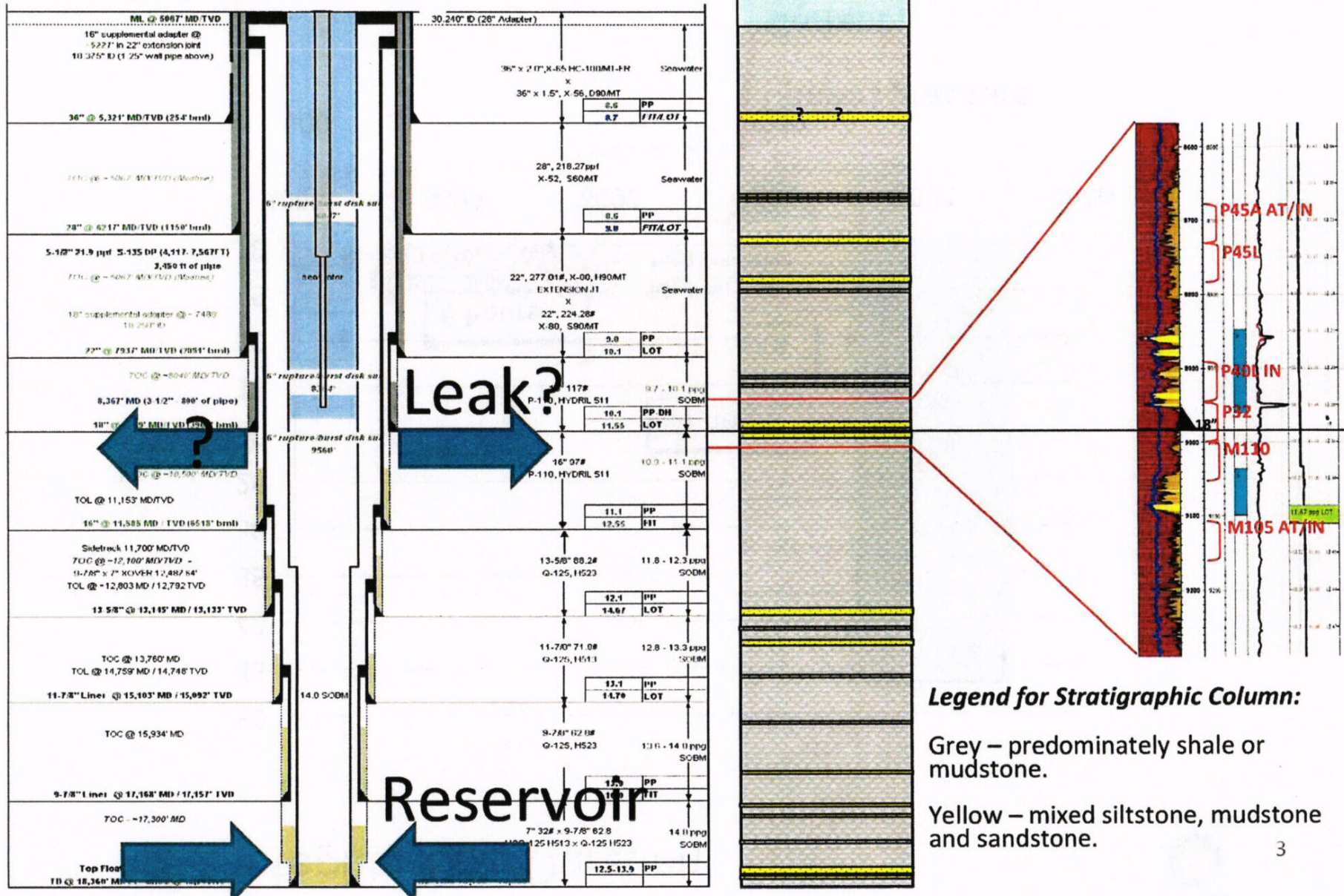
--DOE

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Reference Geometry - Below Mudline Shut In

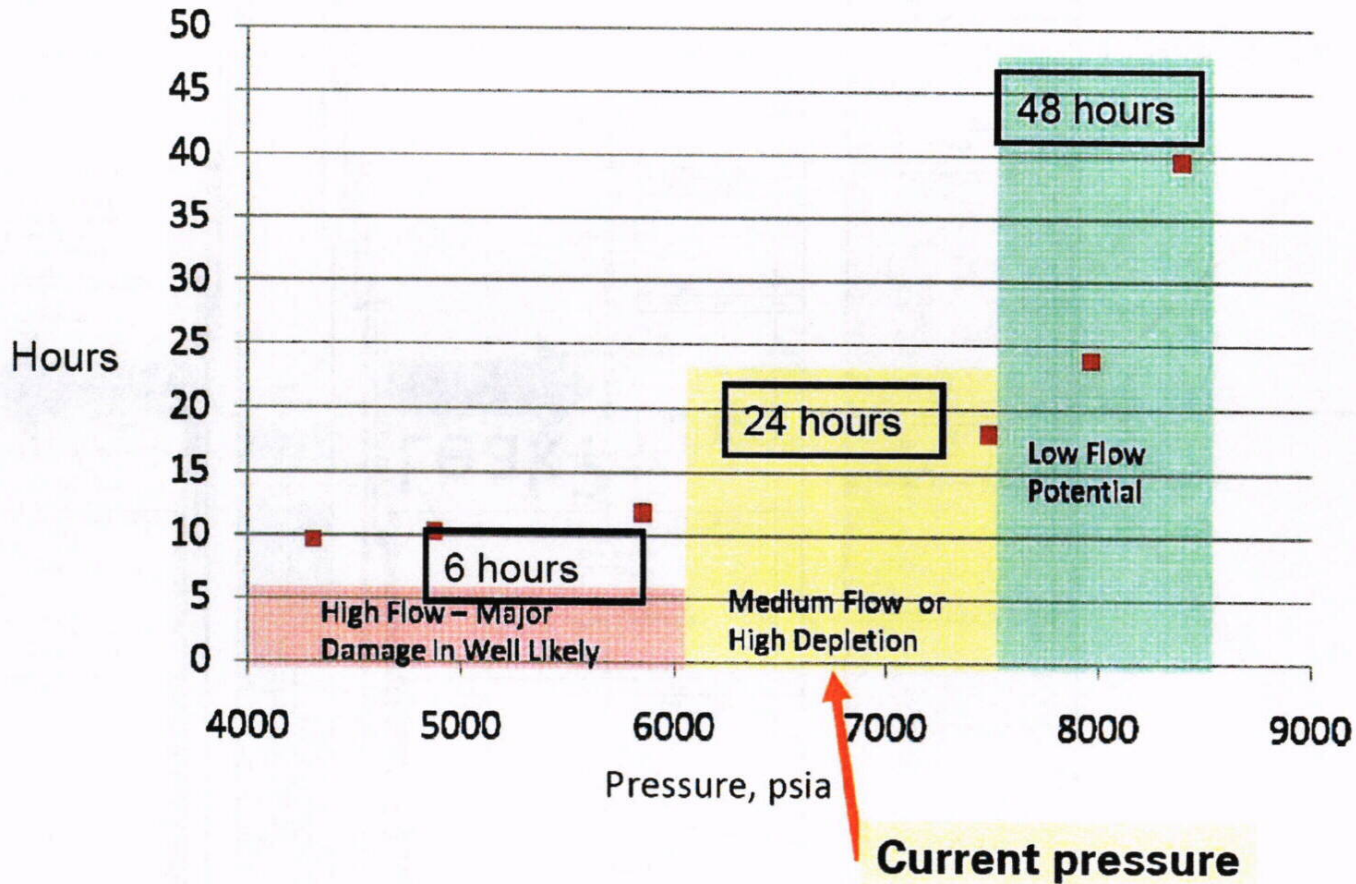


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IGS075-018205

TREX 008639.0003

Well Integrity Test Duration



2
4

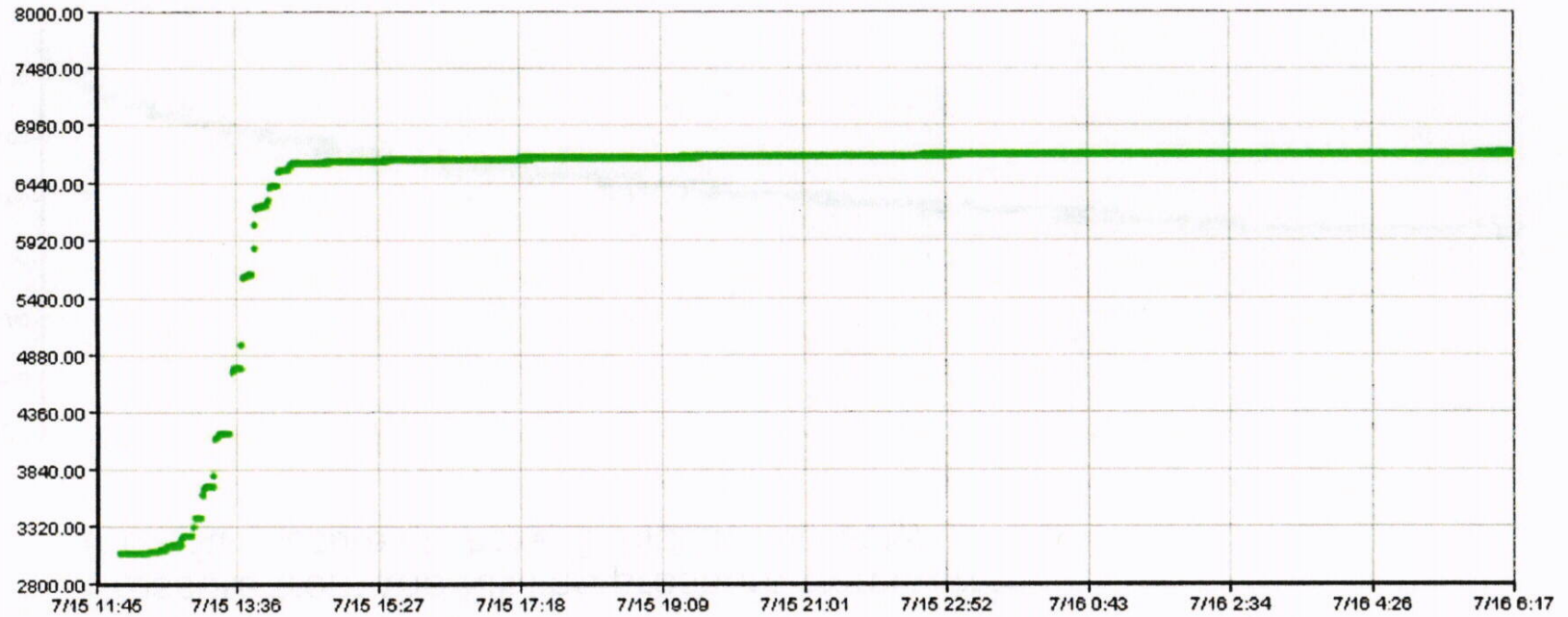
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Data



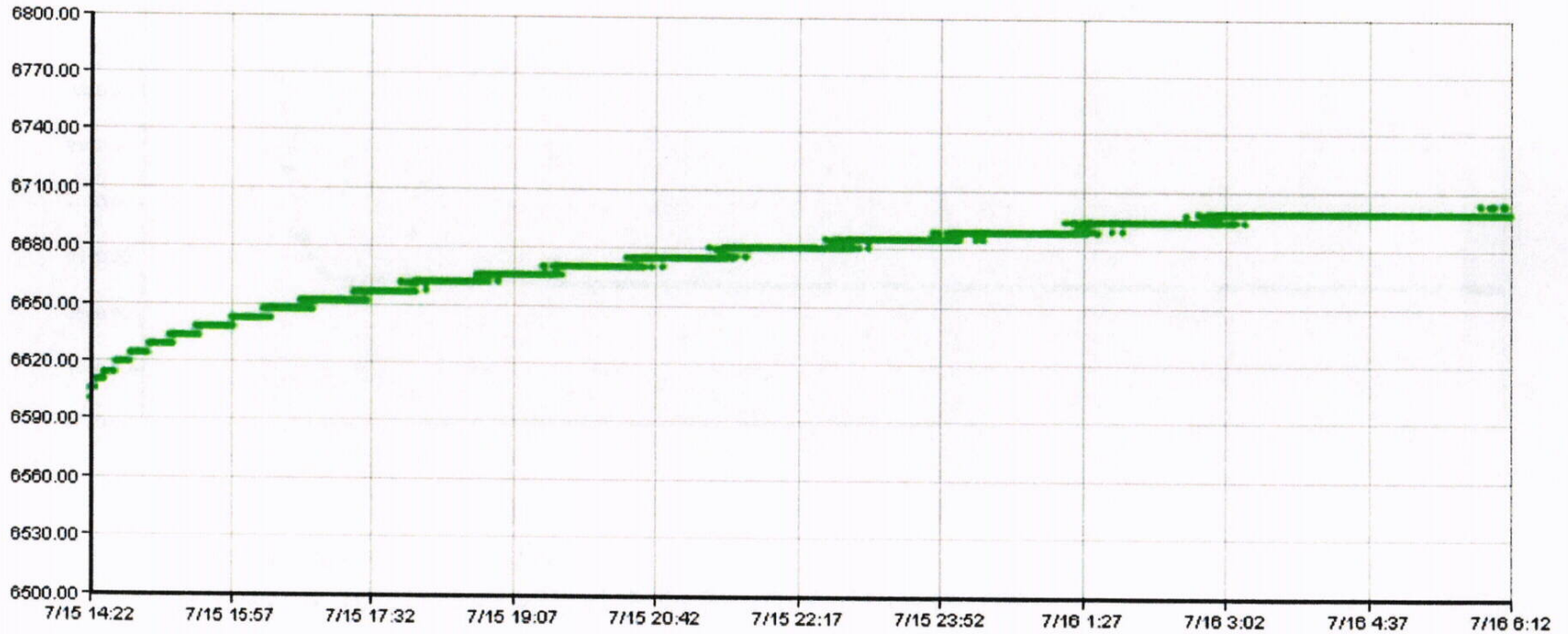
Pressure from the Kill line pressure transmitter
(from 11:45hrs 15th July)



Data



Pressure from the Kill line pressure transmitter
(from full closure of choke @ 14:22hr 15th July)



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Depletion Analysis - BP

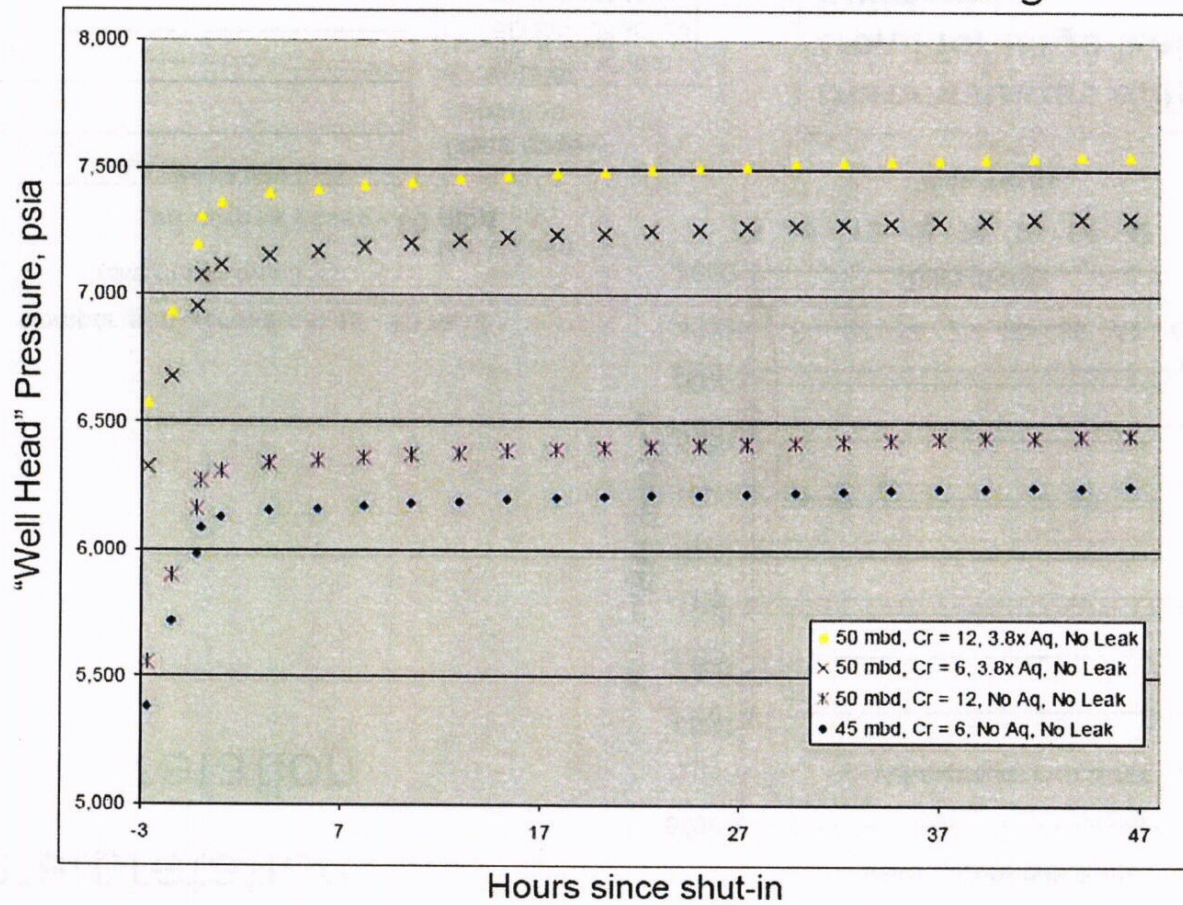
BP

Interpretation



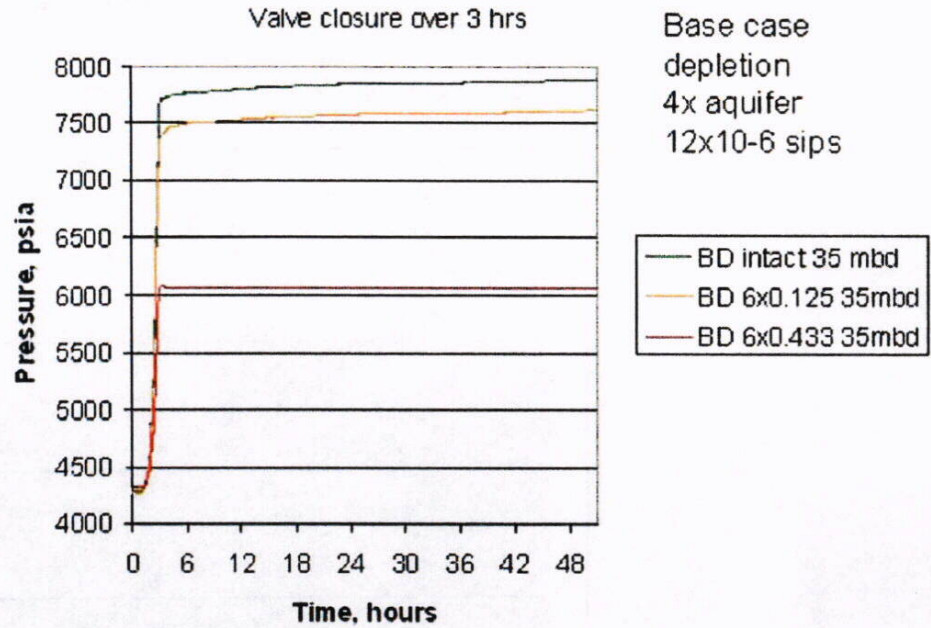
Demonstrates that observed pressures are in line with reasonable cases modeled

Scenario Pressure Trends - Modeling

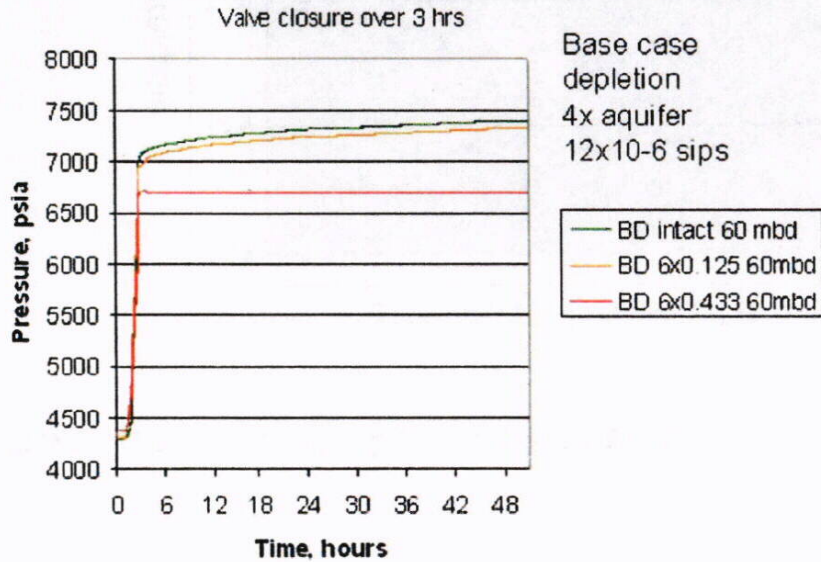


Interpretation

Comparison across cases - 35 mbd



Comparison across cases - 60 mbd

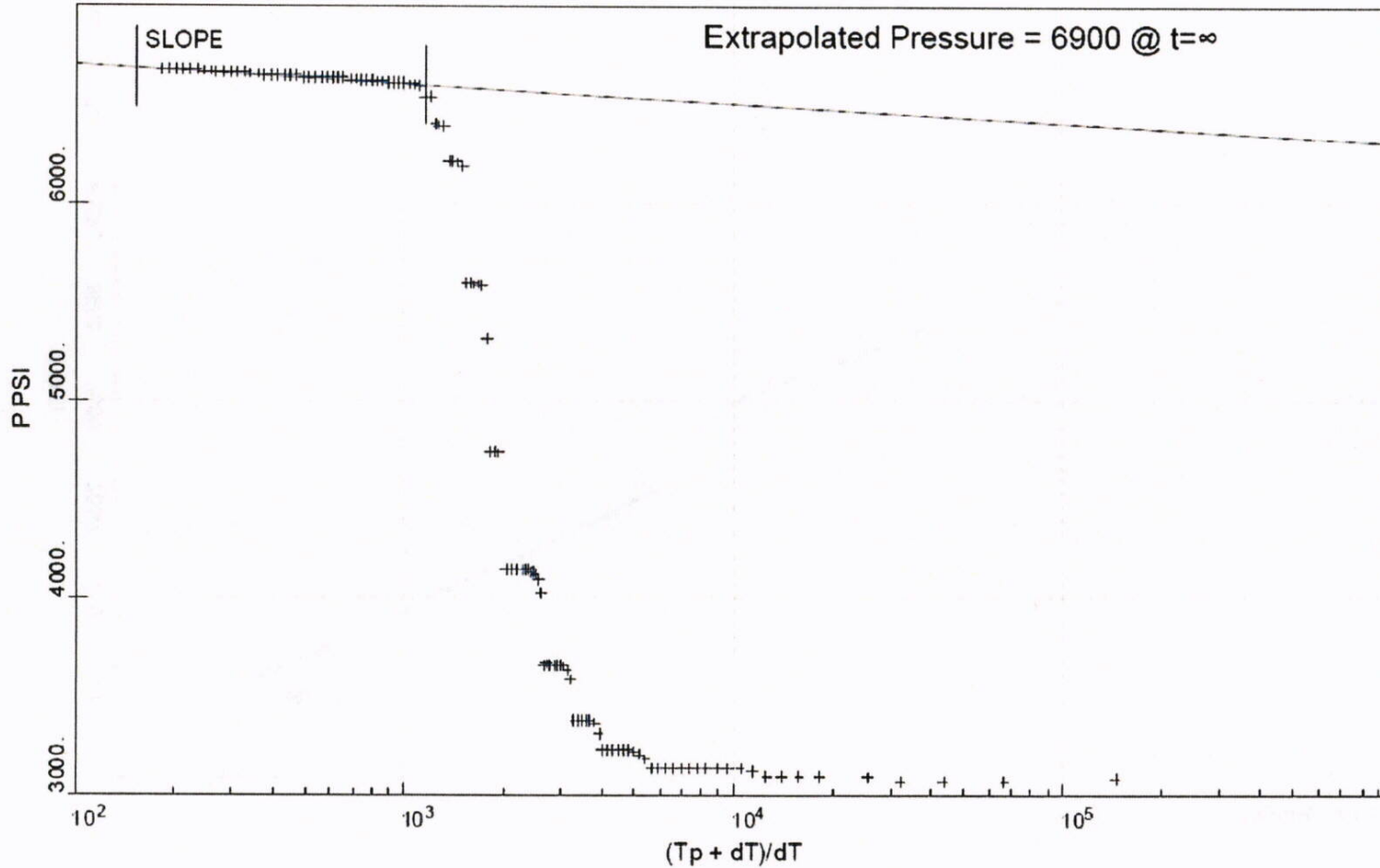


Demonstrates difference in trend for large leak vs. pressure build up.

Horner Plot – Including Data to 0:00 7/16



2010/07/15-1231 : OIL

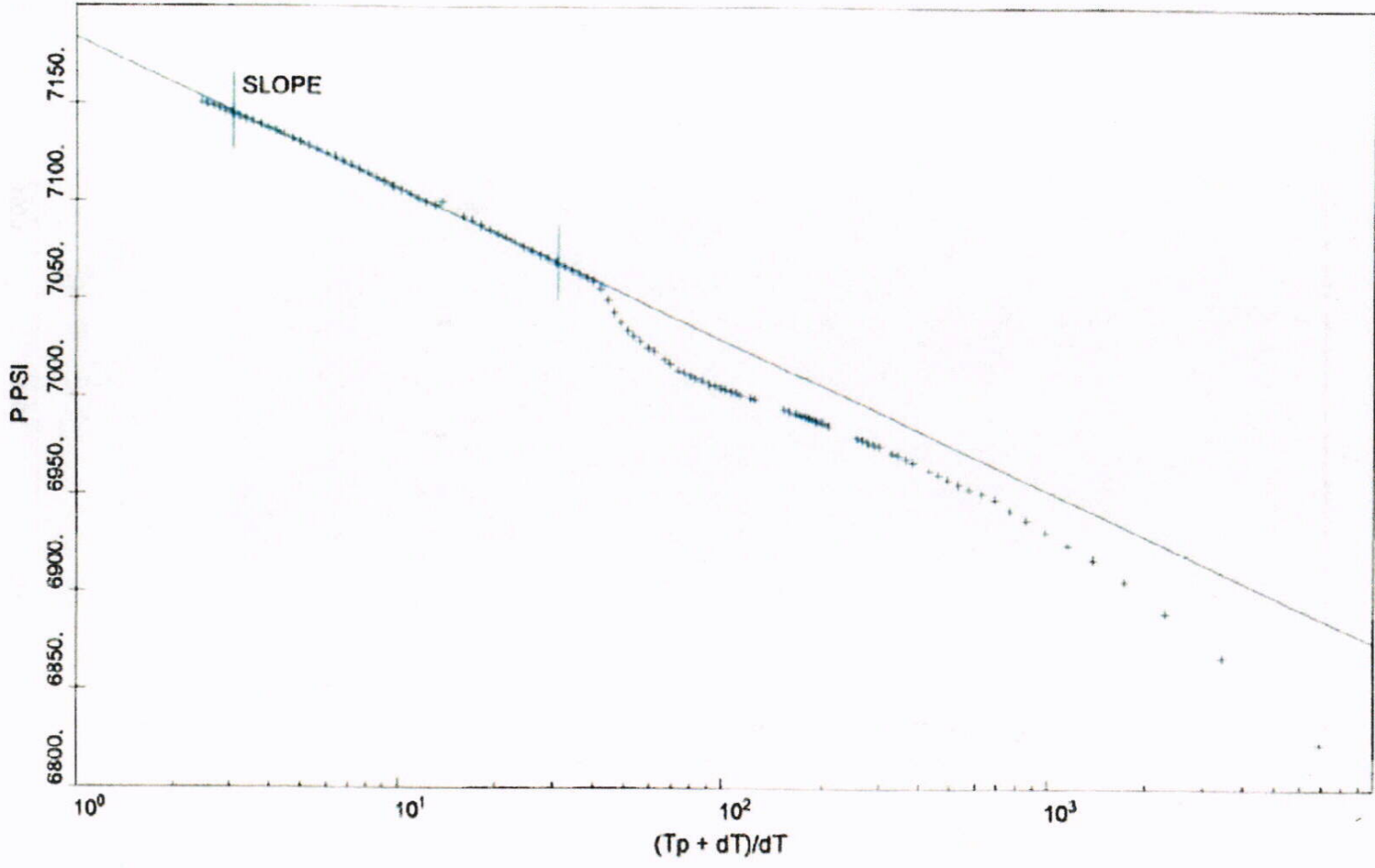


Macondo Macondo Test



Horner Plot (Thunderhorse)

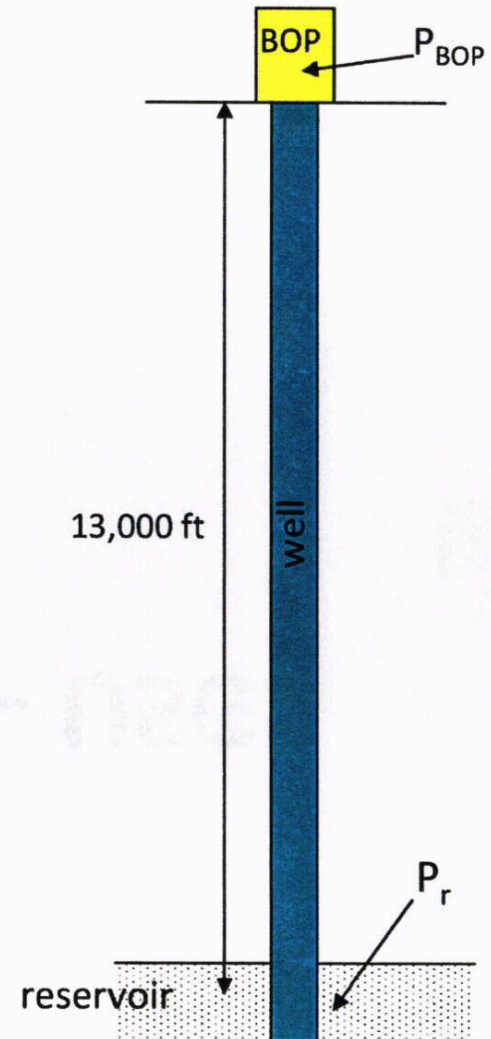
2004/04/19-1655 OIL



Depletion Analysis - USGS

Available Data

- Initial (pre-production) reservoir pressure:
 $P_r = 11,850$ psi
- Oil gradient = 0.25 psi/ft
- Initial pressure at BOP (static conditions):
 $P_{BOP} = P_r - (13,000 \text{ ft} \times 0.25 \text{ psi/ft}) = 8,600$ psi
- Final shut-in pressure at BOP = 6,700 psi
- Reservoir depletion = 1,900 psi

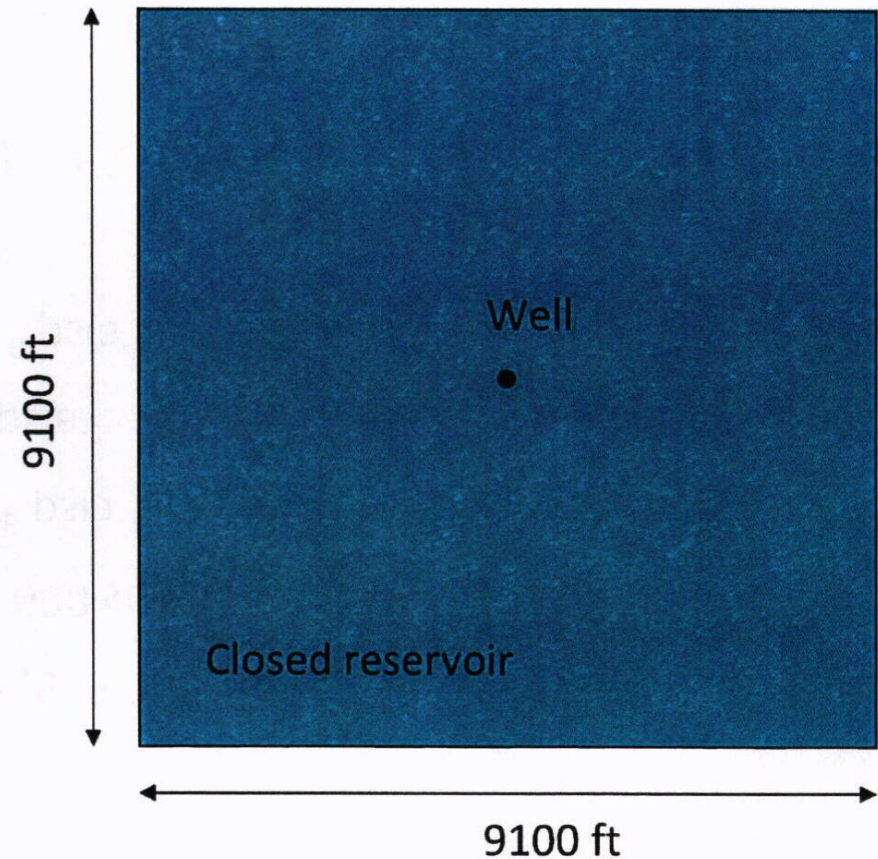


Depletion Calculation (without aquifer drive)

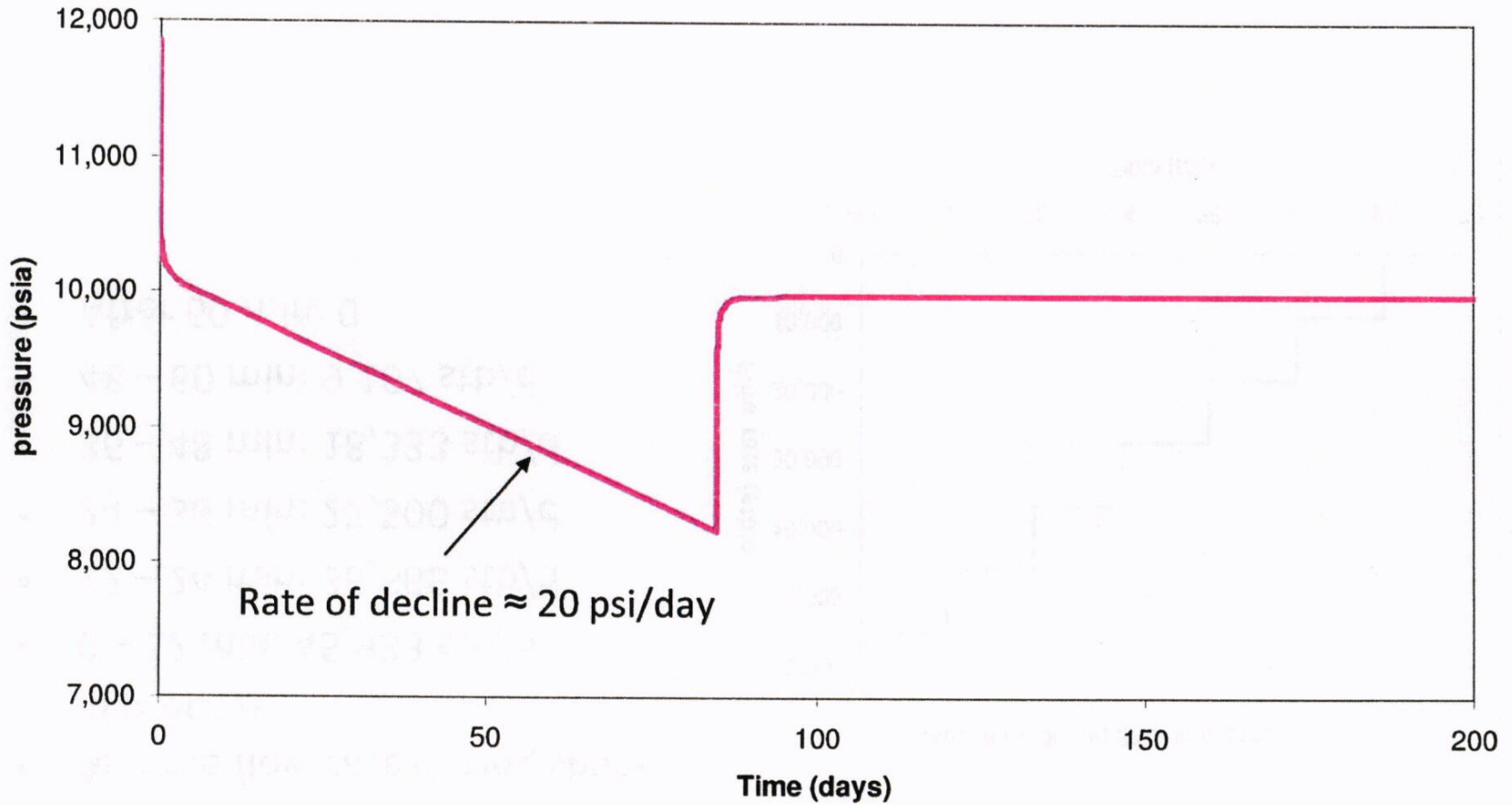
- Production rate = 55,000 stb/d
- Total production in 85 days = $V_p = 4,675,000$ stb
- Original Oil in Place = $V_o = 110,000,000$ stb
- Rock compressibility = $C_r = 12 \times 10^{-6}$ psia⁻¹
- Oil compressibility = $C_o = 12 \times 10^{-6}$ psia⁻¹
- Water compressibility = $C_w = 3 \times 10^{-6}$ psia⁻¹
- Water saturation = $S_w = 0.1$
- Total Compressibility = $C_T = (1 - S_w)C_o + S_w C_w + C_r$
 $= 23 \times 10^{-6}$ psia⁻¹
- Pressure depletion = $V_p / V_o / C_T = 1,850$ psi

Single-phase oil flow simulation

- No casing damage
- Reservoir thickness = 93 ft
- Permeability = 220 md
- Porosity = 20%
- Total Compressibility = $23 \times 10^{-6} \text{ psi}^{-1}$
- Production rate = 55,000 stb/d for 95 days
- Oil viscosity = 0.21 cp
- Oil density = 0.568 gm/cc

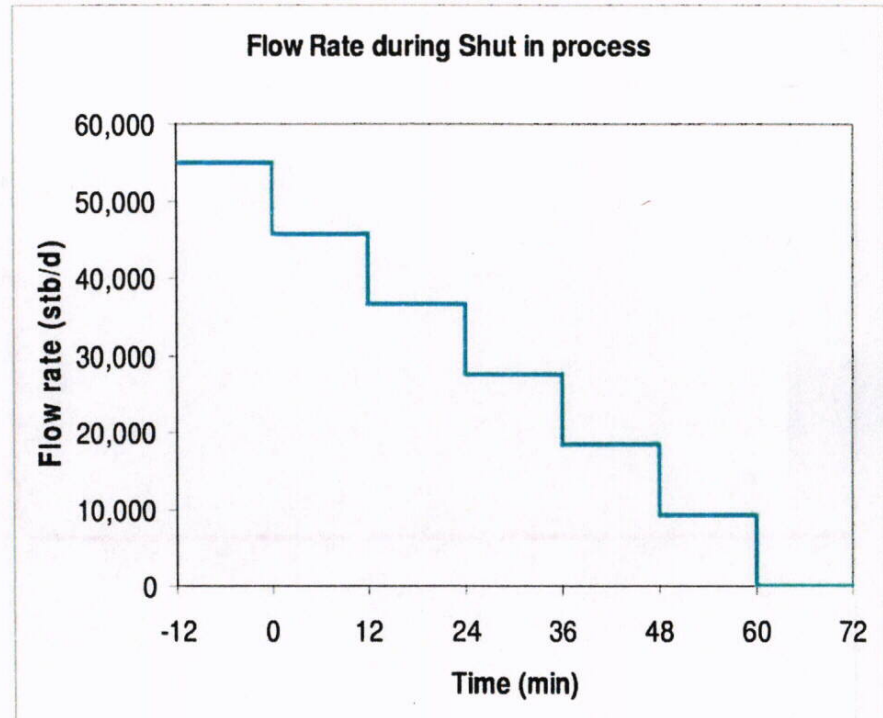


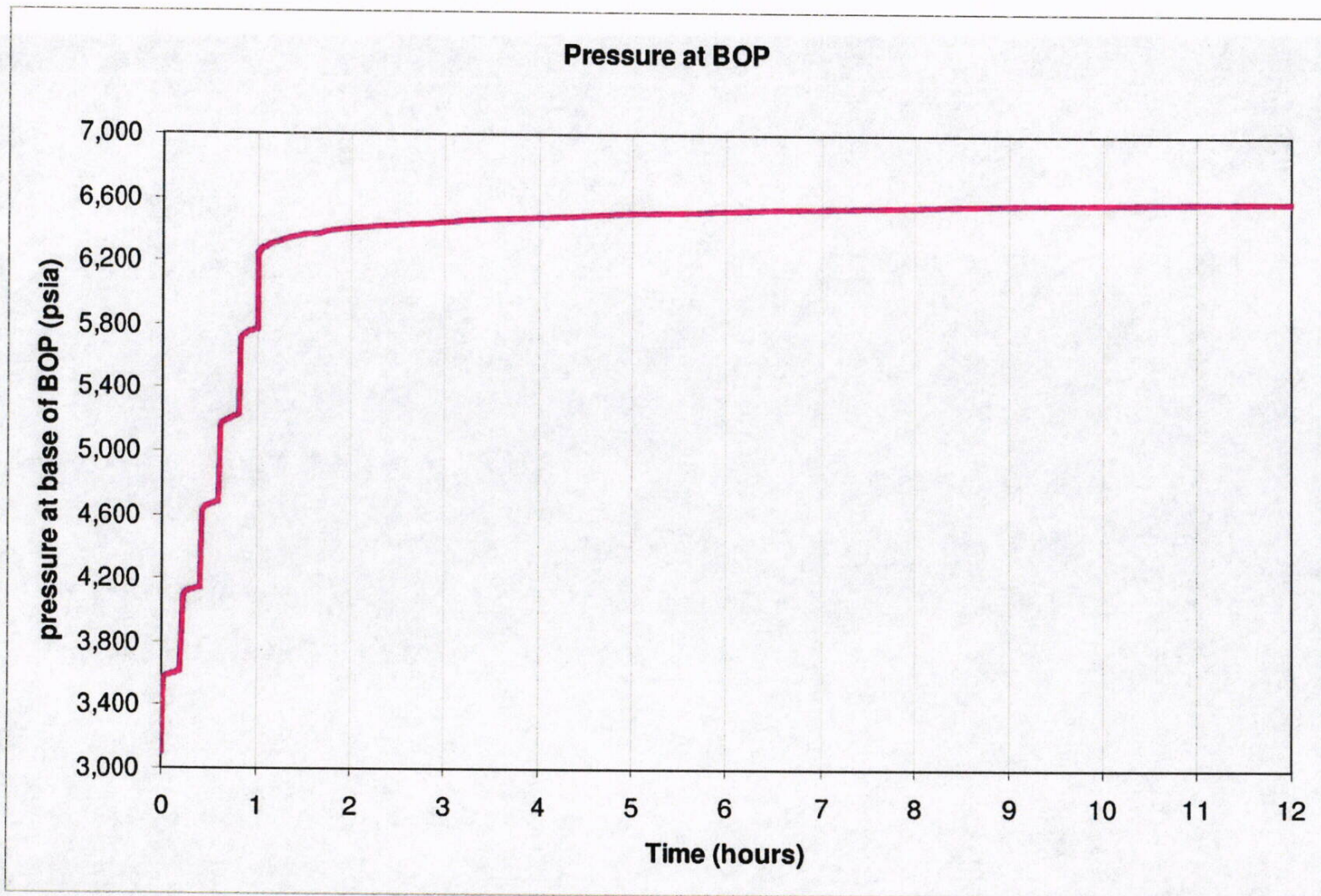
Reservoir Pressure at sandface

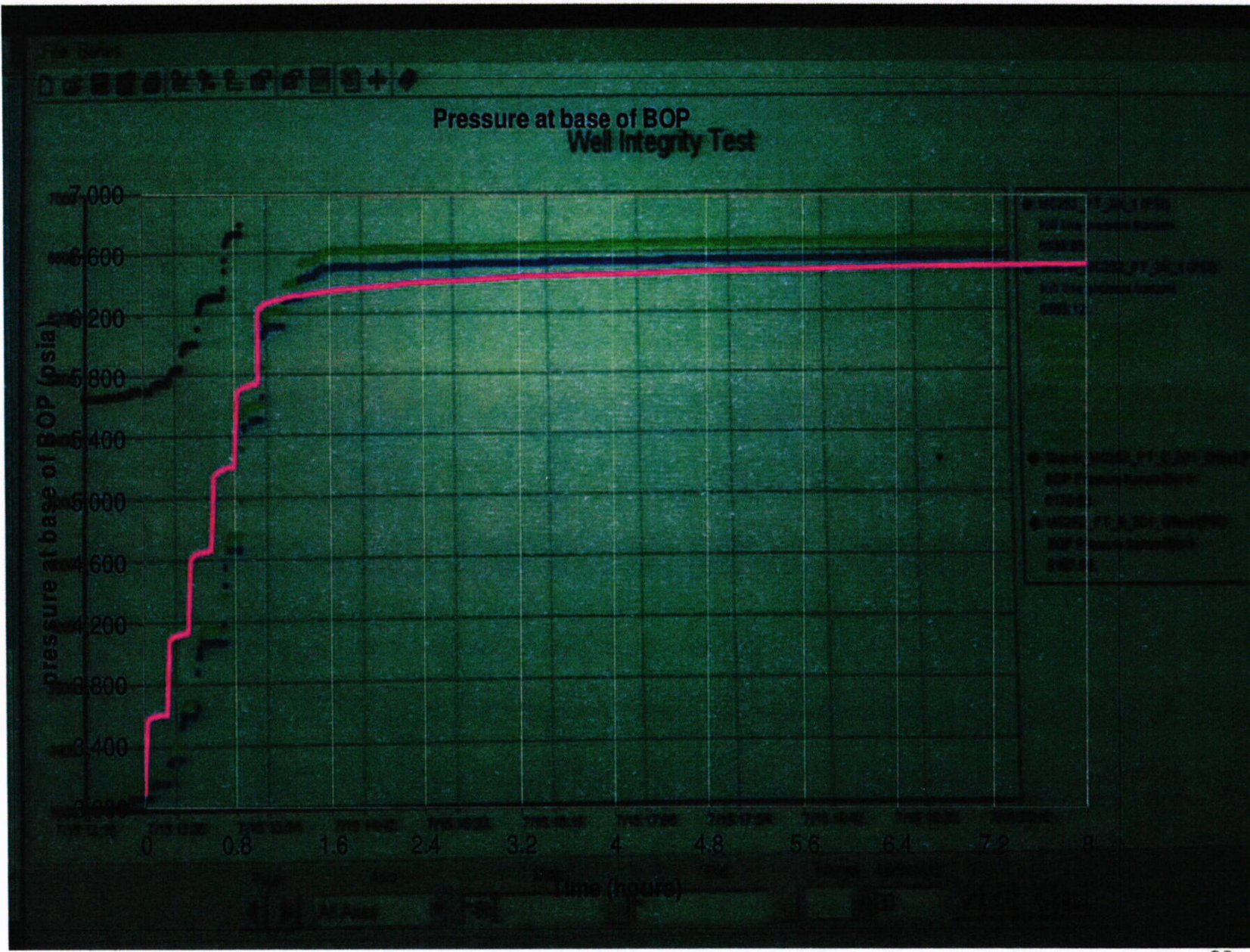


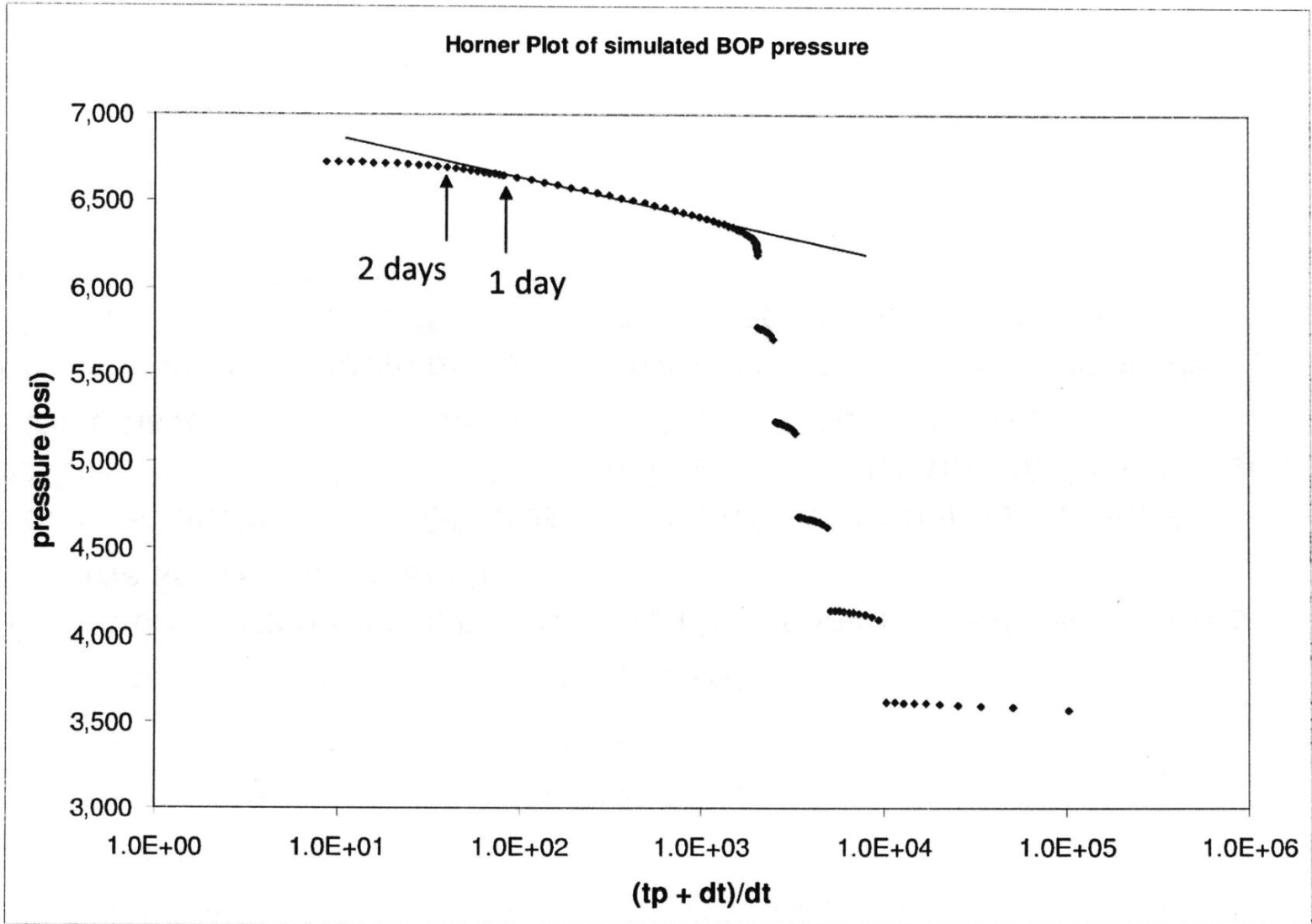
Simulation of Shut-in Process

- Assume flow rate during shut-in process:
- 0 – 12 min: 45,833 stb/d
- 12 – 24 min: 36,666 stb/d
- 24 – 36 min: 27,500 stb/d
- 36 – 48 min: 18,333 stb/d
- 48 – 60 min: 9,167 stb/d
- After 60 min: 0









USGS Conclusions

- Observed shut-in pressure data can be explained by a closed reservoir
 - No aquifer drive
 - 110 million stb of oil originally in place
 - flow rate of 55,000 stb/d for 85 days
 - reasonable values of reservoir properties
- Shut-in pressure data can be simulated by a conventional reservoir model with the above characteristics.
- However, during flow, BOP pressure should be dropping at about 20 psi/day. For example, during the final month before shut in, BOP pressure should have dropped by about 600 psi. This is not observed.
- Horner plot shot should break towards a flat line a few days after shut-in. This should be checked if shut in is extended. (However, temperature change has not been considered.)

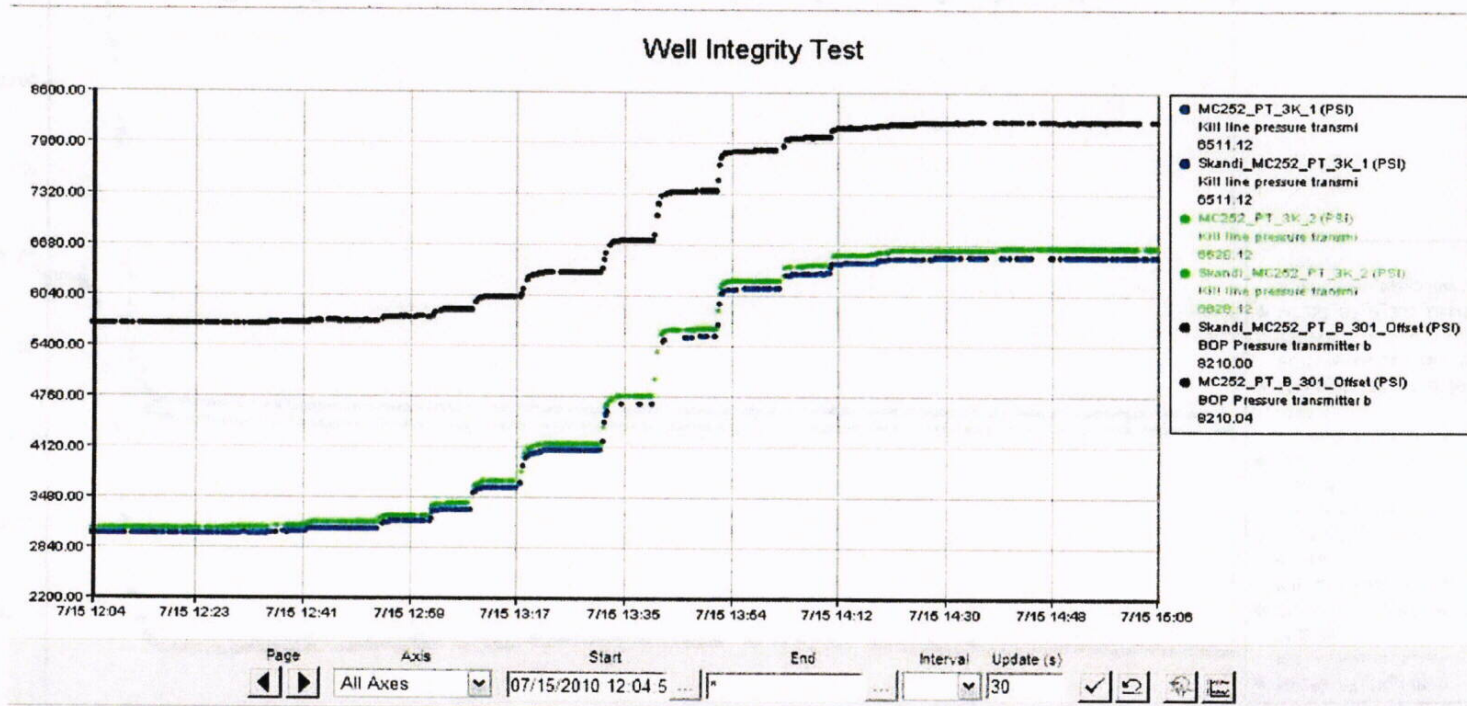
Flow Analysis - DOE

Flow Analyses: What we know

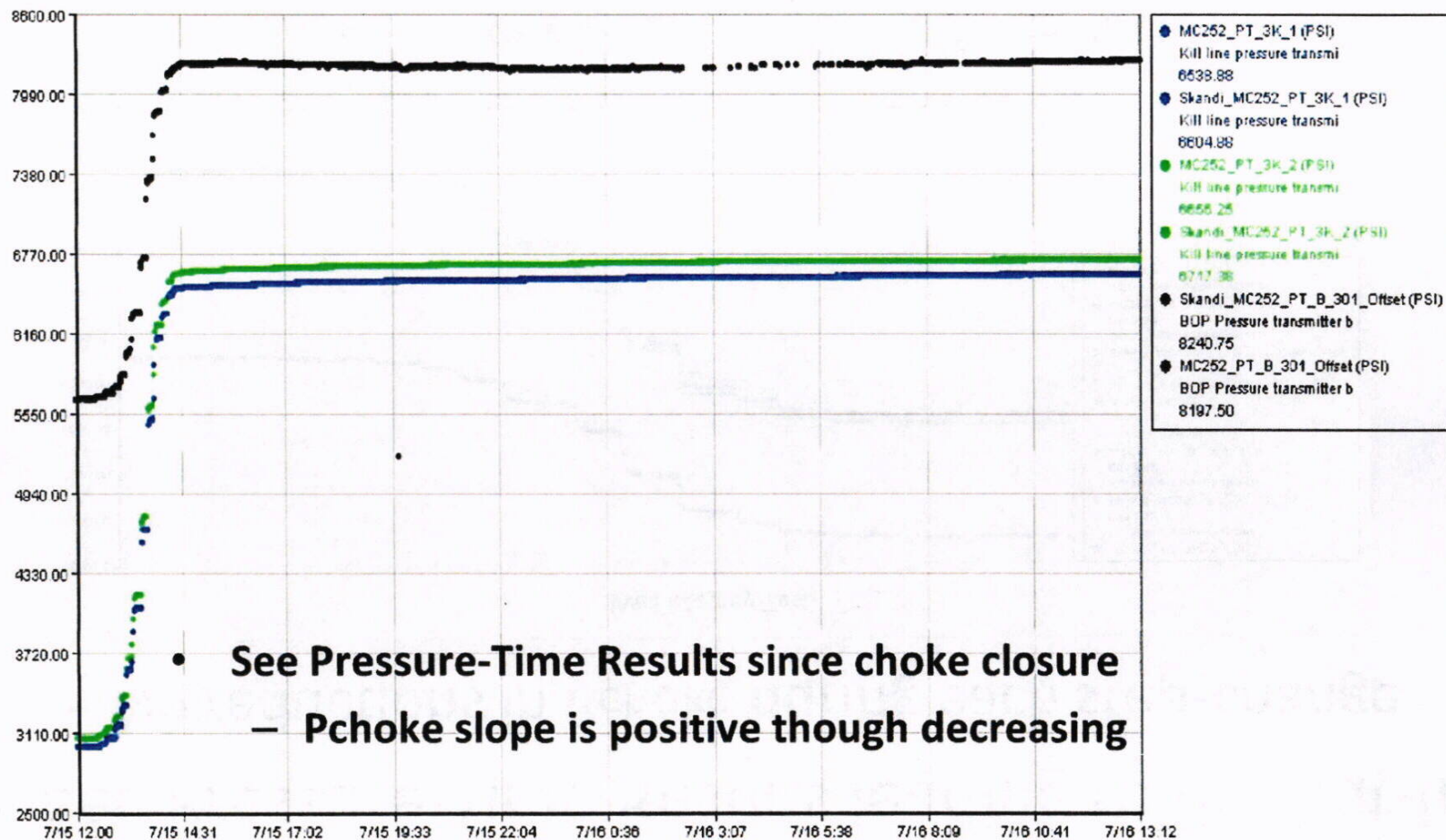
- Estimates from Flow Analyses provide mass flow estimates of 45K-65K bbl/day based on a number of different models (analysis is ongoing)
- Computational analysis of the test are inconclusive regarding the existence of or size of a leak.
- We concur with BP's assessment that the post-shut-in results are consistent with expectations of reservoir recovery (pressure increased after test and rate decreasing with time)

Consider results from Shut-in Test

- See Pressure-Time Results leading to fill shut-in
 - No reductions in Pchoke during each step-change



Consider results from Shut-in Test



<http://gomdwproucessnet.bpweb.bp.com/processnet/isapi/netportal/netportal.dll?html/wellintegritytest>

7/16/2010

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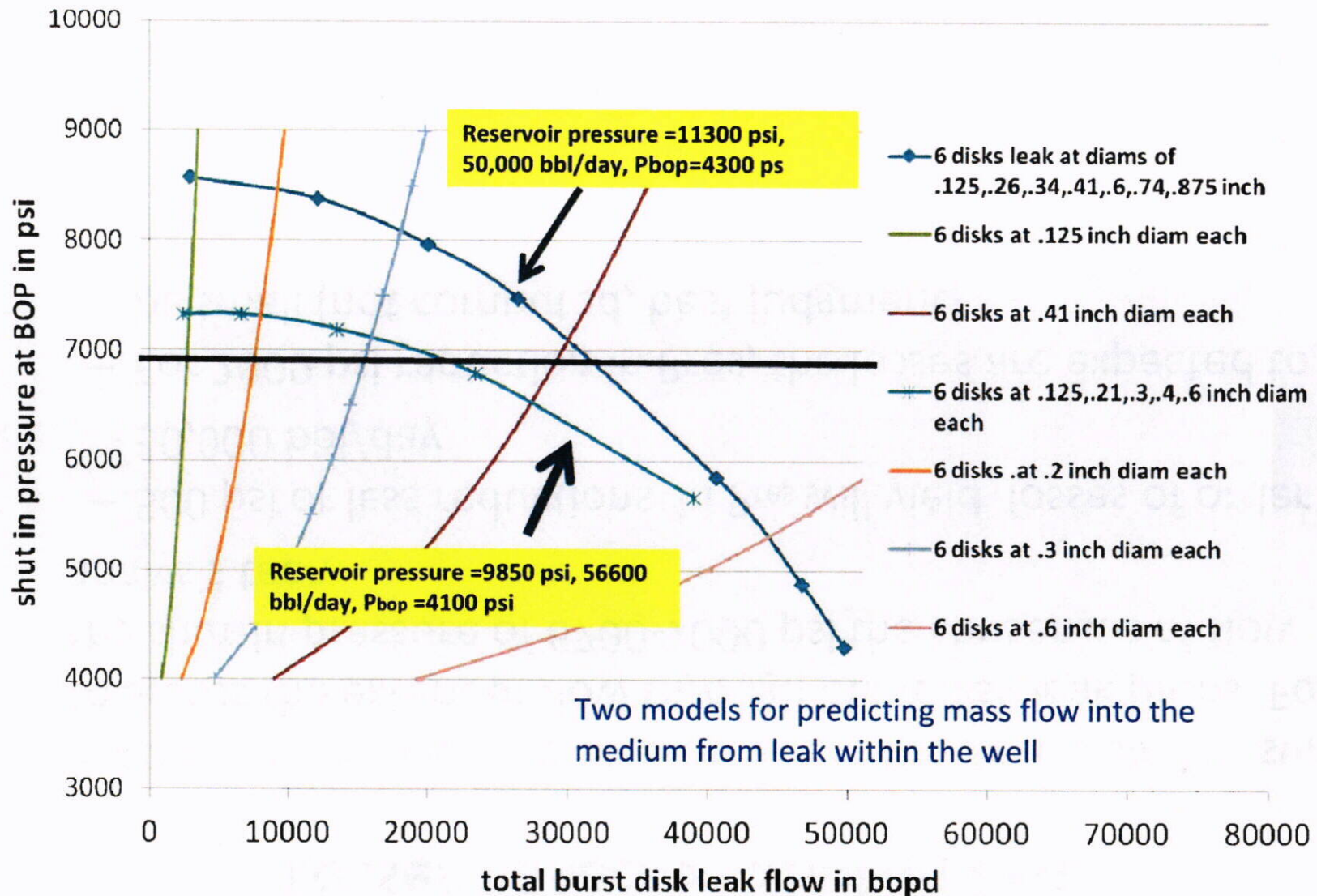
IGS075-018228

TREX 008639.0026

Flow Analysis Team Views on the Potential Losses based on Shut-in test

- Bottom Line: Must have an estimate of the Reservoir Pressure to assess the extent of flow through burst disk leak paths. For the shut-in pressure of 6700-7000 psi the consensus of flow analysis team
 - 500 psi or less reductions in P_{res} will yield losses of order 30,000 bbl/day
 - For 2000 psi reduction in P_{res} , the losses are expected to be small (not computed, best judgment)

Flow in Well Issues – Flow Rate Bounds



10/25/2011-1400 CDT

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III Outstanding questions

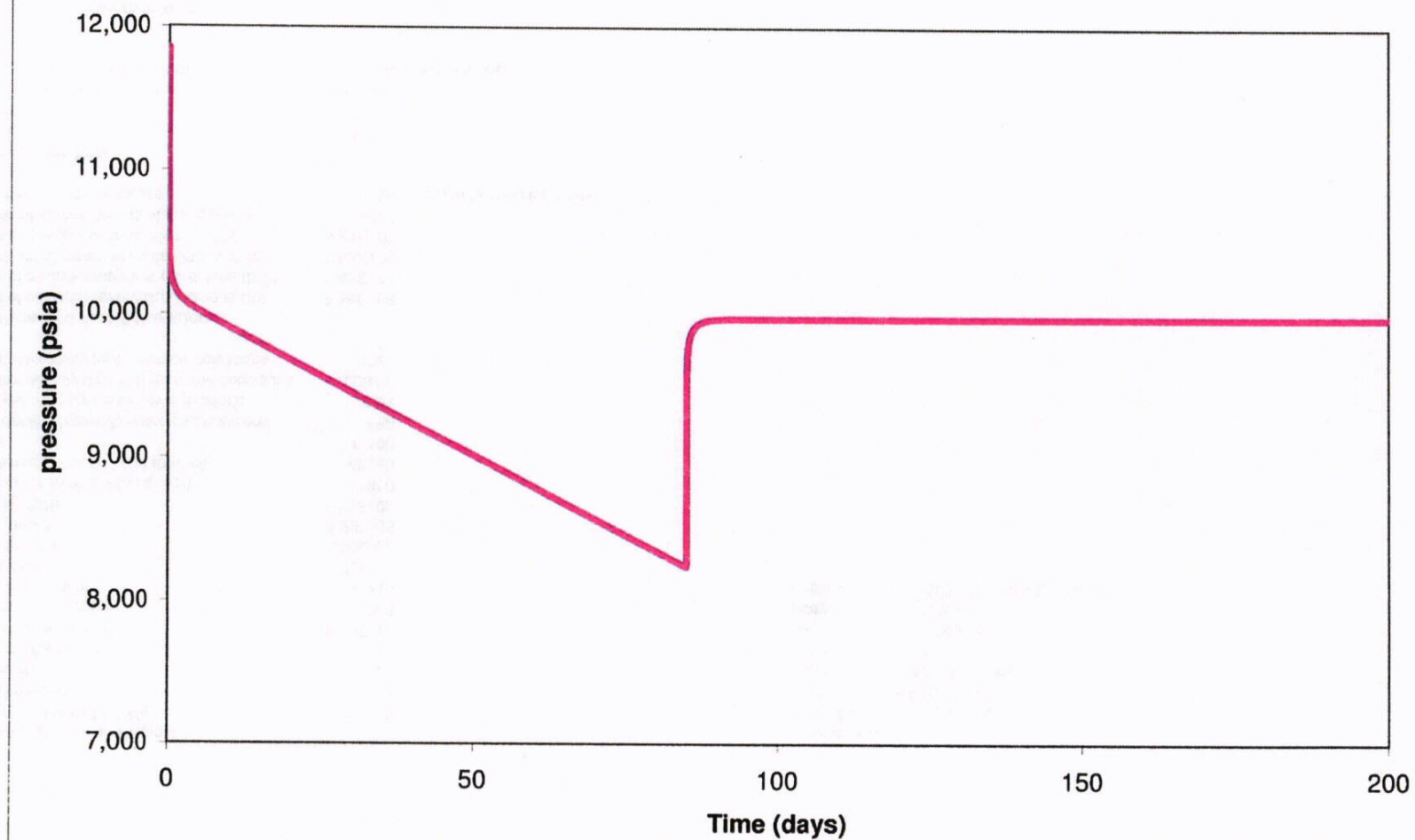
--Validity of Assumptions

--A path forward

Questions

- 1) How likely is it that Macondo 252 is **not** connected to a water aquifer? In order to get the reservoir pressure to drop by 2,000 psi due to well-depletion, there can be virtually no connection to a water reservoir
- 2) The rate of change of pressure and the absolute data are consistent with high depletion and no or very low leak or low depletion and high leak. How do we differentiate between these two scenarios? The large depletion scenario asymptotes to $\sim 7,300$ psi, not the $\sim 6,800$ psi we are seeing. This calculation is not consistent with BP calculations: the two teams are supposed to be comparing their assumptions.
- 3) How do we confirm the assertion that if the well is not connected to an aquifer and has been depleted by 2000 psi, then the pressure at the reservoir must have dropped by 2000 psi? If so, then the pressure at the bottom of the BOP must have dropped a substantial fraction of this amount.

Reservoir Pressure at sandface



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TREX 008639.0031

Reservoir + Fluid Properties

depth to top (ft TVDSS)	18000
thickness (ft)	93
porosity	0.21
permeability (md)	219
permeability (m ²)	2.16E-13
temperature deg F	243
Oil Boi (rb/stb)	2.345
cf (psia-1)	1.20E-05
cw (psia-1)	3.00E-06
co (psia-1)	1.20E-05
OOIP (stb)	1.10E+08
initial reservoir pressure (psi)	11850
initial reservoir oil head (ft of oil)	48153
Sw	0.100
oil density (kg/m ³) reservoir conditions	568
oil viscosity (cp) reservoir conditions	0.21
water density (kg/m ³) reservoir conditions	1000.00
water viscosity (cp) reservoir conditions	0.27

Volume and Area Calculations

vol of oil under reservoir conditions (rb)	2.58E+08
vol of oil under reservoir conditions (ft ³)	1.45E+09
bulk vol of reservoir containing oil (ft ³)	7.66E+09
area of reservoir containing oil (ft ²)	8.24E+07
Side of square area containing oil (ft)	9078
half of the side of square	4539 rounded to 4500 for model

Production Rate

(stb/d)	55000
(rb/d)	128975
ft ³ /d under reservoir conditions	724195
1/4 of production rate (f ³ /d)	181049 used in model

Hydraulic conductivity (oil)

(m/s)	5.73E-06 =rho*g*k/mu
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Conversion

1 barrel =	5.615 ft ³
1 md =	9.87E-16 m ²
1 cp =	1.00E-03 kg/m/s
1 m =	3.281 ft
1 ft =	0.3048 m
1 day =	86400 s
1 psia =	6894 N/m ² = kg/m/s ²

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TREX 008639.0032

(ft/d)	1.62
Hydraulic conductivity (water)	
(m/s)	7.85E-06
(ft/d)	2.22
Specific Storage (oil)	
total compressibility (psia-1)	$2.31E-05 = (1-S_w)c_o + S_w*c_w + c_f$
total compressibility (m*s^2/kg)	3.35E-09
Ss (m-1)	3.53E-06
Ss (ft-1)	1.07E-06

Reservoir Pressure at sandface

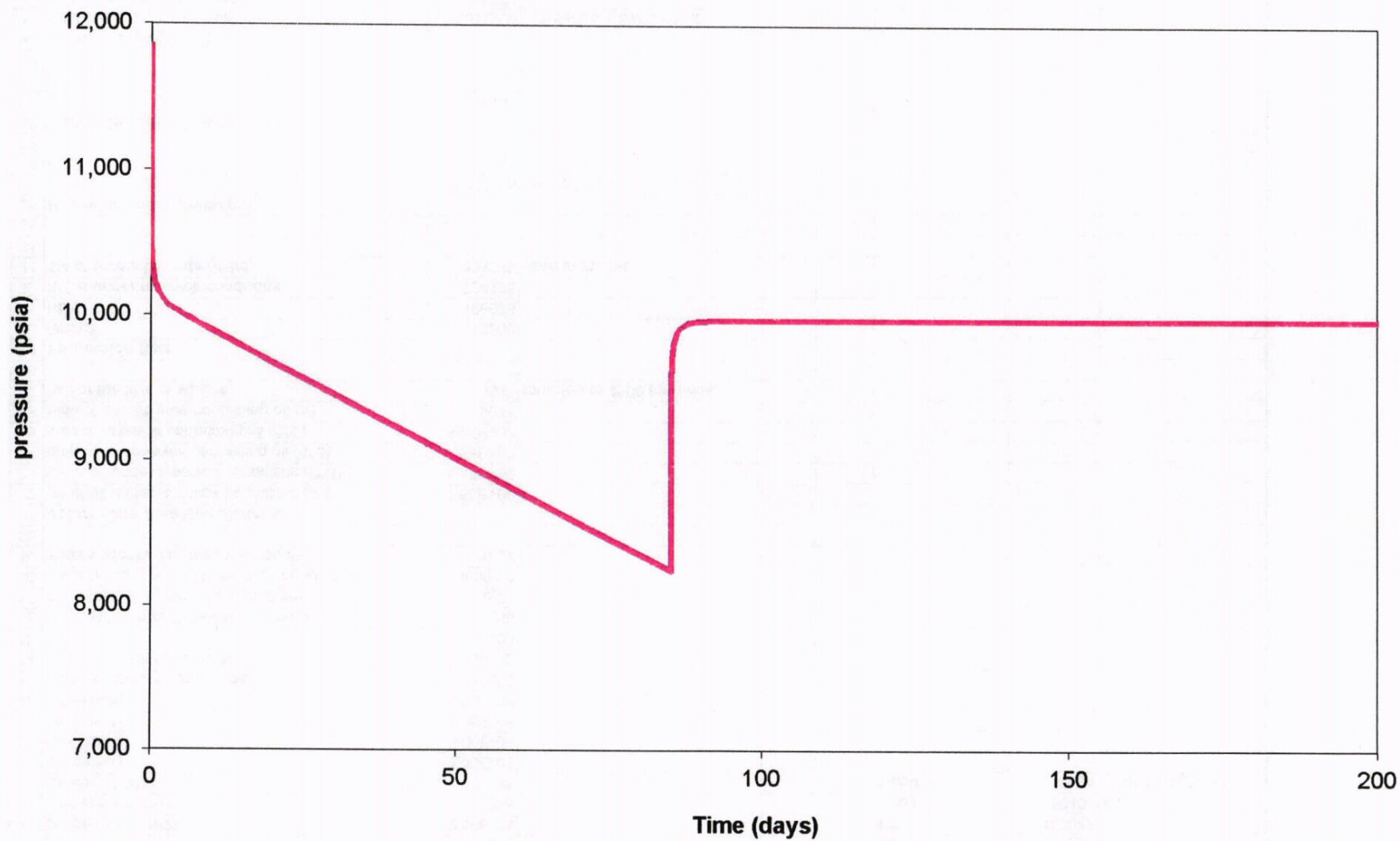
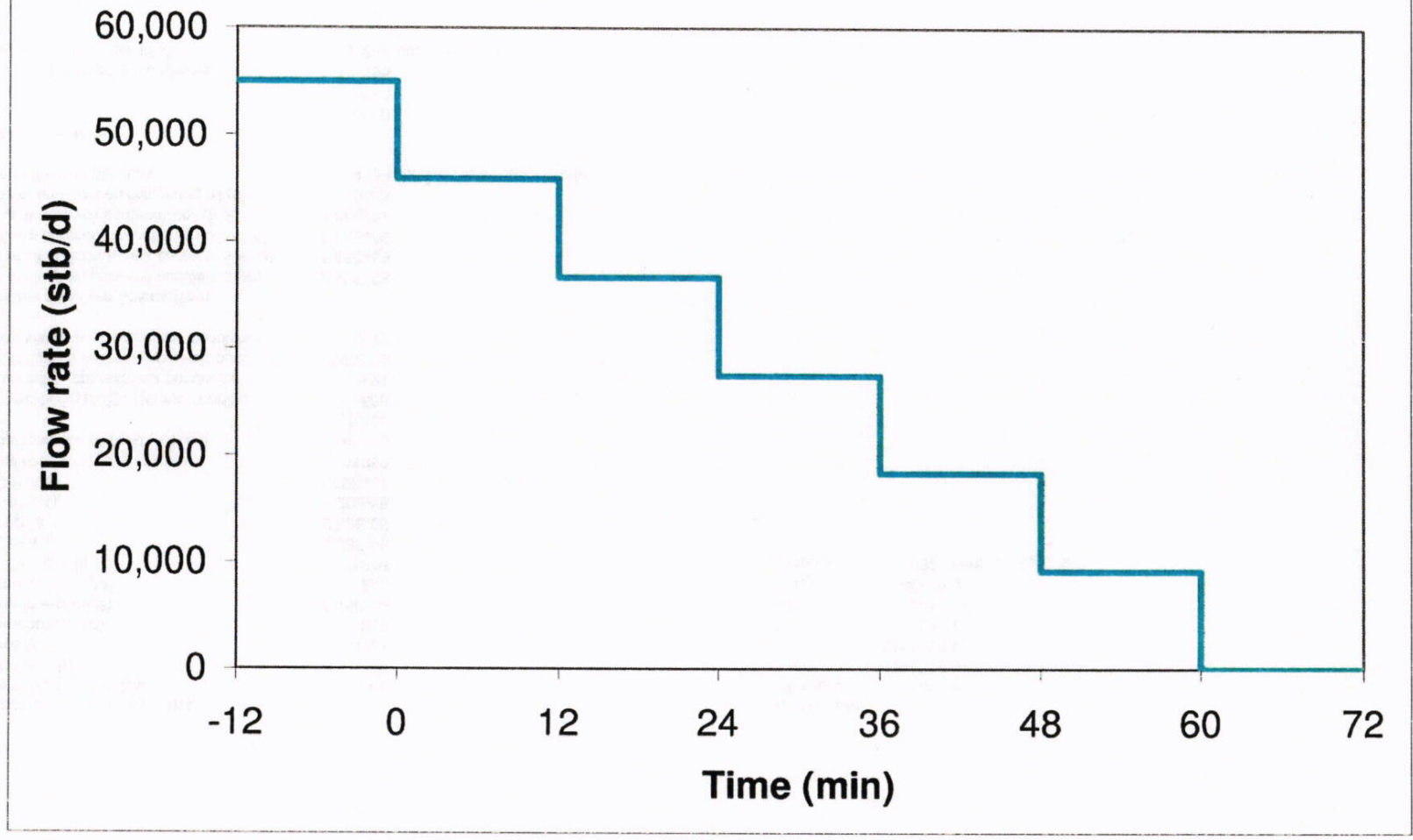


Chart1

	A	B	C	D	E	F	G	H
1	Reservoir + Fluid Properties					Conversion		
2	depth to top (ft TVDSS)	18000				1 barrel =	5.615	ft ³
3	thickness (ft)	93				1 md =	9.87E-16	m ²
4	porosity	0.21				1 cp =	1.00E-03	kg/m/s
5	permeability (md)	219				1 m =	3.281	ft
6	permeability (m ²)	2.16E-13				1 ft =	0.3048	m
7	temperature deg F	243				1 day =	86400	s
8	Oil Boi (rb/stb)	2.345				1 psia =	6894	N/m ² = kg/m/s ²
9	cf (psia-1)	1.20E-05						
10	cw (psia-1)	3.00E-06						
11	co (psia-1)	1.20E-05						
12	OOIP (stb)	1.10E+08						
13	initial reservoir pressure (psi)	11850						
14	initial reservoir oil head (ft of oil)	48153						
15	Sw	0.100						
16	oil density (kg/m ³) reservoir conditions	568						
17	oil viscosity (cp) reservoir conditions	0.21						
18	water density (kg/m ³) reservoir conditions	1000.00						
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20								
21	Volume and Area Calculations							
22	vol of oil under reservoir conditions (rb)	2.58E+08						
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26	Side of square area containing oil (ft)	9078						
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29	Production Rate							
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35								
36	Hydraulic conductivity (oil)							
37	(m/s)	5.73E-06	=rho*g*k/mu					
38	(ft/d)	1.62						
39								
40	Hydraulic conductivity (water)							
41	(m/s)	7.85E-06						
42	(ft/d)	2.22						
43								
44	Specific Storage (oil)							
45	total compressibility (psia-1)	2.31E-05	=(1-Sw)co + Sw*cw + cf					
46	total compressibility (m ² /kg)	3.35E-09						
47	Ss (m-1)	3.53E-06						
48	Ss (ft-1)	1.07E-06						

Flow Rate during Shut in process



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TREX 008639.0037

Reservoir + Fluid Properties

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permeability (m ²)	2.16E-13
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Oil Boi (rb/stb)	2.345
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Hydraulic conductivity (oil)

(m/s)	5.73E-06 =rho*g*k/mu
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Conversion

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1 md =	9.87E-16 m ²
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1 psia =	6894 N/m ² = kg/m/s ²

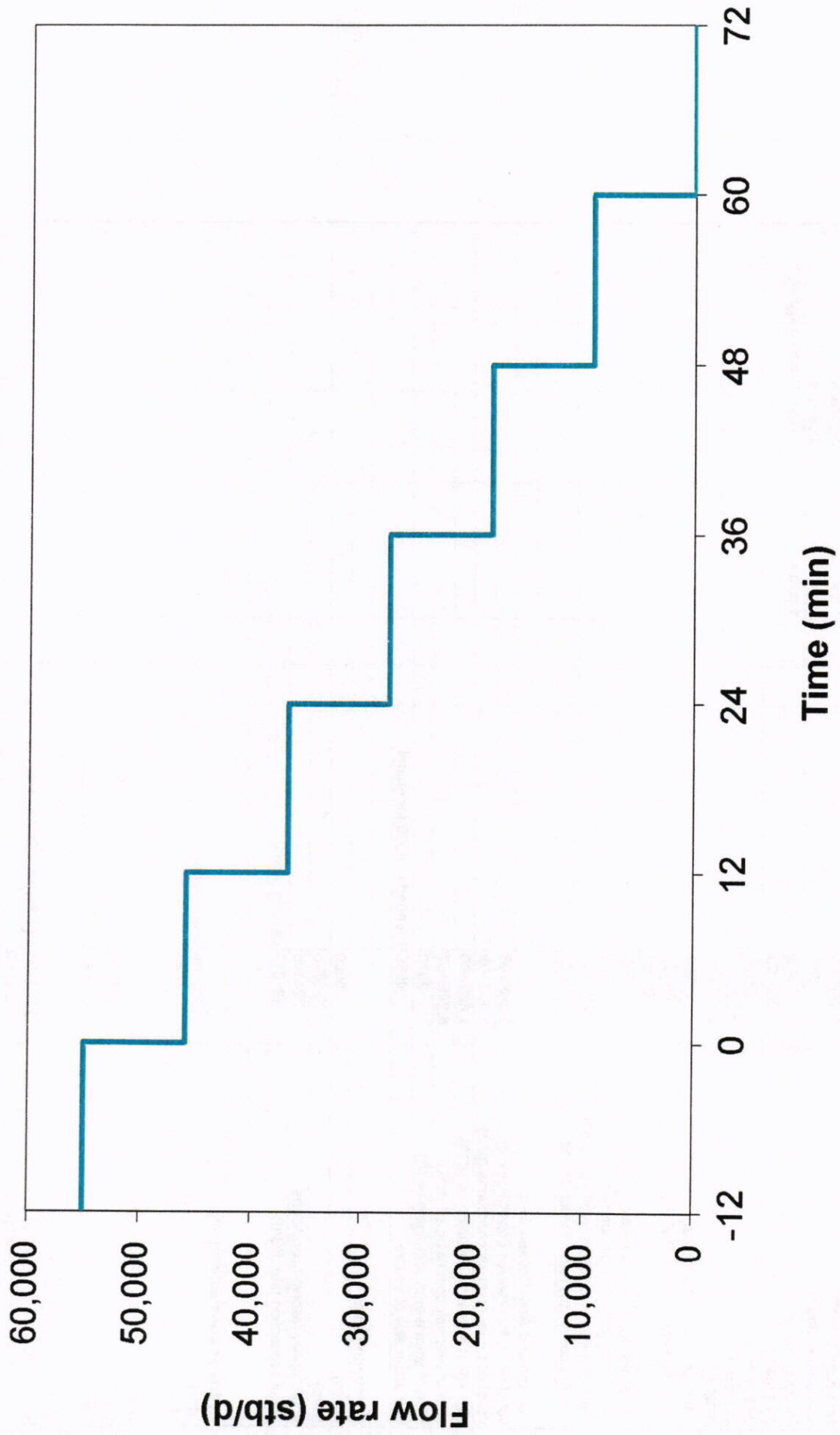
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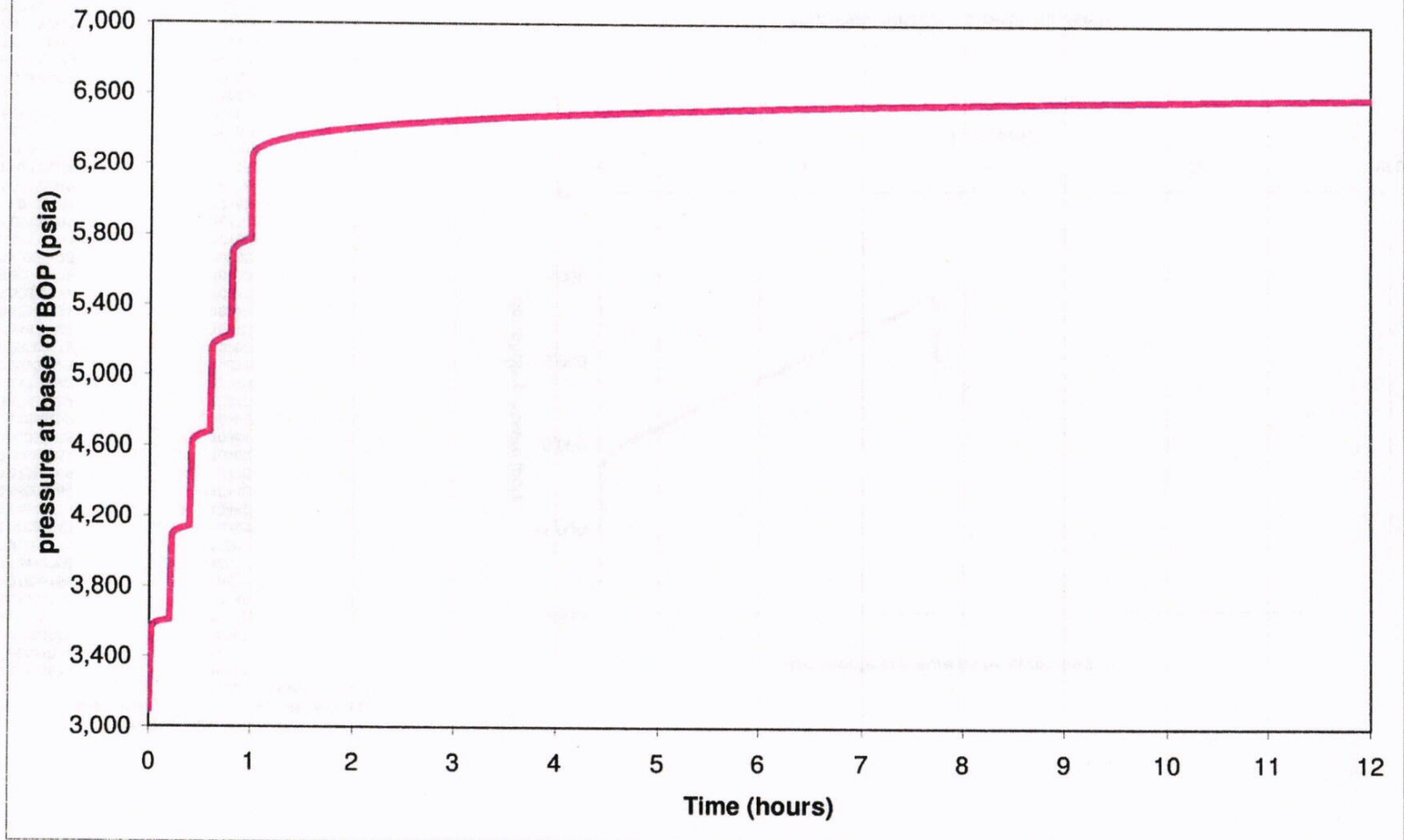
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47	Ss (m-1)	3.53E-06						
48	Ss (ft-1)	1.07E-06						

Pressure at BOP

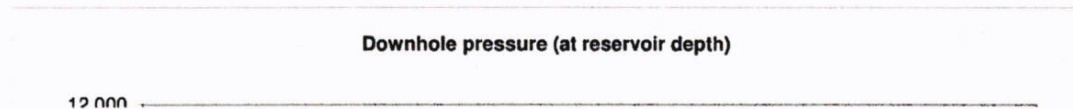
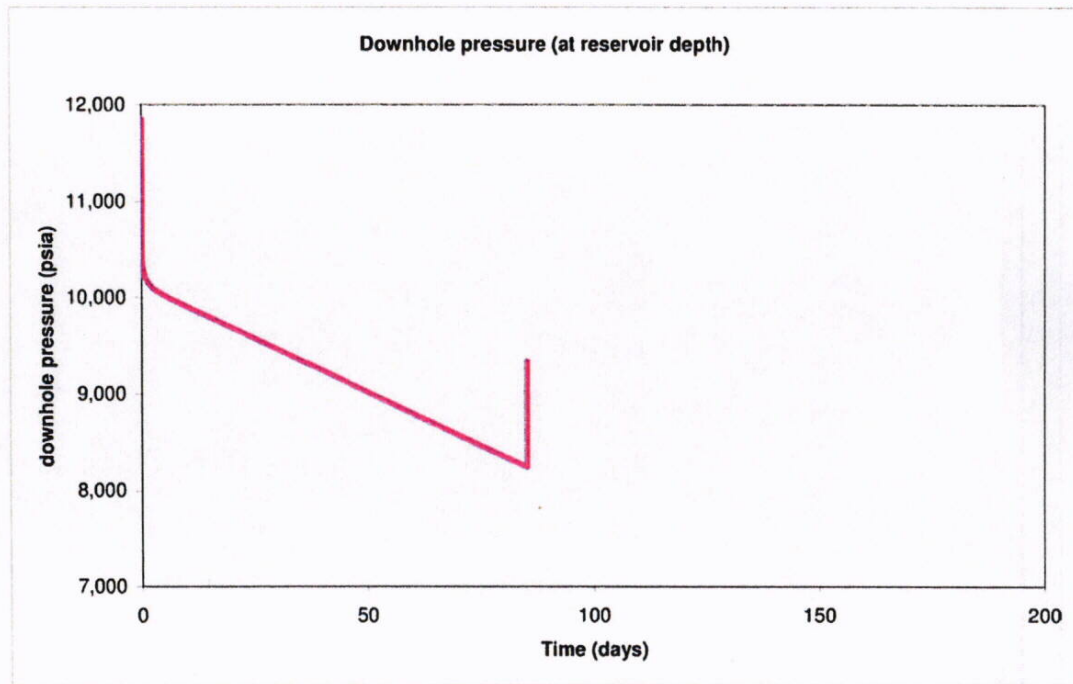


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TREX 008639.0043

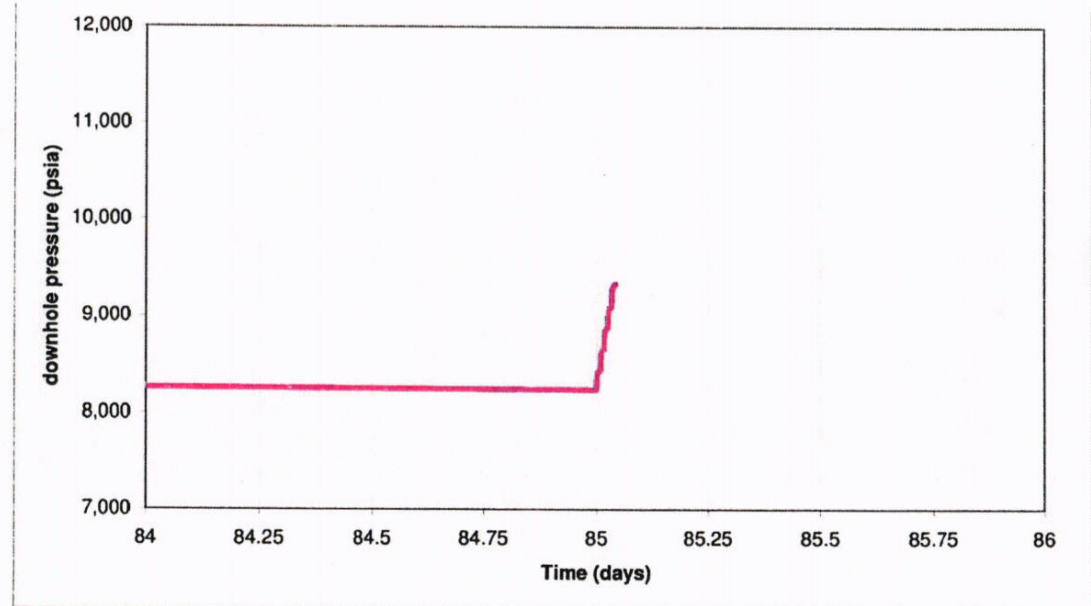
days	down hole pressure		
	days	aq = 0x	aq = 4x aq = 14x
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70.83176422		8554
84.99998474	0	8241
85.00081635	0.02	8399
85.00164795	0.04	8415
85.00247955	0.06	8423
85.00331116	0.08	8429
85.00414276	0.10	8432
85.00497437	0.12	8436
85.00580597	0.14	8438
85.00663757	0.16	8441
85.00746918	0.18	8443
85.00830078	0.20	8444
85.00913239	0.22	8605
85.00996399	0.24	8622
85.01079559	0.26	8631
85.0116272	0.28	8638
85.0124588	0.30	8643
85.01329041	0.32	8647
85.01412201	0.34	8651
85.01495361	0.36	8654
85.01578522	0.38	8657
85.01661682	0.40	8659
85.01744843	0.42	8820
85.01828003	0.44	8838
85.01911163	0.46	8848
85.01994324	0.48	8856
85.02077484	0.50	8861
85.02160645	0.52	8866
85.02243805	0.54	8870
85.02326965	0.56	8874
85.02410126	0.58	8878
85.02493286	0.60	8881
85.02576447	0.62	9042



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TREX 008639.0045

85.02659607	0.64	9061
85.02742767	0.66	9071
85.02825928	0.68	9079
85.02909088	0.70	9085
85.02992249	0.72	9091
85.03075409	0.74	9095
85.03158569	0.76	9100
85.0324173	0.78	9103
85.0332489	0.80	9107
85.03408051	0.82	9269
85.03491211	0.84	9288
85.03574371	0.86	9299
85.03657532	0.88	9307
85.03740692	0.90	9313
85.03823853	0.92	9319
85.03907013	0.94	9324
85.03990173	0.96	9329
85.04073334	0.98	9333
85.04156494	1.00	9337
85.04158783		9438
85.04161072		9455
85.04164124		9465
85.04167938		9472
85.04172516		9478
85.04177856		9483
85.04184723		9487
85.04192352		9492
85.04201508		9496
85.04212952		9500
85.04226685		9504
85.04242706		9508
85.04262543		9512
85.04286194		9516
85.04314423		9521
85.04347992		9525
85.04388428		9530
85.04437256		9535
85.04496002		9540
85.04566193		9545
85.04650116		9551
85.04751587		9557
85.04872894		9564

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TREX 008639.0046

85.05018616	9571
85.05193329	9578
85.05403137	9586
85.05654907	9595
85.05957031	9604
85.06319427	9613
85.06754303	9623
85.07276154	9634
85.07902527	9645
85.08654022	9657
85.09555817	9669
85.10637665	9682
85.11936188	9695
85.1349411	9709
85.15363312	9723
85.17606354	9737
85.20298767	9751
85.23529053	9766
85.27405548	9781
85.3205719	9795
85.37639618	9810
85.44338226	9825
85.52376556	9839
85.620224	9854
85.73597717	9868
85.87487793	9881
86.04156494	9894
85.67682648	9864
85.6872406	9865
85.69765472	9867
85.70806885	9868
85.71848297	9869
85.72889709	9870
85.73931122	9871
85.74972534	9872
85.76013947	9874
85.77055359	9875
85.78096771	9876
85.79138184	9877
85.80179596	9878
85.81221008	9879
85.82262421	9880

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TREX 008639.0047

85.83303833	9881
85.84345245	9882
85.85386658	9883
85.8642807	9884
85.87469482	9885
85.88510895	9886
85.89552307	9887
85.90593719	9887
85.91635132	9888
85.92676544	9889
85.93717957	9890
85.94759369	9891
85.95800781	9892
85.96842194	9892
85.97883606	9893
85.98925018	9894
85.99966431	9895
86.01007843	9896
86.02049255	9896
86.03090668	9897
86.0413208	9898

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IGS075-018244

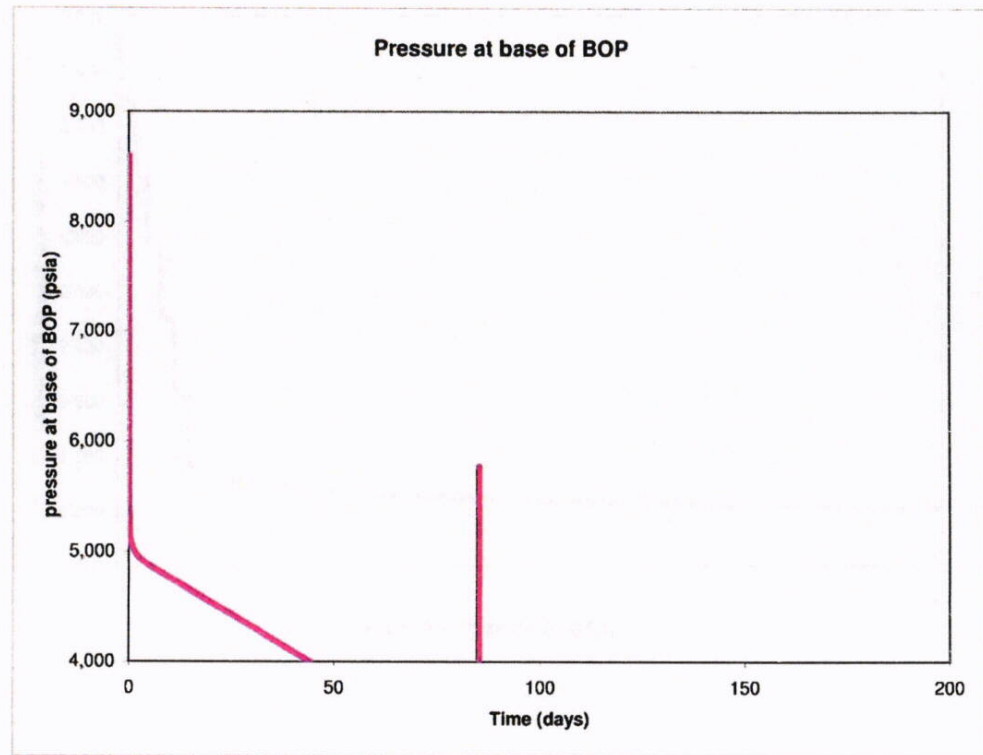
TREX 008639.0048

days	days	pressure at base of BOP aq = 0x	aq = 4x	aq = 14x
	0		8600	6700
0.00186824			5671	
0.00411014			5567	
0.00680041			5510	
0.01002873			5468	
0.01390272			5435	
0.01855151			5406	
0.02413006			5380	
0.03082432			5356	
0.03885743			5333	
0.04849716			5312	
0.06006484			5292	
0.07394605			5272	
0.09060351			5253	
0.11059245			5234	
0.1345792			5215	
0.16336329			5197	
0.1979042			5179	
0.23935328			5161	
0.28909218			5143	
0.34877887			5125	
0.42040291			5108	
0.50635177			5090	
0.60949039			5073	
0.73325676			5055	
0.88177639			5038	
1.05999994			5021	
1.2738682			5003	
1.53051019			4986	
1.83848059			4969	
2.20804501			4951	
2.6515224			4933	
3.18369508			4915	
3.82230258			4896	
4.58863163			4875	
5.50822639			4852	

rho_o = 568

dP = 3250

well loss = 1900

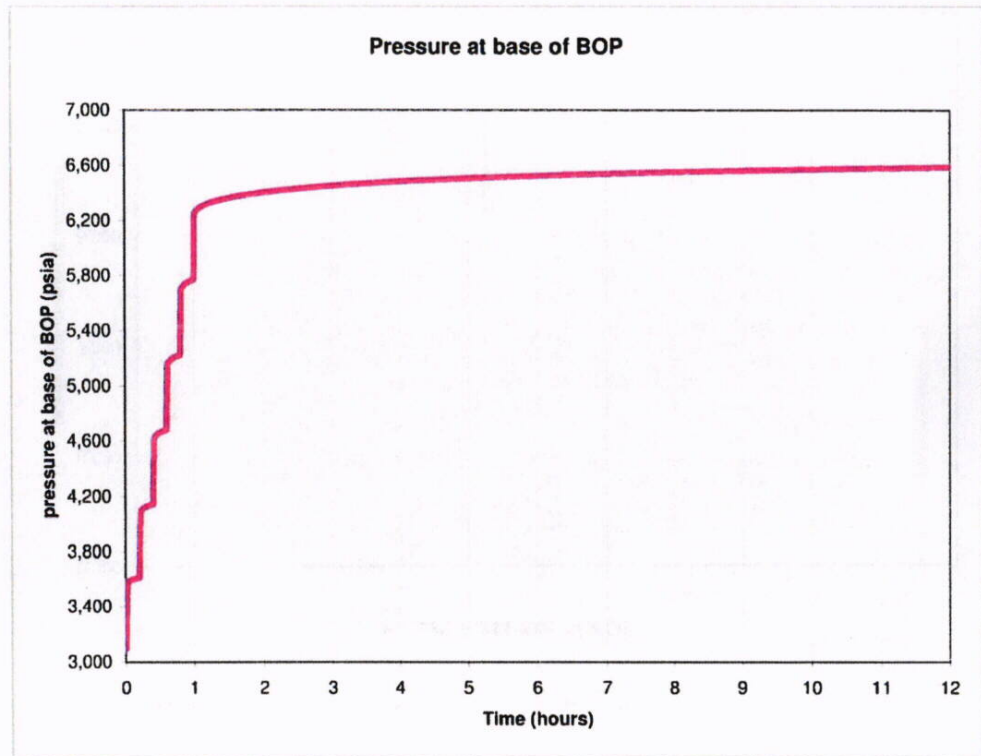


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TREX 008639.0049

6.61174011		4826	
7.93595648		4796	
9.52501678		4760	
11.43188858		4718	
13.72013474		4667	
16.46603012		4606	
19.76110458		4533	
23.7151947		4446	
28.46010399		4341	
34.15399551		4215	
40.98666382		4064	
49.18586731		3883	
59.02490997		3665	
70.83176422		3404	
84.99998474	0	3091	
85.00081635	0.02	3566	0
85.00164795	0.04	3582	0
85.00247955	0.06	3590	0
85.00331116	0.08	3596	0
85.00414276	0.10	3599	0
85.00497437	0.12	3603	0
85.00580597	0.14	3605	0
85.00663757	0.16	3608	0
85.00746918	0.18	3610	0
85.00830078	0.20	3611	0
85.00913239	0.22	4088	0
85.00996399	0.24	4105	0
85.01079559	0.26	4114	0
85.0116272	0.28	4121	0
85.0124588	0.30	4126	0
85.01329041	0.32	4130	0
85.01412201	0.34	4134	0
85.01495361	0.36	4137	0
85.01578522	0.38	4140	0
85.01661682	0.40	4142	0
85.01744843	0.42	4620	0
85.01828003	0.44	4638	0
85.01911163	0.46	4648	0

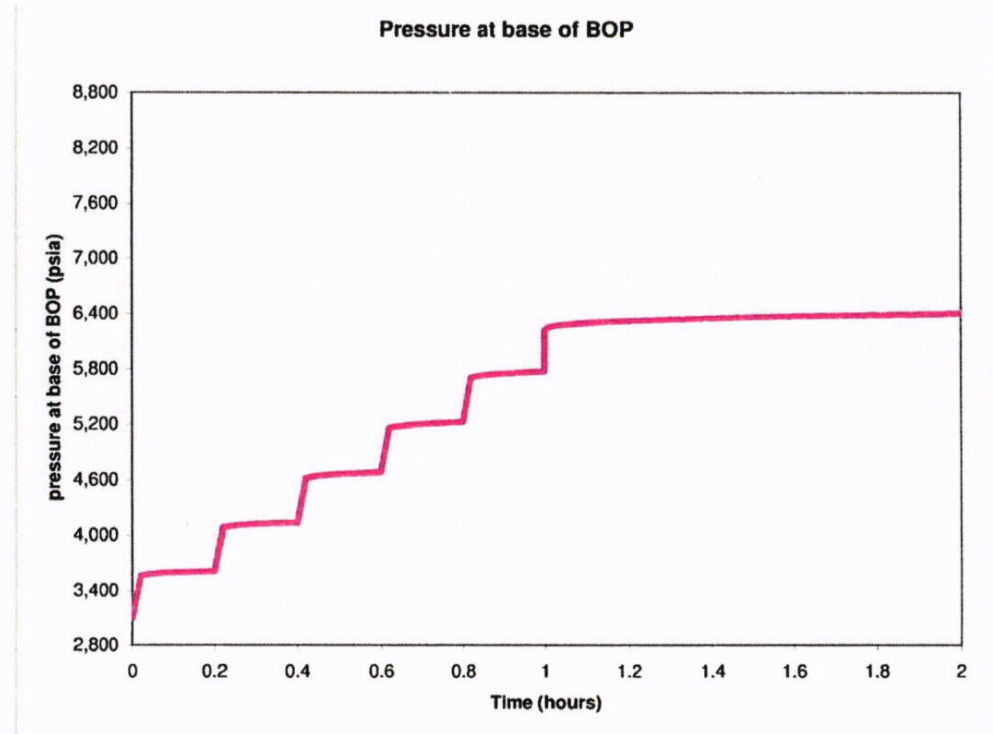


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IGS075-018246

TREX 008639.0050

85.01994324	0.48	4656
85.02077484	0.50	4661
85.02160645	0.52	4666
85.02243805	0.54	4670
85.02326965	0.56	4674
85.02410126	0.58	4678
85.02493286	0.60	4681
85.02576447	0.62	5159
85.02659607	0.64	5178
85.02742767	0.66	5188
85.02825928	0.68	5196
85.02909088	0.70	5202
85.02992249	0.72	5208
85.03075409	0.74	5212
85.03158569	0.76	5217
85.0324173	0.78	5220
85.0332489	0.80	5224
85.03408051	0.82	5702
85.03491211	0.84	5721
85.03574371	0.86	5732
85.03657532	0.88	5740
85.03740692	0.90	5746
85.03823853	0.92	5752
85.03907013	0.94	5757
85.03990173	0.96	5762
85.04073334	0.98	5766
85.04156494	1.00	5770
85.04158783	1.00	6188
85.04161072	1.00	6205
85.04164124	1.00	6215
85.04167938	1.00	6222
85.04172516	1.00	6228
85.04177856	1.00	6233
85.04184723	1.00	6237
85.04192352	1.01	6242
85.04201508	1.01	6246
85.04212952	1.01	6250
85.04226685	1.01	6254



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TREX 008639.0051

85.04242706	1.02	6258
85.04262543	1.02	6262
85.04286194	1.03	6266
85.04314423	1.04	6271
85.04347992	1.04	6275
85.04388428	1.05	6280
85.04437256	1.07	6285
85.04496002	1.08	6290
85.04566193	1.10	6295
85.04650116	1.12	6301
85.04751587	1.14	6307
85.04872894	1.17	6314
85.05018616	1.20	6321
85.05193329	1.25	6328
85.05403137	1.30	6336
85.05654907	1.36	6345
85.05957031	1.43	6354
85.06319427	1.52	6363
85.06754303	1.62	6373
85.07276154	1.75	6384
85.07902527	1.90	6395
85.08654022	2.08	6407
85.09555817	2.29	6419
85.10637665	2.55	6432
85.11936188	2.87	6445
85.1349411	3.24	6459
85.15363312	3.69	6473
85.17606354	4.23	6487
85.20298767	4.87	6501
85.23529053	5.65	6516
85.27405548	6.58	6531
85.3205719	7.69	6545
85.37639618	9.03	6560
85.44338226	10.64	6575
85.52376556	12.57	6589
85.620224	14.89	6604
85.73597717	17.66	6618
85.87487793	21.00	6631

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TREX 008639.0052

86.04156494	25.00	6644
85.67682648	16.24	6614
85.6872406	16.49	6615
85.69765472	16.74	6617
85.70806885	16.99	6618
85.71848297	17.24	6619
85.72889709	17.49	6620
85.73931122	17.74	6621
85.74972534	17.99	6622
85.76013947	18.24	6624
85.77055359	18.49	6625
85.78096771	18.74	6626
85.79138184	18.99	6627
85.80179596	19.24	6628
85.81221008	19.49	6629
85.82262421	19.74	6630
85.83303833	19.99	6631
85.84345245	20.24	6632
85.85386658	20.49	6633
85.8642807	20.74	6634
85.87469482	20.99	6635
85.88510895	21.24	6636
85.89552307	21.49	6637
85.90593719	21.74	6637
85.91635132	21.99	6638
85.92676544	22.24	6639
85.93717957	22.49	6640
85.94759369	22.74	6641
85.95800781	22.99	6642
85.96842194	23.24	6642
85.97883606	23.49	6643
85.98925018	23.74	6644
85.99966431	23.99	6645
86.01007843	24.24	6646
86.02049255	24.49	6646
86.03090668	24.74	6647
86.0413208	24.99	6648

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TREX 008639.0053

Pressure at BOP

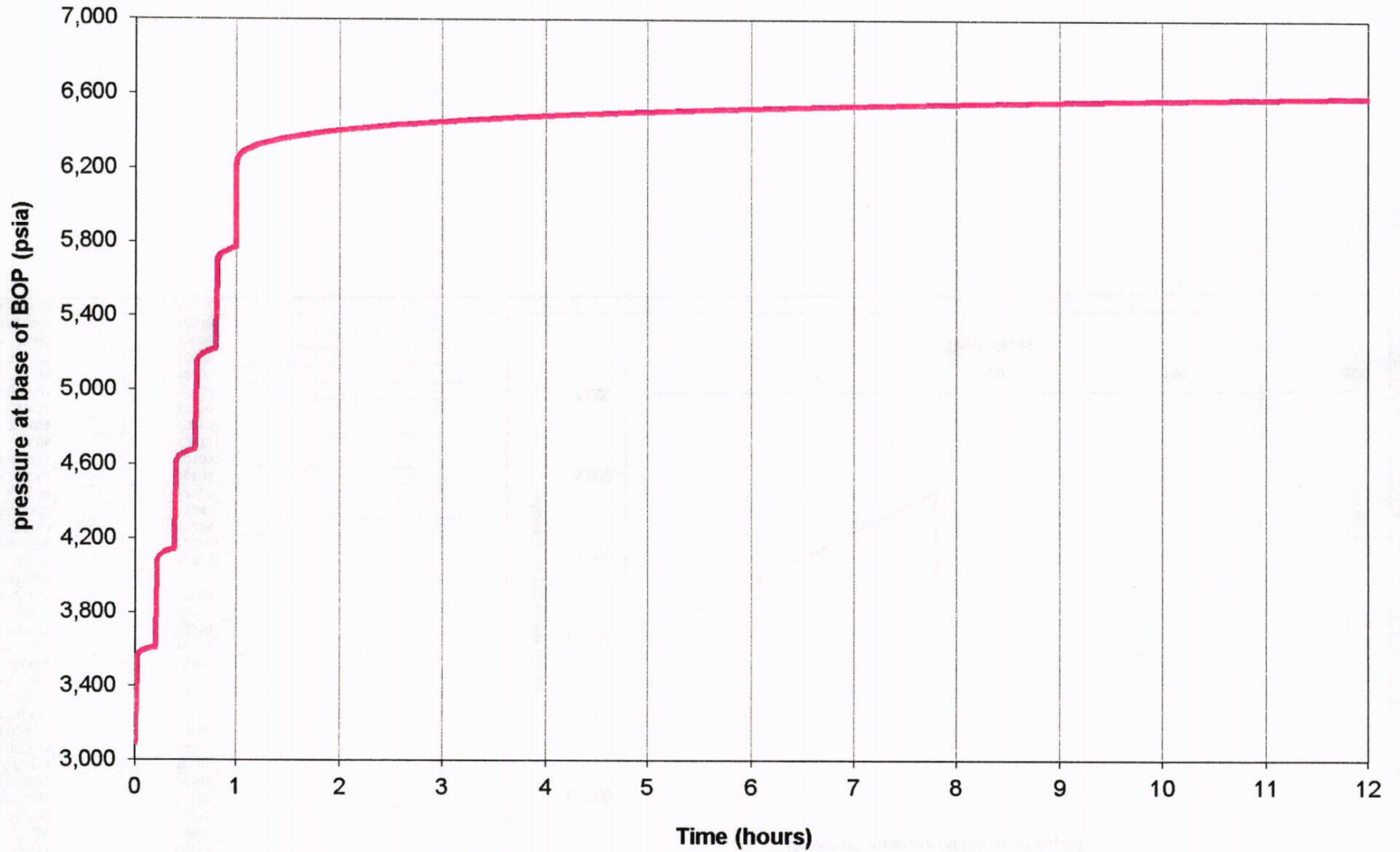
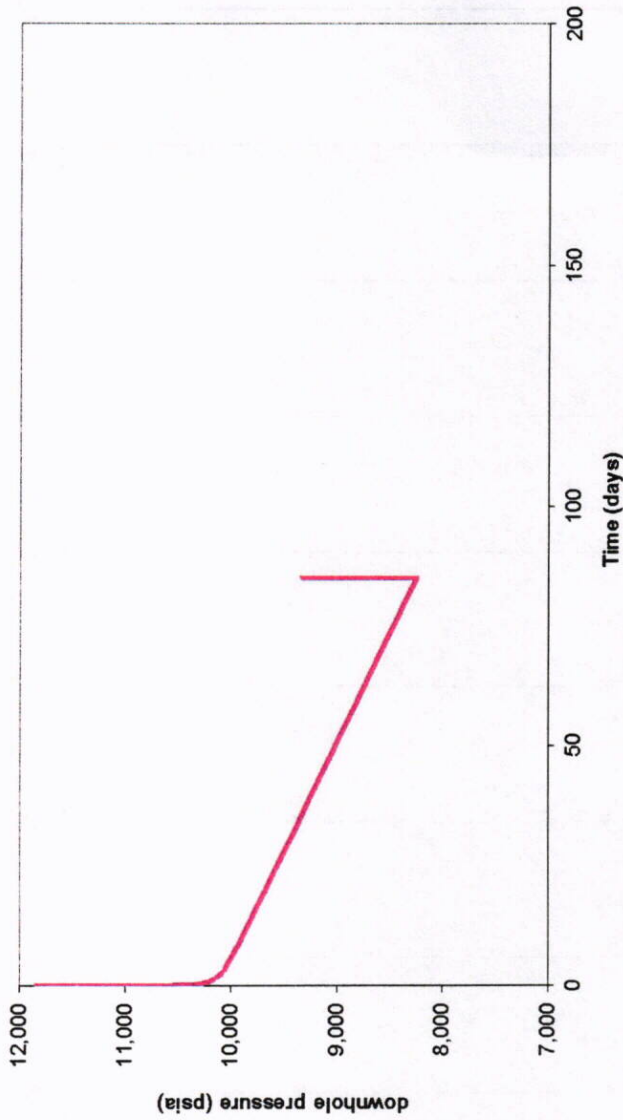


Chart1

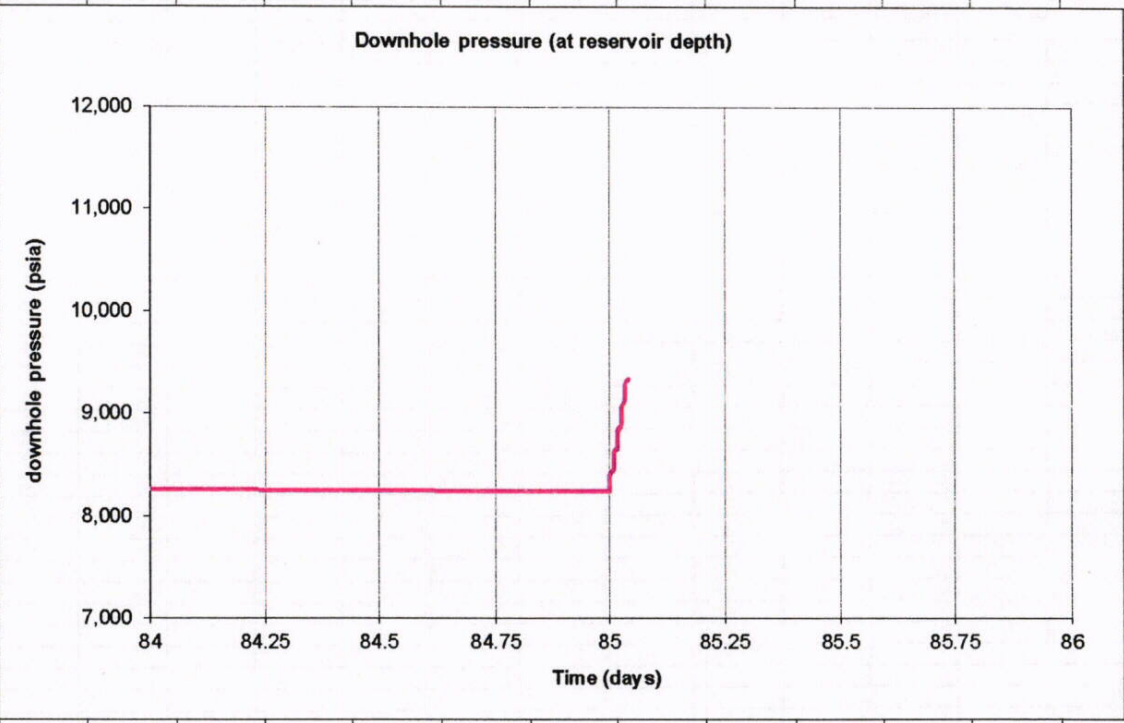
	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	
1																				
2	days		down hole pressure																	
3		days	eq = 0x	eq = 4x	eq = 14x															
4	0.001968		11850	11850	11850															
5	0.00411		10821																	
6	0.0068		10717																	
7	0.010029		10660																	
8	0.013903		10618																	
9	0.018552		10585																	
10	0.02413		10566																	
11	0.030824		10530																	
12	0.038957		10506																	
13	0.048497		10483																	
14	0.060065		10462																	
15	0.073946		10442																	
16	0.090604		10422																	
17	0.110592		10403																	
18	0.134579		10384																	
19	0.163363		10365																	
20	0.197904		10347																	
21	0.239353		10329																	
22	0.289092		10311																	
23	0.348779		10293																	
24	0.420403		10275																	
25	0.506352		10258																	
26	0.60949		10240																	
27	0.733257		10223																	
28	0.881776		10205																	
29	1.06		10188																	
30	1.273968		10171																	
31	1.53051		10153																	
32	1.838481		10136																	
33	2.208045		10119																	
34	2.651522		10101																	
35	3.183695		10083																	
36	3.822303		10065																	
37	4.588632		10046																	
			10025																	

Downhole pressure (at reservoir depth)



downhole pressure

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	
1			down hole pressure																	
2	days	days	aq = 0x	aq = 4x	aq = 14x															
38	5.508226		10002																	
39	6.61174		9976																	
40	7.935956		9946																	
41	9.525017		9910																	
42	11.43189		9868																	
43	13.72013		9817																	
44	16.46603		9756																	
45	19.7611		9683																	
46	23.71519		9596																	
47	28.4601		9491																	
48	34.154		9365																	
49	40.98666		9214																	
50	49.18587		9033																	
51	59.02491		8815																	
52	70.83176		8554																	
53	84.99998	0	8241																	
54	85.00082	0.02	8399																	
55	85.00165	0.04	8415																	
56	85.00248	0.06	8423																	
57	85.00331	0.08	8429																	
58	85.00414	0.10	8432																	
59	85.00497	0.12	8436																	
60	85.00581	0.14	8438																	
61	85.00664	0.16	8441																	
62	85.00747	0.18	8443																	
63	85.0083	0.20	8444																	
64	85.00913	0.22	8605																	
65	85.00996	0.24	8622																	
66	85.0108	0.26	8631																	
67	85.01163	0.28	8638																	
68	85.01246	0.30	8643																	
69	85.01329	0.32	8647																	
70	85.01412	0.34	8651																	
71	85.01495	0.36	8654																	
72	85.01579	0.38	8657																	
73	85.01662	0.40	8659																	
74	85.01745	0.42	8820																	
75	85.01828	0.44	8838																	
76	85.01911	0.46	8848																	
77	85.01994	0.48	8856																	
78	85.02077	0.50	8861																	
79	85.02161	0.52	8866																	
80	85.02244	0.54	8870																	
81	85.02327	0.56	8874																	
82	85.0241	0.58	8878																	
83	85.02493	0.60	8881																	
84	85.02576	0.62	9042																	
85	85.0266	0.64	9061																	
86	85.02743	0.66	9071																	
87	85.02826	0.68	9079																	
88	85.02909	0.70	9085																	
89	85.02992	0.72	9091																	
90	85.03075	0.74	9095																	
91	85.03159	0.76	9100																	



	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
1																			
2	days	days	down hole pressure eq = 0x	eq = 4x	eq = 14x														
92	85.03242	0.78	9103																
93	85.03325	0.80	9107																
94	85.03408	0.82	9269																
95	85.03491	0.84	9288																
96	85.03574	0.86	9299																
97	85.03658	0.88	9307																
98	85.03741	0.90	9313																
99	85.03824	0.92	9319																
100	85.03907	0.94	9324																
101	85.03999	0.96	9329																
102	85.04073	0.98	9333																
103	85.04156	1.00	9337																
104	85.04159		9438																
105	85.04161		9455																
106	85.04164		9465																
107	85.04168		9472																
108	85.04173		9478																
109	85.04178		9483																
110	85.04185		9487																
111	85.04192		9482																
112	85.04202		9496																
113	85.04213		9500																
114	85.04227		9504																
115	85.04243		9508																
116	85.04263		9512																
117	85.04286		9516																
118	85.04314		9521																
119	85.04348		9525																
120	85.04388		9530																
121	85.04437		9535																
122	85.04496		9540																
123	85.04566		9545																
124	85.04665		9551																
125	85.04752		9557																
126	85.04873		9564																
127	85.05019		9571																
128	85.05193		9578																
129	85.05403		9586																
130	85.05665		9595																
131	85.05957		9604																
132	85.06319		9613																
133	85.06754		9623																
134	85.07276		9634																
135	85.07903		9645																
136	85.08654		9657																
137	85.09556		9669																
138	85.10638		9682																
139	85.11936		9695																
140	85.13494		9708																
141	85.15363		9723																
142	85.17606		9737																
143	85.20299		9751																
144	85.23529		9766																
145	85.27406		9781																

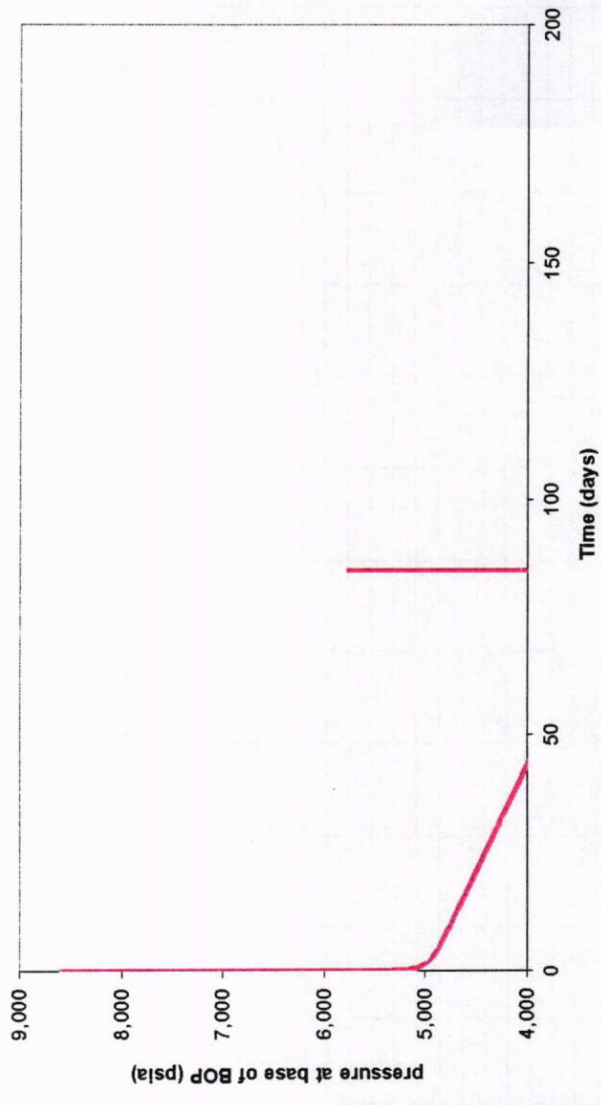
down hole pressure

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	
1																				
2	days	days	down hole pressure	down hole pressure	aq = 14x															
146	85.32057		aq = 0x	aq = 4x																
147	85.3764		9795																	
148	85.44338		9810																	
149	85.52377		9825																	
150	85.62022		9839																	
151	85.73598		9854																	
152	85.87488		9868																	
153	86.04156		9881																	
154	85.67683		9894																	
155	85.68724		9864																	
156	85.68765		9865																	
157	85.70807		9867																	
158	85.71848		9868																	
159	85.7289		9869																	
160	85.73931		9870																	
161	85.74973		9871																	
162	85.76014		9872																	
163	85.77055		9874																	
164	85.78097		9875																	
165	85.79138		9876																	
166	85.8018		9877																	
167	85.81221		9878																	
168	85.82262		9879																	
169	85.83304		9880																	
170	85.84345		9881																	
171	85.85387		9882																	
172	85.86428		9883																	
173	85.87469		9884																	
174	85.88511		9885																	
175	85.89552		9886																	
176	85.90594		9887																	
177	85.91635		9888																	
178	85.92677		9889																	
179	85.93718		9890																	
180	85.94759		9891																	
181	85.95801		9892																	
182	85.96842		9893																	
183	85.97884		9894																	
184	85.98925		9895																	
185	85.99966		9896																	
186	86.01008		9897																	
187	86.02049		9898																	
188	86.03091		9899																	
189	86.04132		9898																	

downhole pressure

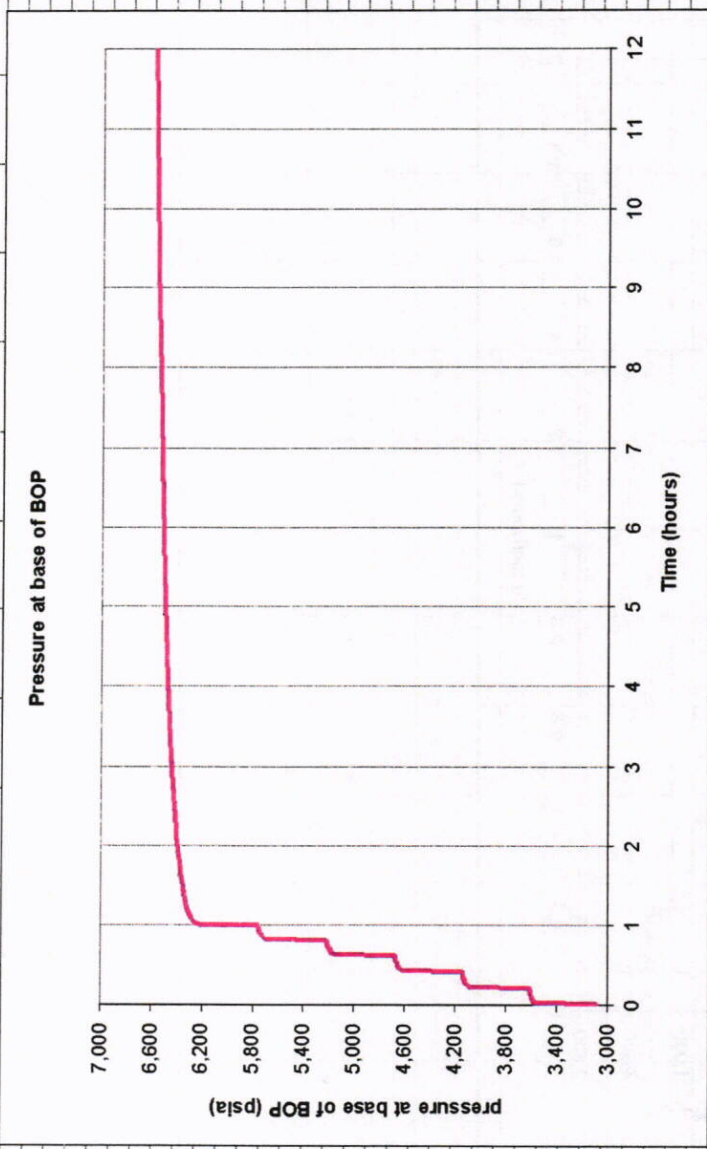
	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
1																			
2	days	days	pressure at base of BOP aq = 0x	pressure at base of BOP aq = 4x	aq = 14x 6700			rho_o =	568		dP =	3250		well loss =	1900				
3	0		8600																
4	0.001868		5671																
5	0.00411		5567																
6	0.0068		5510																
7	0.010028		5468																
8	0.013903		5435																
9	0.018552		5406																
10	0.02413		5380																
11	0.030824		5356																
12	0.038857		5333																
13	0.048497		5312																
14	0.060085		5292																
15	0.073946		5272																
16	0.090604		5253																
17	0.110592		5234																
18	0.134579		5215																
19	0.163363		5197																
20	0.197804		5179																
21	0.239353		5161																
22	0.289092		5143																
23	0.348779		5125																
24	0.420403		5108																
25	0.506352		5090																
26	0.60849		5073																
27	0.733257		5055																
28	0.881776		5038																
29	1.06		5021																
30	1.273868		5003																
31	1.53051		4986																
32	1.839481		4969																
33	2.208045		4951																
34	2.651522		4933																
35	3.183695		4915																
36	3.822303		4896																
37	4.589632		4875																

Pressure at base of BOP



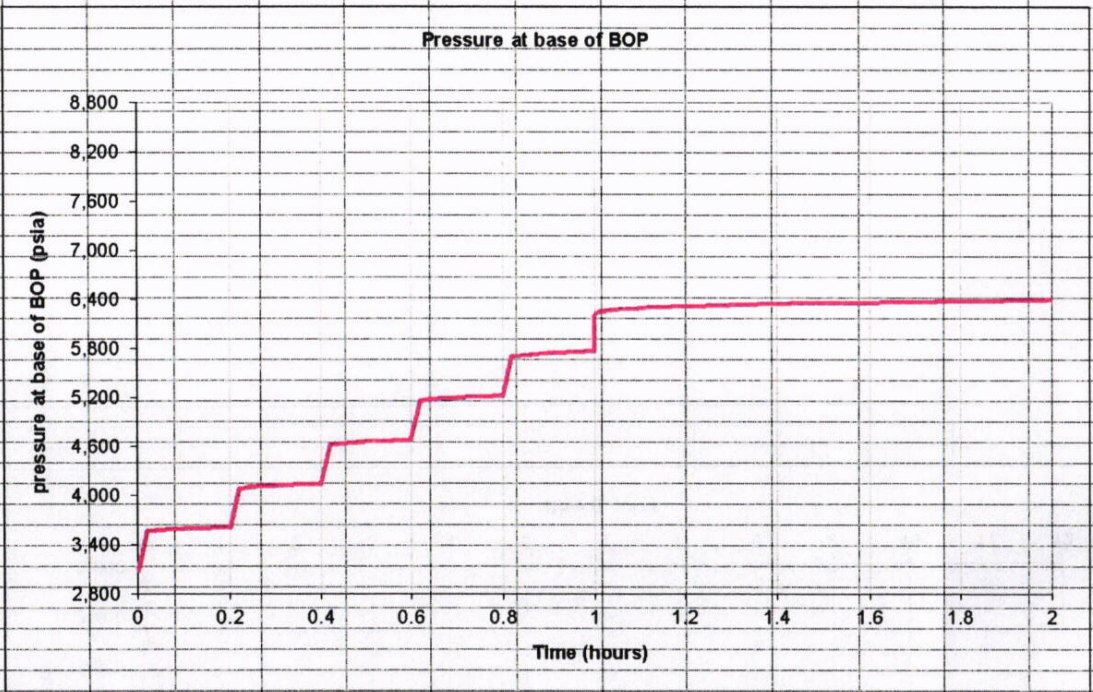
press: 'base of BOP

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	
1																				
2	days	days	pressure at base of BOP aq = 0x	pressure at base of BOP aq = 4x	aq = 14x			rho_o =	568		dP =	3250		well loss =	1900					
38	5.508226		4852																	
39	6.61174		4826																	
40	7.935956		4796																	
41	9.525017		4760																	
42	11.43189		4718																	
43	13.72013		4667																	
44	16.46603		4606																	
45	19.7611		4533																	
46	23.71519		4446																	
47	28.4601		4341																	
48	34.154		4215																	
49	40.98666		4064																	
50	49.18587		3883																	
51	59.02491		3665																	
52	70.83176		3404																	
53	84.99998	0	3091																	
54	85.00082	0.02	3566	0																
55	85.00165	0.04	3582	0																
56	85.00248	0.06	3590	0																
57	85.00331	0.08	3596	0																
58	85.00414	0.10	3599	0																
59	85.00497	0.12	3603	0																
60	85.00581	0.14	3605	0																
61	85.00664	0.16	3608	0																
62	85.00747	0.18	3610	0																
63	85.0083	0.20	3611	0																
64	85.00913	0.22	4088	0																
65	85.00996	0.24	4105	0																
66	85.0108	0.26	4114	0																
67	85.01163	0.28	4121	0																
68	85.01246	0.30	4126	0																
69	85.01329	0.32	4130	0																
70	85.01412	0.34	4134	0																
71	85.01495	0.36	4137	0																
72	85.01579	0.38	4140	0																
73	85.01662	0.40	4142	0																
74	85.01745	0.42	4620	0																



pressure at base of BOP

1	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
2	days	days	pressure at base of BOP aq = 0x	aq = 4x	aq = 14x			rho_o =	568		dP =	3250		well loss =	1900				
75	85.01828	0.44	4638		0														
76	85.01911	0.46	4648		0														
77	85.01994	0.48	4656																
78	85.02077	0.50	4661																
79	85.02161	0.52	4666																
80	85.02244	0.54	4670																
81	85.02327	0.56	4674																
82	85.0241	0.58	4678																
83	85.02493	0.60	4681																
84	85.02576	0.62	5159																
85	85.0266	0.64	5178																
86	85.02743	0.66	5188																
87	85.02826	0.68	5196																
88	85.02909	0.70	5202																
89	85.02992	0.72	5208																
90	85.03075	0.74	5212																
91	85.03159	0.76	5217																
92	85.03242	0.78	5220																
93	85.03325	0.80	5224																
94	85.03408	0.82	5702																
95	85.03491	0.84	5721																
96	85.03574	0.86	5732																
97	85.03658	0.88	5740																
98	85.03741	0.90	5746																
99	85.03824	0.92	5752																
100	85.03907	0.94	5757																
101	85.0399	0.96	5762																
102	85.04073	0.98	5766																
103	85.04156	1.00	5770																
104	85.04159	1.00	6188																
105	85.04161	1.00	6205																
106	85.04164	1.00	6215																
107	85.04168	1.00	6222																
108	85.04173	1.00	6228																
109	85.04178	1.00	6233																
110	85.04185	1.00	6237																
111	85.04192	1.01	6242																
112	85.04202	1.01	6246																
113	85.04213	1.01	6250																
114	85.04227	1.01	6254																
115	85.04243	1.02	6258																
116	85.04263	1.02	6262																
117	85.04286	1.03	6266																
118	85.04314	1.04	6271																
119	85.04348	1.04	6275																
120	85.04388	1.05	6280																
121	85.04437	1.07	6285																
122	85.04496	1.08	6290																



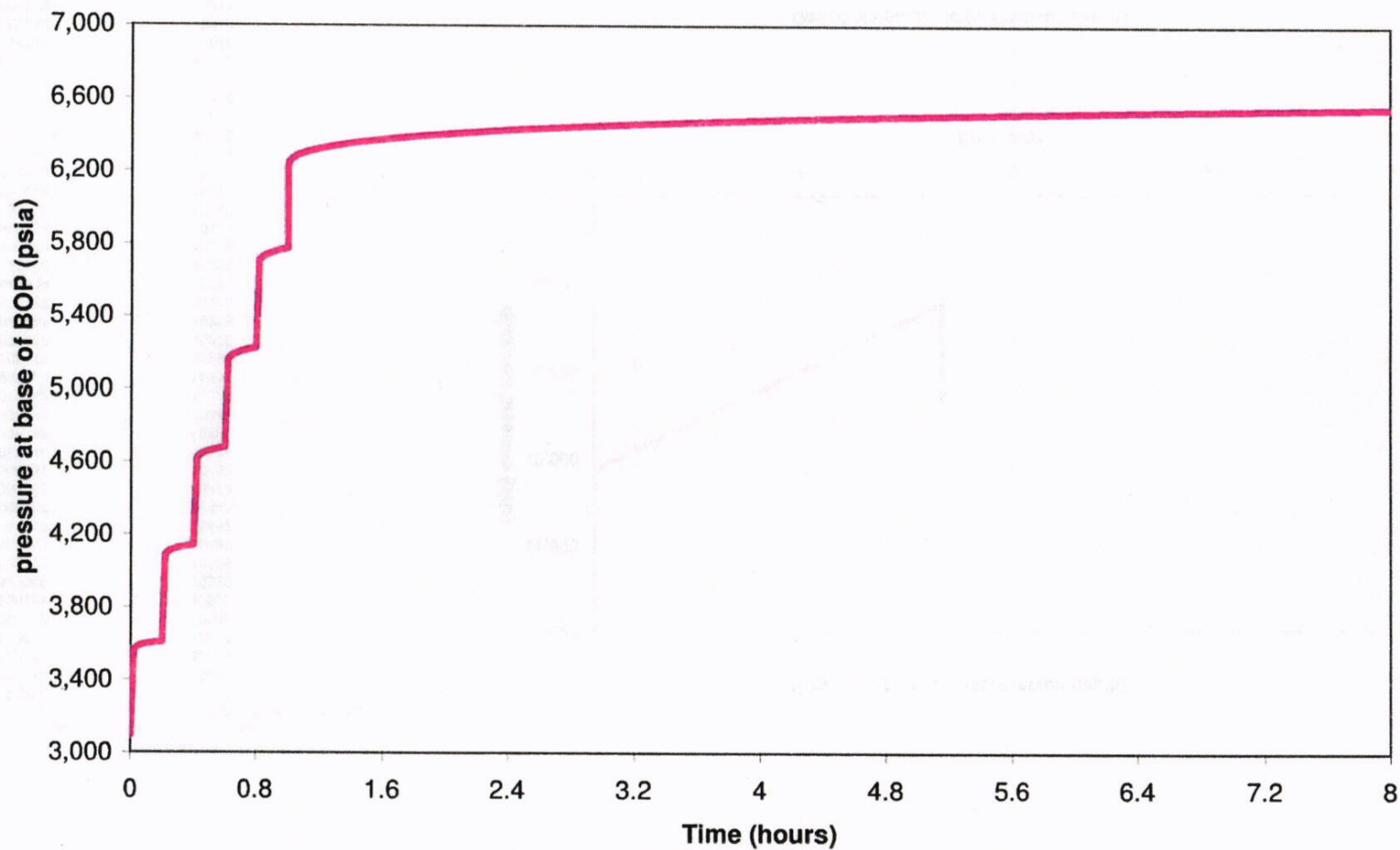
press' base of BOP

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	
1																				
2	days	days	pressure at base of BOP aq = 0x	aq = 4x	aq = 14x			rho_o =	568	dP =	3250			well loss =	1900					
123	85.04566	1.10	6295																	
124	85.0465	1.12	6301																	
125	85.04752	1.14	6307																	
126	85.04873	1.17	6314																	
127	85.05019	1.20	6321																	
128	85.05193	1.25	6328																	
129	85.05403	1.30	6336																	
130	85.05655	1.36	6345																	
131	85.05957	1.43	6354																	
132	85.06319	1.52	6363																	
133	85.06754	1.62	6373																	
134	85.07276	1.75	6384																	
135	85.07903	1.90	6395																	
136	85.08654	2.08	6407																	
137	85.09556	2.29	6419																	
138	85.10638	2.55	6432																	
139	85.11936	2.87	6445																	
140	85.13494	3.24	6459																	
141	85.15363	3.69	6473																	
142	85.17606	4.23	6487																	
143	85.20299	4.87	6501																	
144	85.23529	5.65	6516																	
145	85.27406	6.58	6531																	
146	85.32057	7.69	6545																	
147	85.3764	9.03	6560																	
148	85.44338	10.64	6575																	
149	85.52377	12.57	6589																	
150	85.62022	14.89	6604																	
151	85.73598	17.66	6618																	
152	85.87488	21.00	6631																	
153	86.04156	25.00	6644																	
154	85.67683	16.24	6614																	
155	85.68724	16.49	6615																	
156	85.69765	16.74	6617																	
157	85.70807	16.99	6618																	
158	85.71848	17.24	6619																	

1	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
2	days	days	pressure at base of BOP eq = 0x	eq = 4x	eq = 14x			rho_o =	568		dP =	3250		well loss =	1900				
159	85.7289	17.49	6620																
160	85.73931	17.74	6621																
161	85.74973	17.99	6622																
162	85.76014	18.24	6624																
163	85.77055	18.49	6625																
164	85.78097	18.74	6626																
165	85.79138	18.99	6627																
166	85.8018	19.24	6628																
167	85.81221	19.49	6629																
168	85.82262	19.74	6630																
169	85.83304	19.99	6631																
170	85.84345	20.24	6632																
171	85.85387	20.49	6633																
172	85.86428	20.74	6634																
173	85.87469	20.99	6635																
174	85.88511	21.24	6636																
175	85.89552	21.49	6637																
176	85.90594	21.74	6637																
177	85.91635	21.99	6638																
178	85.92677	22.24	6639																
179	85.93718	22.49	6640																
180	85.94759	22.74	6641																
181	85.95801	22.99	6642																
182	85.96842	23.24	6642																
183	85.97884	23.49	6643																
184	85.98925	23.74	6644																
185	85.99966	23.99	6645																
186	86.01008	24.24	6646																
187	86.02049	24.49	6646																
188	86.03091	24.74	6647																
189	86.04132	24.99	6648																

pressur base of BOP

Pressure at base of BOP

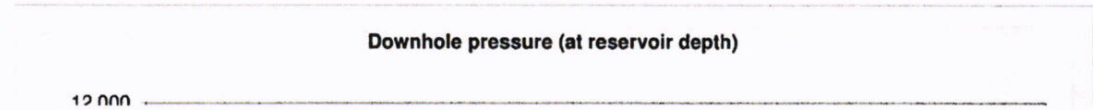
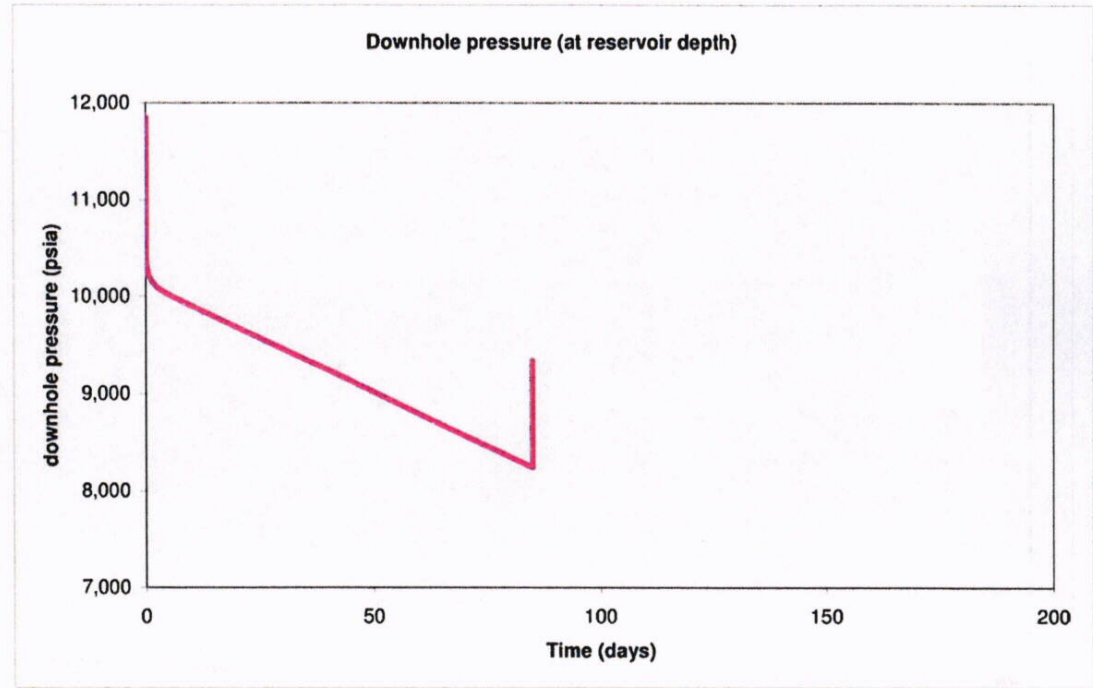


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TREX 008639.0065

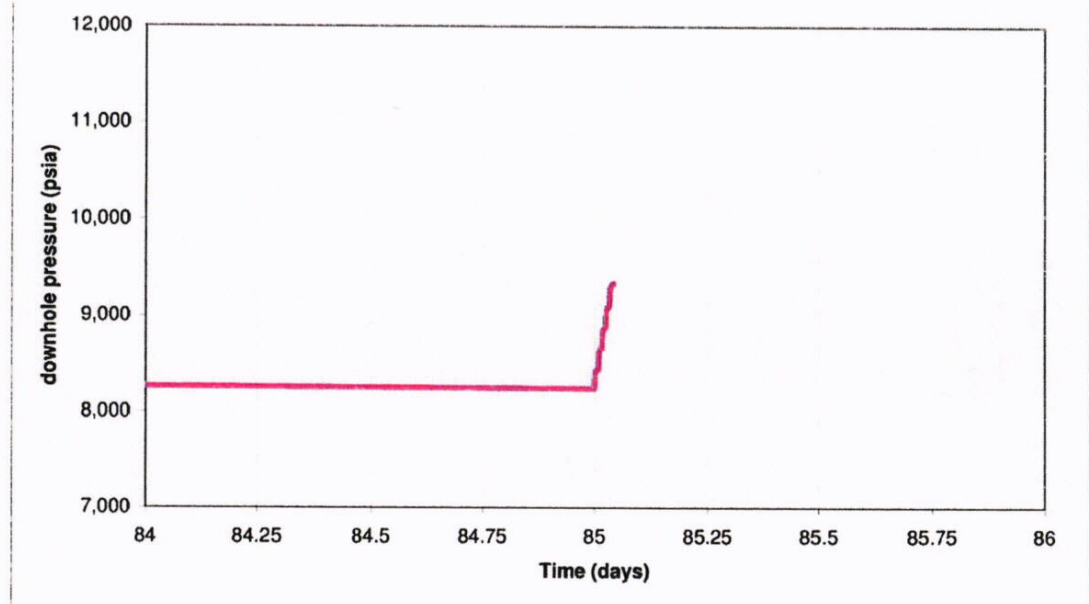
down hole pressure				
days	days	aq = 0x	aq = 4x	aq = 14x
	0		11850	11850
	0.00186824		10821	
	0.00411014		10717	
	0.00680041		10660	
	0.01002873		10618	
	0.01390272		10585	
	0.01855151		10556	
	0.02413006		10530	
	0.03082432		10506	
	0.03885743		10483	
	0.04849716		10462	
	0.06006484		10442	
	0.07394605		10422	
	0.09060351		10403	
	0.11059245		10384	
	0.1345792		10365	
	0.16336329		10347	
	0.1979042		10329	
	0.23935328		10311	
	0.28909218		10293	
	0.34877887		10275	
	0.42040291		10258	
	0.50635177		10240	
	0.60949039		10223	
	0.73325676		10205	
	0.88177639		10188	
	1.05999994		10171	
	1.2738682		10153	
	1.53051019		10136	
	1.83848059		10119	
	2.20804501		10101	
	2.6515224		10083	
	3.18369508		10065	
	3.82230258		10046	
	4.58863163		10025	
	5.50822639		10002	
	6.61174011		9976	
	7.93595648		9946	
	9.52501678		9910	
	11.43188858		9868	



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13.72013474		9817
16.46603012		9756
19.76110458		9683
23.7151947		9596
28.46010399		9491
34.15399551		9365
40.98666382		9214
49.18586731		9033
59.02490997		8815
70.83176422		8554
84.99998474	0	8241
85.00081635	0.02	8399
85.00164795	0.04	8415
85.00247955	0.06	8423
85.00331116	0.08	8429
85.00414276	0.10	8432
85.00497437	0.12	8436
85.00580597	0.14	8438
85.00663757	0.16	8441
85.00746918	0.18	8443
85.00830078	0.20	8444
85.00913239	0.22	8605
85.00996399	0.24	8622
85.01079559	0.26	8631
85.0116272	0.28	8638
85.0124588	0.30	8643
85.01329041	0.32	8647
85.01412201	0.34	8651
85.01495361	0.36	8654
85.01578522	0.38	8657
85.01661682	0.40	8659
85.01744843	0.42	8820
85.01828003	0.44	8838
85.01911163	0.46	8848
85.01994324	0.48	8856
85.02077484	0.50	8861
85.02160645	0.52	8866
85.02243805	0.54	8870
85.02326965	0.56	8874
85.02410126	0.58	8878
85.02493286	0.60	8881
85.02576447	0.62	9042



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TREX 008639.0067

85.02659607	0.64	9061
85.02742767	0.66	9071
85.02825928	0.68	9079
85.02909088	0.70	9085
85.02992249	0.72	9091
85.03075409	0.74	9095
85.03158569	0.76	9100
85.0324173	0.78	9103
85.0332489	0.80	9107
85.03408051	0.82	9269
85.03491211	0.84	9288
85.03574371	0.86	9299
85.03657532	0.88	9307
85.03740692	0.90	9313
85.03823853	0.92	9319
85.03907013	0.94	9324
85.03990173	0.96	9329
85.04073334	0.98	9333
85.04156494	1.00	9337
85.04158783		9438
85.04161072		9455
85.04164124		9465
85.04167938		9472
85.04172516		9478
85.04177856		9483
85.04184723		9487
85.04192352		9492
85.04201508		9496
85.04212952		9500
85.04226685		9504
85.04242706		9508
85.04262543		9512
85.04286194		9516
85.04314423		9521
85.04347992		9525
85.04388428		9530
85.04437256		9535
85.04496002		9540
85.04566193		9545
85.04650116		9551
85.04751587		9557
85.04872894		9564

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TREX 008639.0068

85.05018616	9571
85.05193329	9578
85.05403137	9586
85.05654907	9595
85.05957031	9604
85.06319427	9613
85.06754303	9623
85.07276154	9634
85.07902527	9645
85.08654022	9657
85.09555817	9669
85.10637665	9682
85.11936188	9695
85.1349411	9709
85.15363312	9723
85.17606354	9737
85.20298767	9751
85.23529053	9766
85.27405548	9781
85.3205719	9795
85.37639618	9810
85.44338226	9825
85.52376556	9839
85.620224	9854
85.73597717	9868
85.87487793	9881
86.04156494	9894
85.67682648	9864
85.6872406	9865
85.69765472	9867
85.70806885	9868
85.71848297	9869
85.72889709	9870
85.73931122	9871
85.74972534	9872
85.76013947	9874
85.77055359	9875
85.78096771	9876
85.79138184	9877
85.80179596	9878
85.81221008	9879
85.82262421	9880

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TREX 008639.0069

85.83303833	9881
85.84345245	9882
85.85386658	9883
85.8642807	9884
85.87469482	9885
85.88510895	9886
85.89552307	9887
85.90593719	9888
85.91635132	9889
85.92676544	9890
85.93717957	9891
85.94759369	9892
85.95800781	9893
85.96842194	9894
85.97883606	9895
85.98925018	9896
85.99966431	9897
86.01007843	9898
86.02049255	
86.03090668	
86.0413208	

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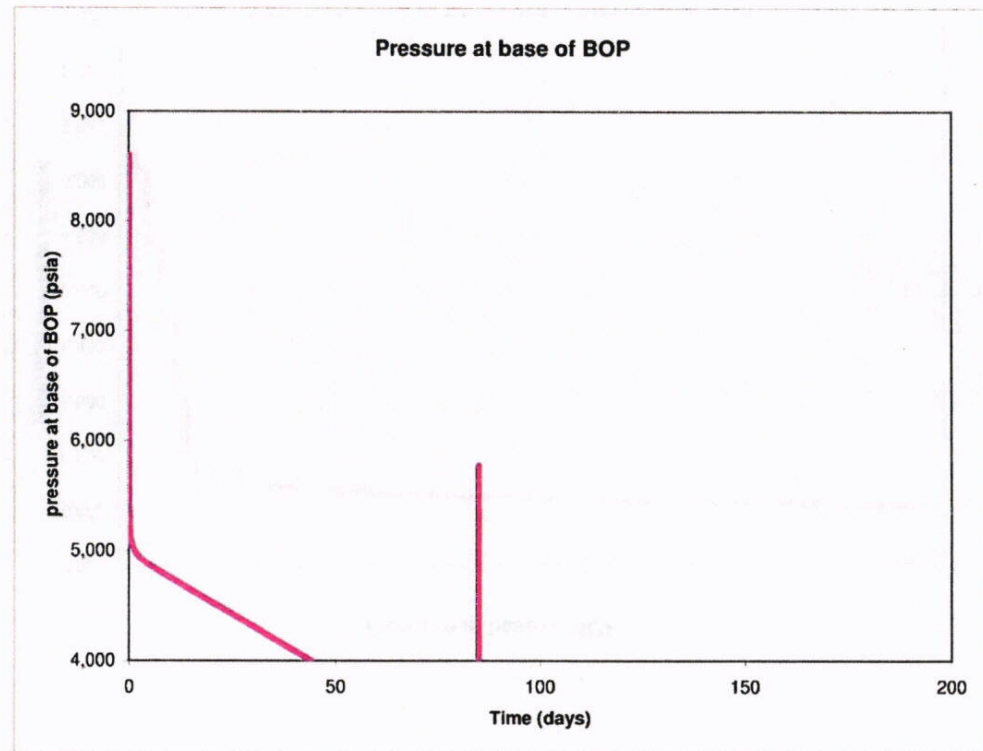
TREX 008639.0070

days	days	pressure at base of BOP aq = 0x	aq = 4x	aq = 14x 6700
	0		8600	
0.00186824			5671	
0.00411014			5567	
0.00680041			5510	
0.01002873			5468	
0.01390272			5435	
0.01855151			5406	
0.02413006			5380	
0.03082432			5356	
0.03885743			5333	
0.04849716			5312	
0.06006484			5292	
0.07394605			5272	
0.09060351			5253	
0.11059245			5234	
0.1345792			5215	
0.16336329			5197	
0.1979042			5179	
0.23935328			5161	
0.28909218			5143	
0.34877887			5125	
0.42040291			5108	
0.50635177			5090	
0.60949039			5073	
0.73325676			5055	
0.88177639			5038	
1.05999994			5021	
1.2738682			5003	
1.53051019			4986	
1.83848059			4969	
2.20804501			4951	
2.6515224			4933	
3.18369508			4915	
3.82230258			4896	
4.58863163			4875	
5.50822639			4852	

rho_o = 568

dP = 3250

well loss = 1900

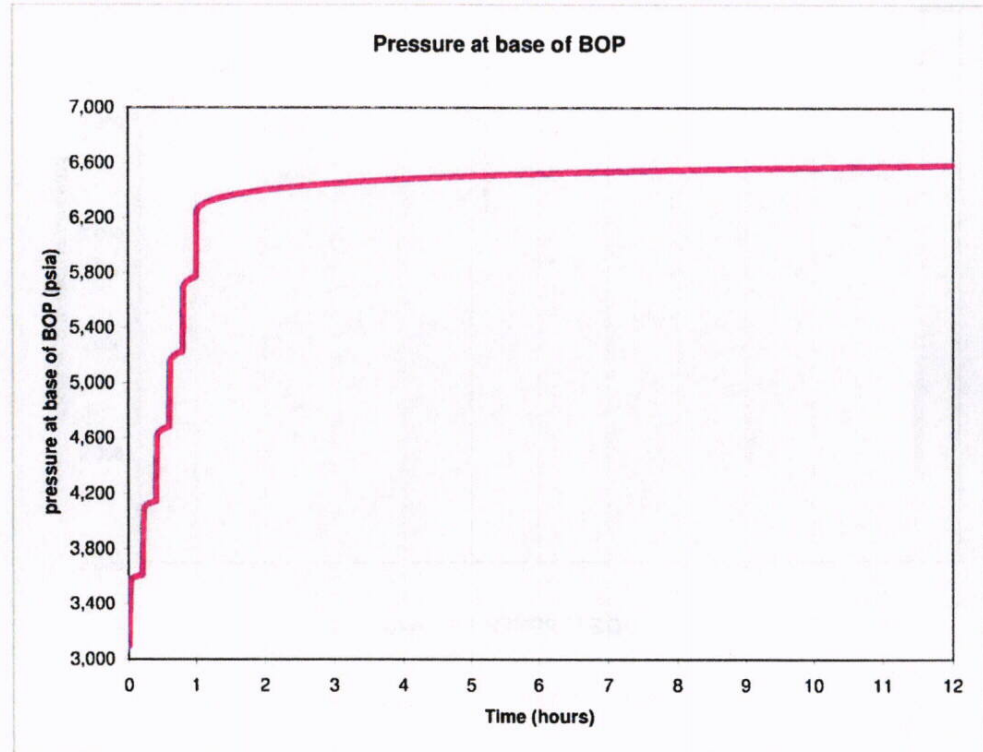


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TREX 008639.0071

6.61174011		4826	
7.93595648		4796	
9.52501678		4760	
11.43188858		4718	
13.72013474		4667	
16.46603012		4606	
19.76110458		4533	
23.7151947		4446	
28.46010399		4341	
34.15399551		4215	
40.98666382		4064	
49.18586731		3883	
59.02490997		3665	
70.83176422		3404	
84.99998474	0	3091	
85.00081635	0.02	3566	0
85.00164795	0.04	3582	0
85.00247955	0.06	3590	0
85.00331116	0.08	3596	0
85.00414276	0.10	3599	0
85.00497437	0.12	3603	0
85.00580597	0.14	3605	0
85.00663757	0.16	3608	0
85.00746918	0.18	3610	0
85.00830078	0.20	3611	0
85.00913239	0.22	4088	0
85.00996399	0.24	4105	0
85.01079559	0.26	4114	0
85.0116272	0.28	4121	0
85.0124588	0.30	4126	0
85.01329041	0.32	4130	0
85.01412201	0.34	4134	0
85.01495361	0.36	4137	0
85.01578522	0.38	4140	0
85.01661682	0.40	4142	0
85.01744843	0.42	4620	0
85.01828003	0.44	4638	0
85.01911163	0.46	4648	0

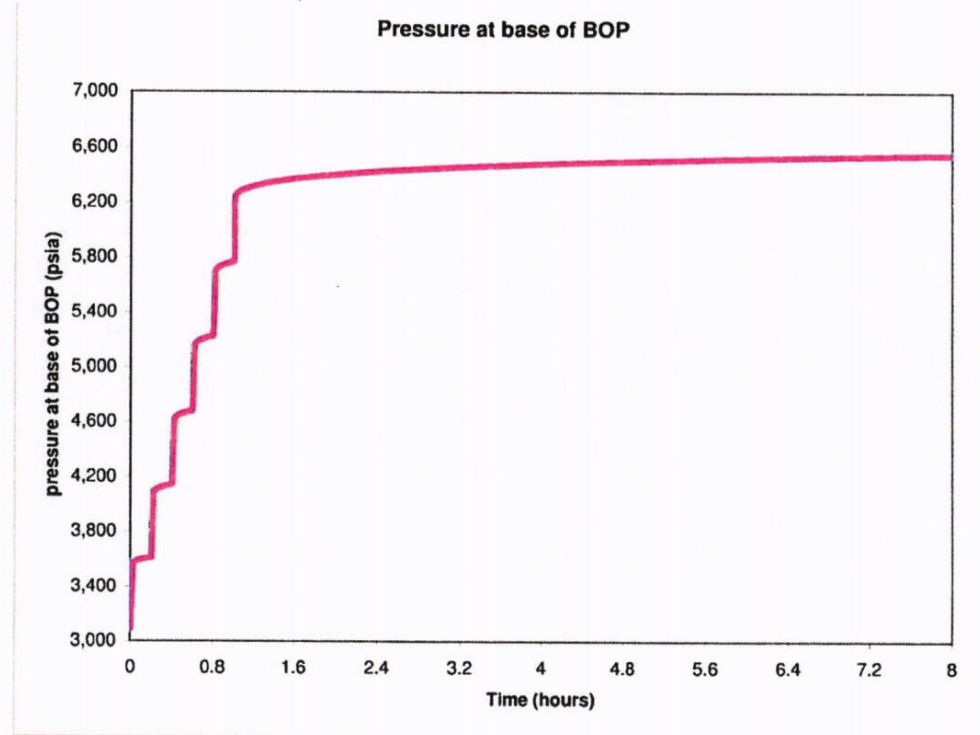


Pressure at base of BOP

CONFIDENTIAL

IGS075-018257

85.01994324	0.48	4656
85.02077484	0.50	4661
85.02160645	0.52	4666
85.02243805	0.54	4670
85.02326965	0.56	4674
85.02410126	0.58	4678
85.02493286	0.60	4681
85.02576447	0.62	5159
85.02659607	0.64	5178
85.02742767	0.66	5188
85.02825928	0.68	5196
85.02909088	0.70	5202
85.02992249	0.72	5208
85.03075409	0.74	5212
85.03158569	0.76	5217
85.0324173	0.78	5220
85.0332489	0.80	5224
85.03408051	0.82	5702
85.03491211	0.84	5721
85.03574371	0.86	5732
85.03657532	0.88	5740
85.03740692	0.90	5746
85.03823853	0.92	5752
85.03907013	0.94	5757
85.03990173	0.96	5762
85.04073334	0.98	5766
85.04156494	1.00	5770
85.04158783	1.00	6188
85.04161072	1.00	6205
85.04164124	1.00	6215
85.04167938	1.00	6222
85.04172516	1.00	6228
85.04177856	1.00	6233
85.04184723	1.00	6237
85.04192352	1.01	6242
85.04201508	1.01	6246
85.04212952	1.01	6250
85.04226685	1.01	6254



CONFIDENTIAL

IGS075-018258

TREX 008639.0073

85.04242706	1.02	6258
85.04262543	1.02	6262
85.04286194	1.03	6266
85.04314423	1.04	6271
85.04347992	1.04	6275
85.04388428	1.05	6280
85.04437256	1.07	6285
85.04496002	1.08	6290
85.04566193	1.10	6295
85.04650116	1.12	6301
85.04751587	1.14	6307
85.04872894	1.17	6314
85.05018616	1.20	6321
85.05193329	1.25	6328
85.05403137	1.30	6336
85.05654907	1.36	6345
85.05957031	1.43	6354
85.06319427	1.52	6363
85.06754303	1.62	6373
85.07276154	1.75	6384
85.07902527	1.90	6395
85.08654022	2.08	6407
85.09555817	2.29	6419
85.10637665	2.55	6432
85.11936188	2.87	6445
85.1349411	3.24	6459
85.15363312	3.69	6473
85.17606354	4.23	6487
85.20298767	4.87	6501
85.23529053	5.65	6516
85.27405548	6.58	6531
85.3205719	7.69	6545
85.37639618	9.03	6560
85.44338226	10.64	6575
85.52376556	12.57	6589
85.620224	14.89	6604
85.73597717	17.66	6618
85.87487793	21.00	6631

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IGS075-018259

TREX 008639.0074

86.04156494	25.00	6644
85.67682648	16.24	6614
85.6872406	16.49	6615
85.69765472	16.74	6617
85.70806885	16.99	6618
85.71848297	17.24	6619
85.72889709	17.49	6620
85.73931122	17.74	6621
85.74972534	17.99	6622
85.76013947	18.24	6624
85.77055359	18.49	6625
85.78096771	18.74	6626
85.79138184	18.99	6627
85.80179596	19.24	6628
85.81221008	19.49	6629
85.82262421	19.74	6630
85.83303833	19.99	6631
85.84345245	20.24	6632
85.85386658	20.49	6633
85.8642807	20.74	6634
85.87469482	20.99	6635
85.88510895	21.24	6636
85.89552307	21.49	6637
85.90593719	21.74	6637
85.91635132	21.99	6638
85.92676544	22.24	6639
85.93717957	22.49	6640
85.94759369	22.74	6641
85.95800781	22.99	6642
85.96842194	23.24	6642
85.97883606	23.49	6643
85.98925018	23.74	6644
85.99966431	23.99	6645
86.01007843	24.24	6646
86.02049255	24.49	6646
86.03090668	24.74	6647
86.0413208	24.99	6648

CONFIDENTIAL

IGS075-018260

TREX 008639.0075

Pressure at base of BOP

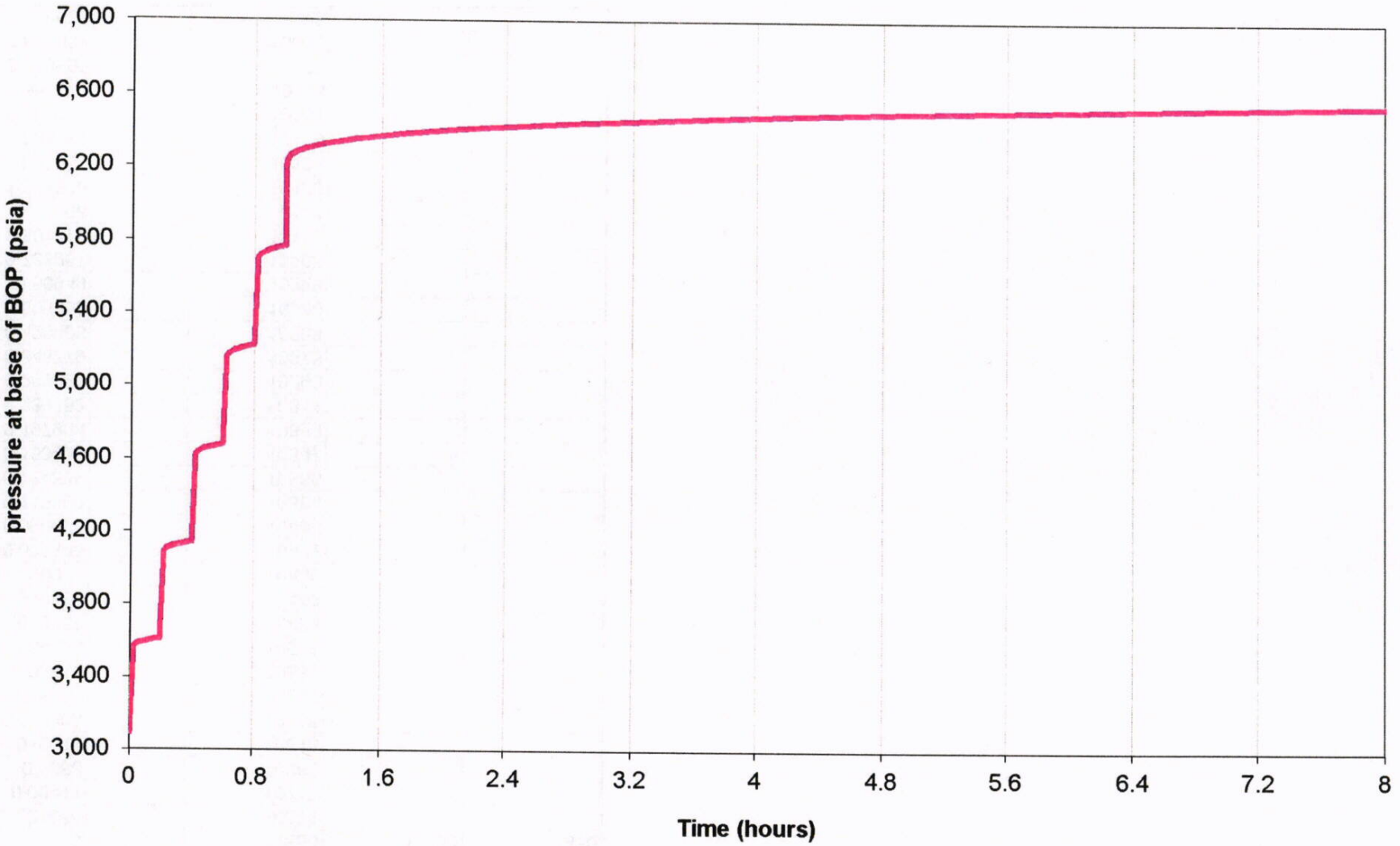


Chart2

	A	B	C	D	E
1			down hole pressure		
2	days	days	aq = 0x	aq = 4x	aq = 14x
3	0		11850	11850	11850
4	0.001868		10821		
5	0.00411		10717		
6	0.0068		10660		
7	0.010029		10618		
8	0.013903		10585		
9	0.018552		10556		
10	0.02413		10530		
11	0.030824		10506		
12	0.038857		10483		
13	0.048497		10462		
14	0.060065		10442		
15	0.073946		10422		
16	0.090604		10403		
17	0.110592		10384		
18	0.134579		10365		
19	0.163363		10347		
20	0.197904		10329		
21	0.239353		10311		
22	0.289092		10293		
23	0.348779		10275		
24	0.420403		10258		
25	0.506352		10240		
26	0.60949		10223		
27	0.733257		10205		
28	0.881776		10188		
29	1.06		10171		
30	1.273868		10153		
31	1.53051		10136		
32	1.838481		10119		
33	2.208045		10101		
34	2.651522		10083		
35	3.183695		10065		
36	3.822303		10046		
37	4.588632		10025		

downhole pressure

	A	B	C	D	E
1			down hole pressure		
2	days	days	aq = 0x	aq = 4x	aq = 14x
38	5.508226		10002		
39	6.61174		9976		
40	7.935956		9946		
41	9.525017		9910		
42	11.43189		9868		
43	13.72013		9817		
44	16.46603		9756		
45	19.7611		9683		
46	23.71519		9596		
47	28.4601		9491		
48	34.154		9365		
49	40.98666		9214		
50	49.18587		9033		
51	59.02491		8815		
52	70.83176		8554		
53	84.99998	0	8241		
54	85.00082	0.02	8399		
55	85.00165	0.04	8415		
56	85.00248	0.06	8423		
57	85.00331	0.08	8429		
58	85.00414	0.10	8432		
59	85.00497	0.12	8436		
60	85.00581	0.14	8438		
61	85.00664	0.16	8441		
62	85.00747	0.18	8443		
63	85.0083	0.20	8444		
64	85.00913	0.22	8605		
65	85.00996	0.24	8622		
66	85.0108	0.26	8631		
67	85.01163	0.28	8638		
68	85.01246	0.30	8643		
69	85.01329	0.32	8647		
70	85.01412	0.34	8651		
71	85.01495	0.36	8654		
72	85.01579	0.38	8657		
73	85.01662	0.40	8659		
74	85.01745	0.42	8820		
75	85.01828	0.44	8838		

downhole pressure

	A	B	C	D	E
1			down hole pressure		
2	days	days	aq = 0x	aq = 4x	aq = 14x
76	85.01911	0.46	8848		
77	85.01994	0.48	8856		
78	85.02077	0.50	8861		
79	85.02161	0.52	8866		
80	85.02244	0.54	8870		
81	85.02327	0.56	8874		
82	85.0241	0.58	8878		
83	85.02493	0.60	8881		
84	85.02576	0.62	9042		
85	85.0266	0.64	9061		
86	85.02743	0.66	9071		
87	85.02826	0.68	9079		
88	85.02909	0.70	9085		
89	85.02992	0.72	9091		
90	85.03075	0.74	9095		
91	85.03159	0.76	9100		
92	85.03242	0.78	9103		
93	85.03325	0.80	9107		
94	85.03408	0.82	9269		
95	85.03491	0.84	9288		
96	85.03574	0.86	9299		
97	85.03658	0.88	9307		
98	85.03741	0.90	9313		
99	85.03824	0.92	9319		
100	85.03907	0.94	9324		
101	85.0399	0.96	9329		
102	85.04073	0.98	9333		
103	85.04156	1.00	9337		
104	85.04159		9438		
105	85.04161		9455		
106	85.04164		9465		
107	85.04168		9472		
108	85.04173		9478		
109	85.04178		9483		
110	85.04185		9487		
111	85.04192		9492		
112	85.04202		9496		
113	85.04213		9500		

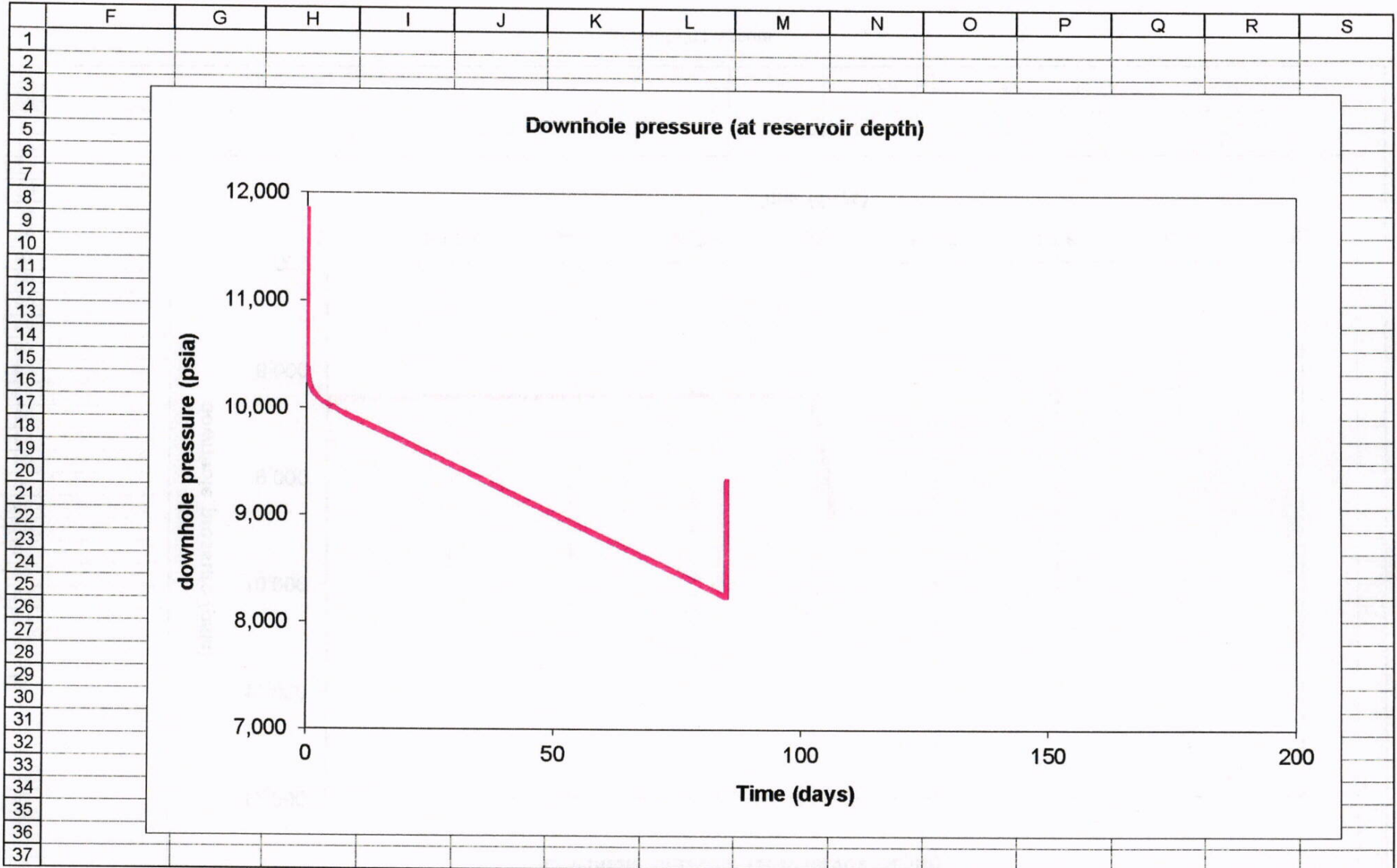
down hole pressure

	A	B	C	D	E
1			down hole pressure		
2	days	days	aq = 0x	aq = 4x	aq = 14x
114	85.04227		9504		
115	85.04243		9508		
116	85.04263		9512		
117	85.04286		9516		
118	85.04314		9521		
119	85.04348		9525		
120	85.04388		9530		
121	85.04437		9535		
122	85.04496		9540		
123	85.04566		9545		
124	85.0465		9551		
125	85.04752		9557		
126	85.04873		9564		
127	85.05019		9571		
128	85.05193		9578		
129	85.05403		9586		
130	85.05655		9595		
131	85.05957		9604		
132	85.06319		9613		
133	85.06754		9623		
134	85.07276		9634		
135	85.07903		9645		
136	85.08654		9657		
137	85.09556		9669		
138	85.10638		9682		
139	85.11936		9695		
140	85.13494		9709		
141	85.15363		9723		
142	85.17606		9737		
143	85.20299		9751		
144	85.23529		9766		
145	85.27406		9781		
146	85.32057		9795		
147	85.3764		9810		
148	85.44338		9825		
149	85.52377		9839		
150	85.62022		9854		
151	85.73598		9868		

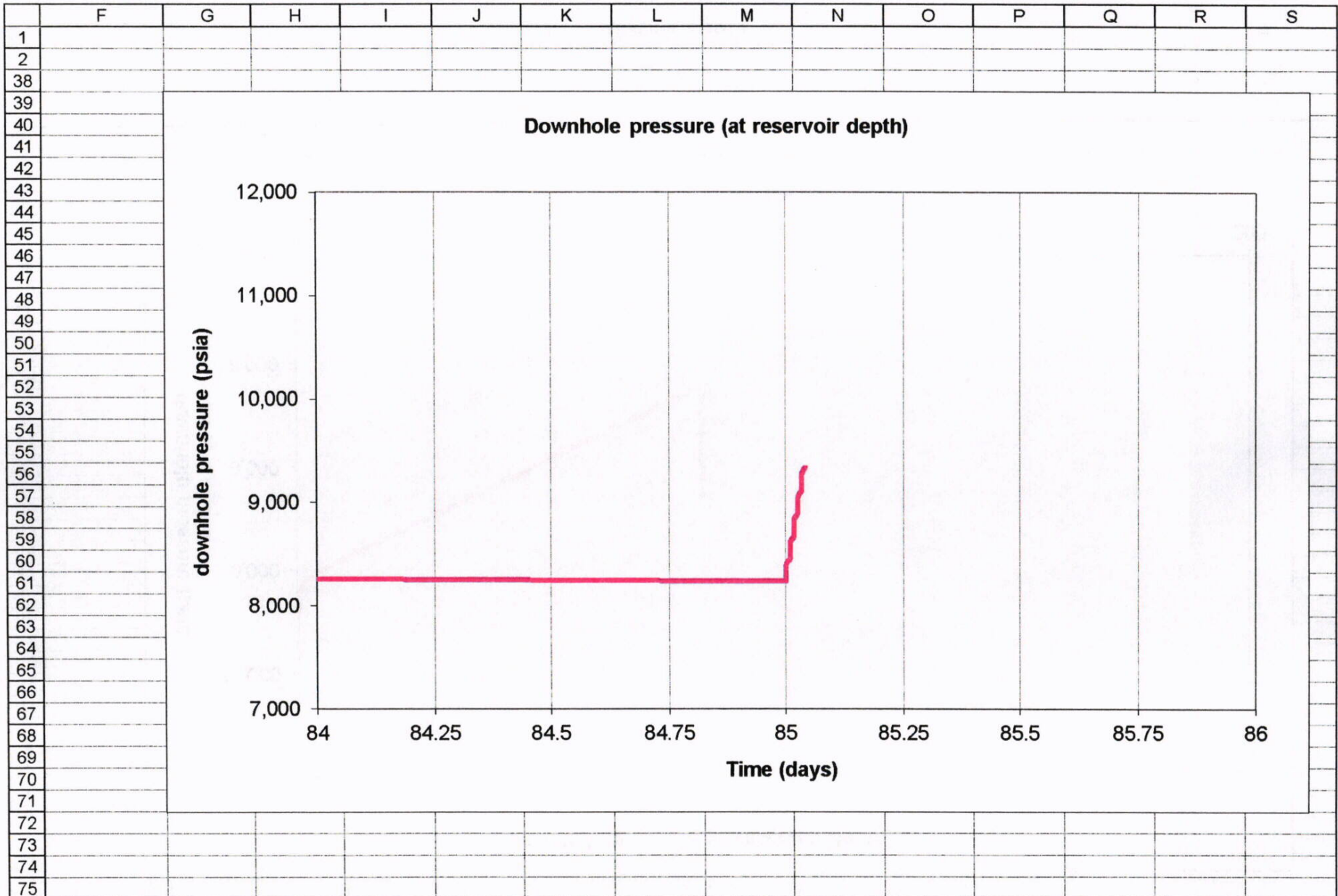
downhole pressure

	A	B	C	D	E
1			down hole pressure		
2	days	days	aq = 0x	aq = 4x	aq = 14x
152	85.87488		9881		
153	86.04156		9894		
154	85.67683		9864		
155	85.68724		9865		
156	85.69765		9867		
157	85.70807		9868		
158	85.71848		9869		
159	85.7289		9870		
160	85.73931		9871		
161	85.74973		9872		
162	85.76014		9874		
163	85.77055		9875		
164	85.78097		9876		
165	85.79138		9877		
166	85.8018		9878		
167	85.81221		9879		
168	85.82262		9880		
169	85.83304		9881		
170	85.84345		9882		
171	85.85387		9883		
172	85.86428		9884		
173	85.87469		9885		
174	85.88511		9886		
175	85.89552		9887		
176	85.90594		9887		
177	85.91635		9888		
178	85.92677		9889		
179	85.93718		9890		
180	85.94759		9891		
181	85.95801		9892		
182	85.96842		9892		
183	85.97884		9893		
184	85.98925		9894		
185	85.99966		9895		
186	86.01008		9896		
187	86.02049		9896		
188	86.03091		9897		
189	86.04132		9898		

down hole pressure



downhole pressure



downhole pressure

	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
1														
2														
76														
77														
78														
79														
80														
81														
82														
83														
84														
85														
86														
87														
88														
89														
90														
91														
92														
93														
94														
95														
96														
97														
98														
99														
100														
101														
102														
103														
104														
105														
106														
107														
108														
109														
110														
111														
112														
113														

downhole pressure

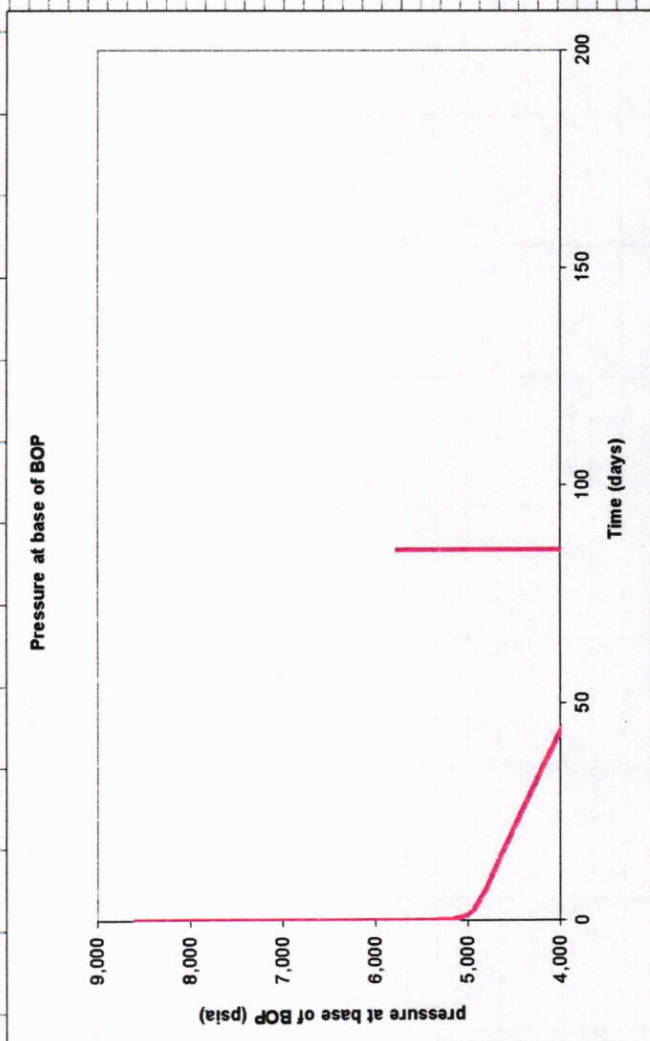
	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
1														
2														
114														
115														
116														
117														
118														
119														
120														
121														
122														
123														
124														
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151														

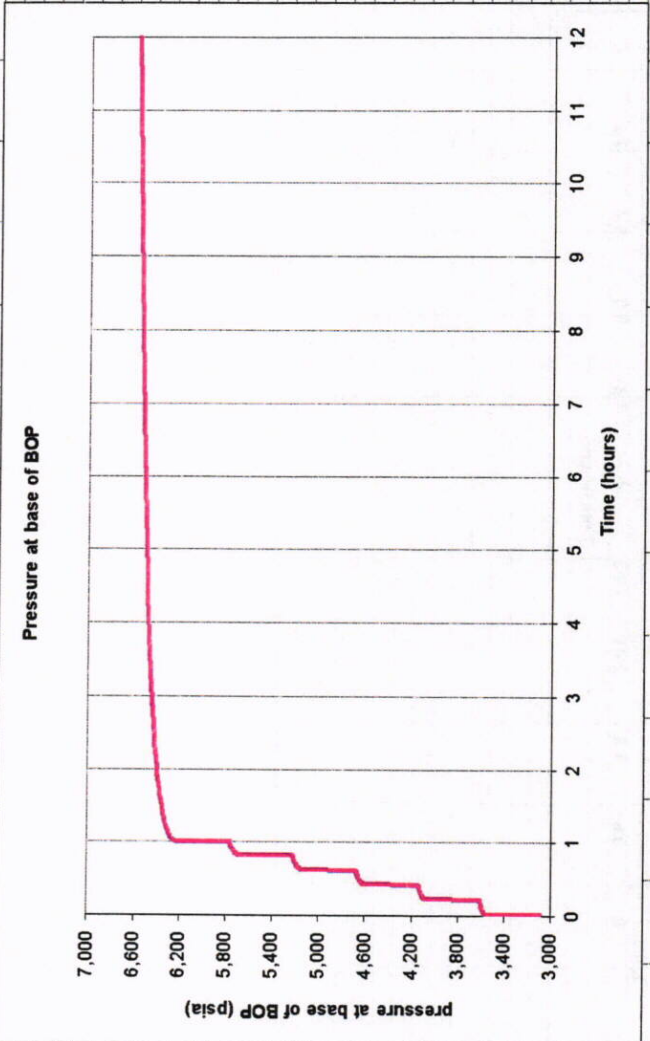
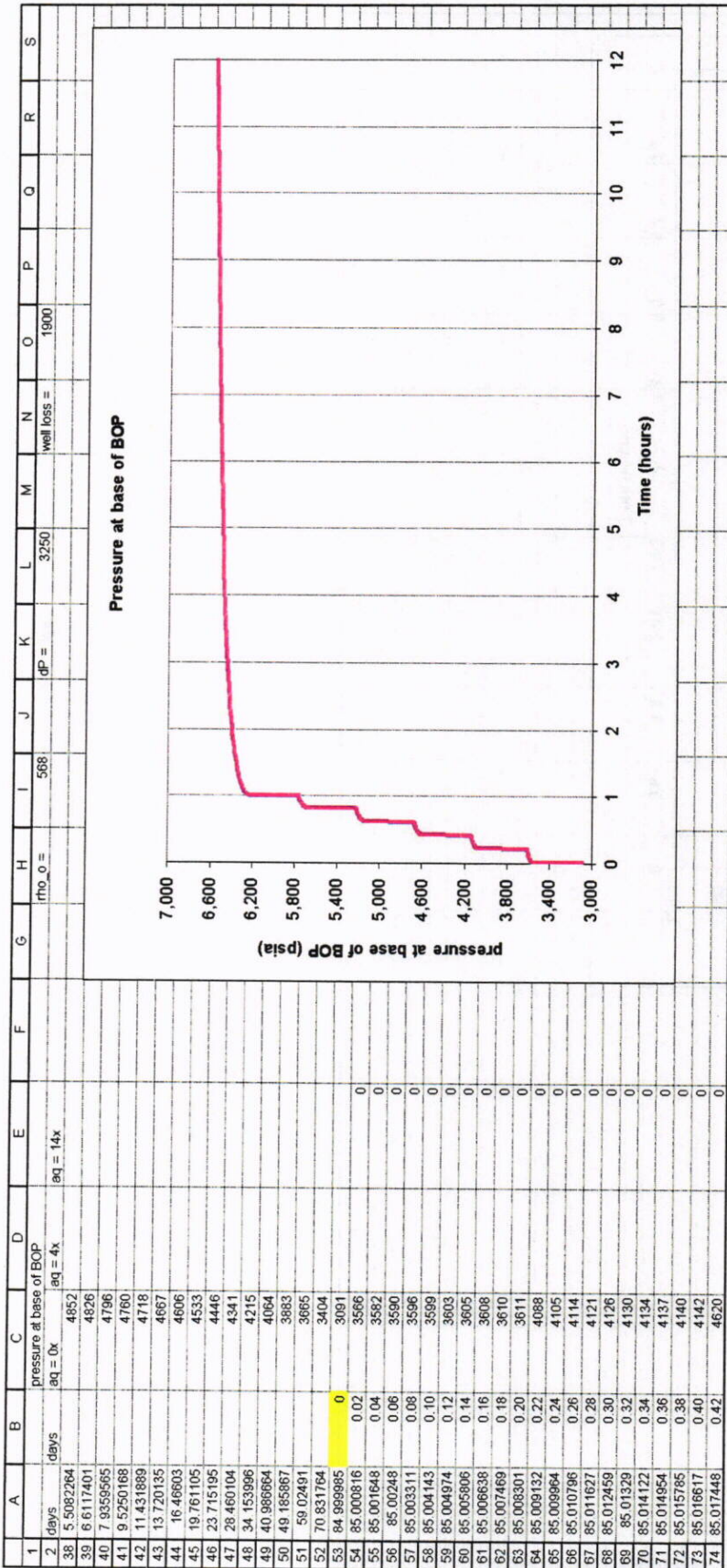
downr⁻¹/₂ pressure

	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
1														
2														
152														
153														
154														
155														
156														
157														
158														
159														
160														
161														
162														
163														
164														
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189														

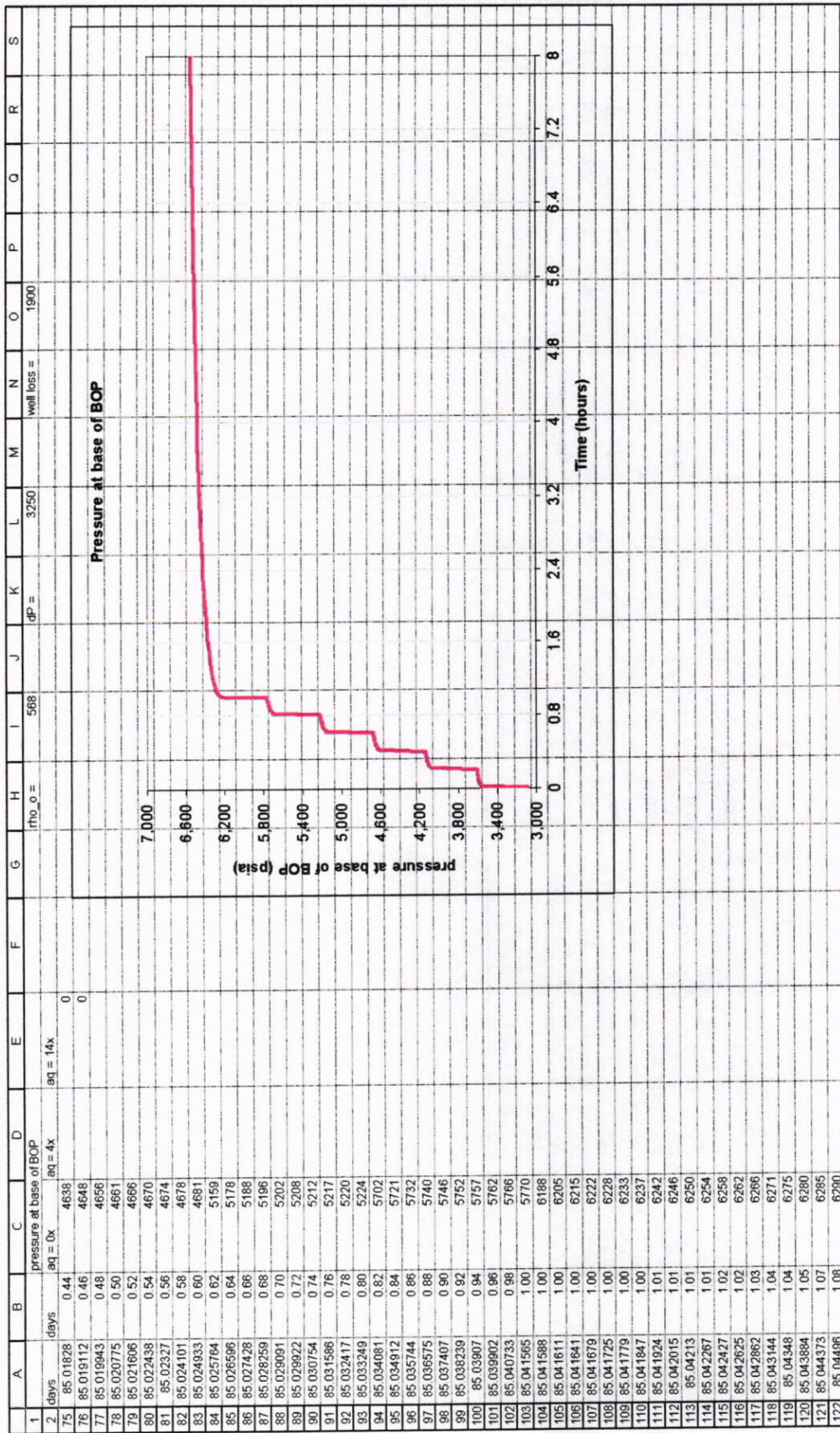
downhole pressure

A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
1	days	pressure at base of BOP dq = 0x	pressure at base of BOP dq = 4x	aq = 14x 6700														
2	0	8600						568			3250			1900				
3	4	0.0018682	5671															
4	5	0.0041101	5567															
5	6	0.0068004	5510															
6	7	0.0100287	5468															
7	8	0.0139027	5435															
8	9	0.0185515	5406															
9	10	0.0241301	5380															
10	11	0.0308243	5356															
11	12	0.0388574	5333															
12	13	0.0484972	5312															
13	14	0.0600648	5292															
14	15	0.0739461	5272															
15	16	0.0906035	5253															
16	17	0.1105925	5234															
17	18	0.1345792	5215															
18	19	0.1633633	5197															
19	20	0.1979042	5179															
20	21	0.2383533	5161															
21	22	0.2850922	5143															
22	23	0.3487789	5125															
23	24	0.4204029	5108															
24	25	0.5063518	5090															
25	26	0.6094904	5073															
26	27	0.7332568	5055															
27	28	0.8817764	5038															
28	29	1.0599999	5021															
29	30	1.2736682	5003															
30	31	1.5305102	4986															
31	32	1.8394806	4969															
32	33	2.2080045	4951															
33	34	2.6515224	4933															
34	35	3.1836951	4915															
35	36	3.8273026	4896															
36	37	4.5886316	4875															





pressure at base of BOP



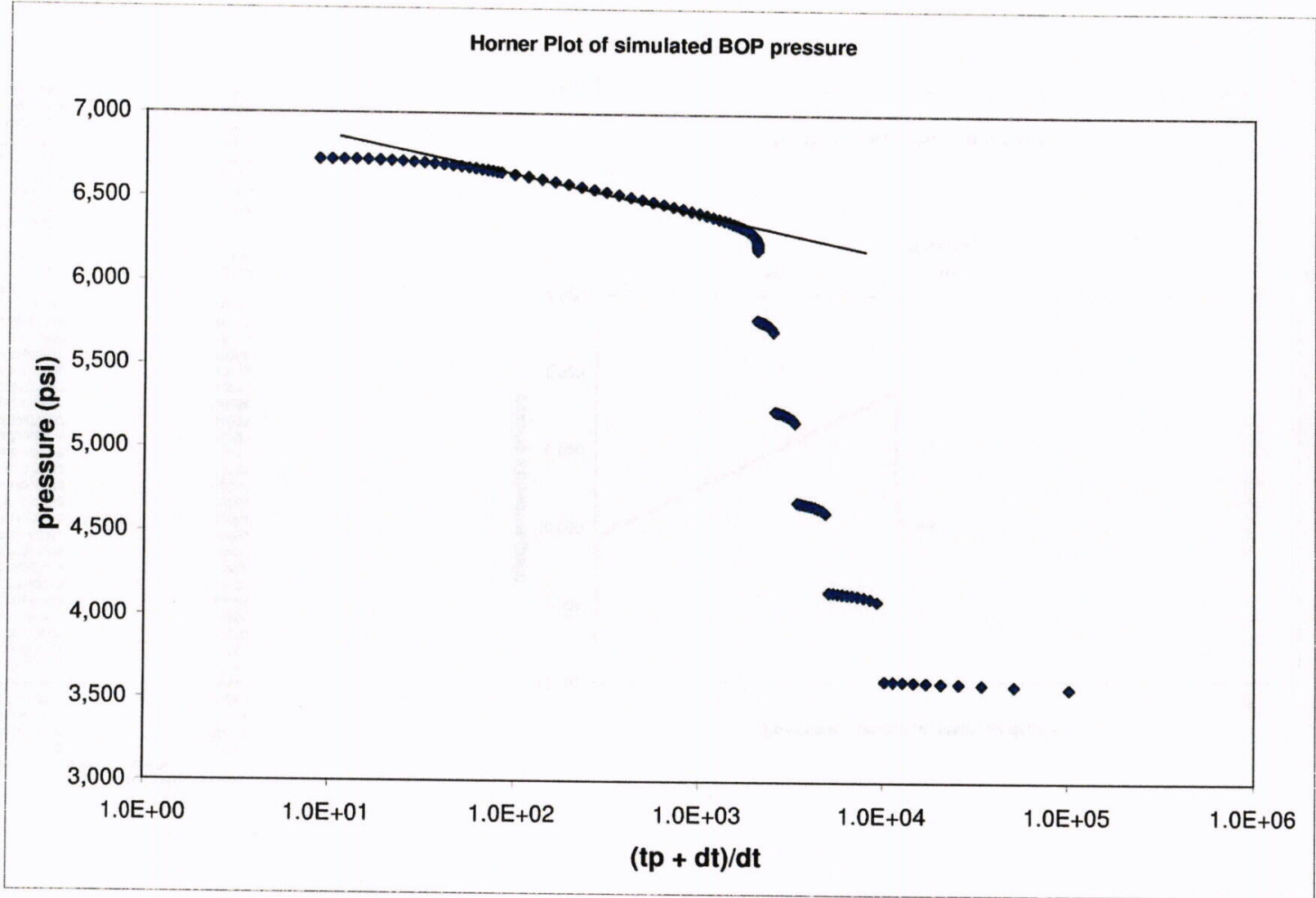
pref: ' base of BOP

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	
1																				
2	days	days	pressure at base of BOP aq = 0x	aq = 4x	aq = 14x			rho_o =	588	dP =	3250			well loss =	1900					
123	85 045662	1.10	6295																	
124	85 046501	1.12	6301																	
125	85 047516	1.14	6307																	
126	85 048729	1.17	6314																	
127	85 050186	1.20	6321																	
128	85 051933	1.25	6328																	
129	85 054031	1.30	6336																	
130	85 056549	1.36	6345																	
131	85 05957	1.43	6354																	
132	85 063194	1.52	6363																	
133	85 067543	1.62	6373																	
134	85 072762	1.75	6384																	
135	85 079025	1.90	6395																	
136	85 08654	2.08	6407																	
137	85 095558	2.29	6419																	
138	85 106377	2.55	6432																	
139	85 119362	2.87	6445																	
140	85 134941	3.24	6459																	
141	85 153633	3.69	6473																	
142	85 176064	4.23	6487																	
143	85 202988	4.87	6501																	
144	85 235291	5.65	6516																	
145	85 274055	6.58	6531																	
146	85 320572	7.69	6545																	
147	85 376396	9.03	6560																	
148	85 443382	10.64	6575																	
149	85 523786	12.57	6589																	
150	85 620224	14.89	6604																	
151	85 735977	17.66	6618																	
152	85 874878	21.00	6631																	
153	86 041565	25.00	6644																	

pressure at base of BOP

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
1	2 days		pressure at base of BOP aq = 0x	aq = 4x	aq = 14x			rho_0 =	568		dp =	3250		well loss =	1800				
154	85.676826	16.24	6614																
155	85.687241	16.49	6615																
156	85.697655	16.74	6617																
157	85.708069	16.99	6618																
158	85.718483	17.24	6619																
159	85.728897	17.49	6620																
160	85.739311	17.74	6621																
161	85.749725	17.99	6622																
162	85.760139	18.24	6624																
163	85.770554	18.49	6625																
164	85.780968	18.74	6626																
165	85.791382	18.99	6627																
166	85.801796	19.24	6628																
167	85.81221	19.49	6629																
168	85.822624	19.74	6630																
169	85.833038	19.99	6631																
170	85.843452	20.24	6632																
171	85.853867	20.49	6633																
172	85.864281	20.74	6634																
173	85.874695	20.99	6635																
174	85.885109	21.24	6636																
175	85.895523	21.49	6637																
176	85.905937	21.74	6637																
177	85.916351	21.99	6638																
178	85.926765	22.24	6639																
179	85.93718	22.49	6640																
180	85.947594	22.74	6641																
181	85.958008	22.99	6642																
182	85.968422	23.24	6642																
183	85.978836	23.49	6643																
184	85.98925	23.74	6644																
185	85.999664	23.99	6645																
186	86.010078	24.24	6646																
187	86.020493	24.49	6646																
188	86.030907	24.74	6647																
189	86.041321	24.99	6648																

pres: * base of BOP

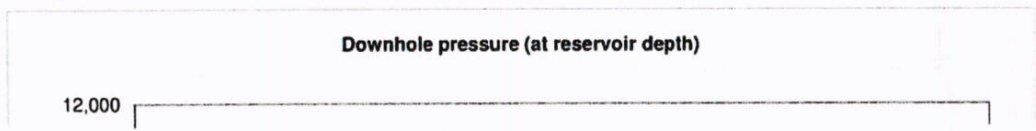
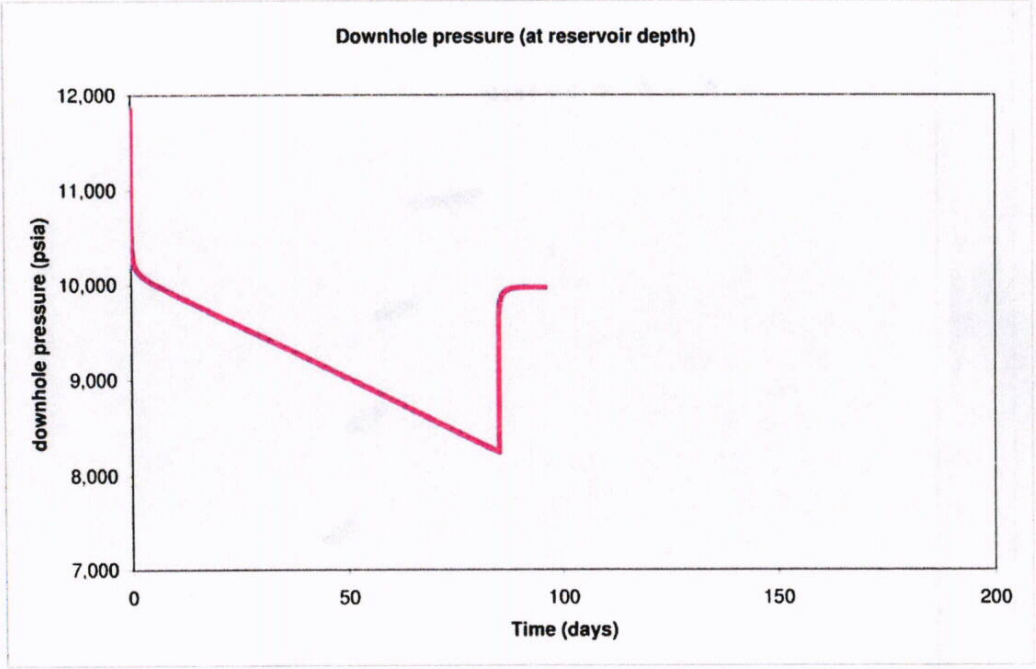


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IGS075-018261

TREX 008639.0093

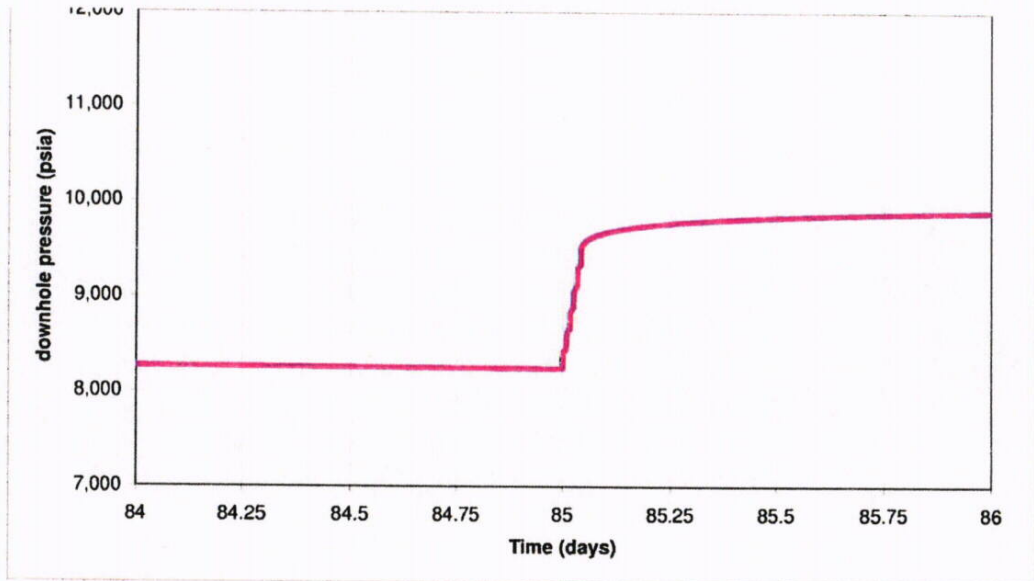
days	days	down hole pressure aq = 0x
0		11850
0.00186824		10821
0.00411014		10717
0.00680041		10660
0.01002873		10618
0.01390272		10585
0.01855151		10556
0.02413006		10530
0.03082432		10506
0.03885743		10483
0.04849716		10462
0.06006484		10442
0.07394605		10422
0.09060351		10403
0.11059245		10384
0.1345792		10365
0.16336329		10347
0.1979042		10329
0.23935328		10311
0.28909218		10293
0.34877887		10275
0.42040291		10258
0.50635177		10240
0.60949039		10223
0.73325676		10205
0.88177639		10188
1.05999994		10171
1.2738682		10153
1.53051019		10136
1.83848059		10119
2.20804501		10101
2.6515224		10083
3.18369508		10065
3.82230258		10046
4.58863163		10025
5.50822639		10002
6.61174011		9976
7.93595648		9946
9.52501678		9910
11.43188858		9868
13.72013474		9817



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16.46603012	9756
19.76110458	9683
23.7151947	9596
28.46010399	9491
34.15399551	9365
40.98666382	9214
49.18586731	9033
59.02490997	8815
70.83176422	8554 dP (psia) dT (day)
84.9998474	8241 815 35.81411743
85.00081635 0.000832	8399
85.00164795 0.001663	8415
85.00247955 0.002495	8423
85.00331116 0.003326	8429
85.00414276 0.004158	8432
85.00497437 0.004990	8436
85.00580597 0.005821	8438
85.00663757 0.006653	8441
85.00746918 0.007484	8443
85.00830078 0.008316	8444
85.00913239 0.009148	8605
85.00996399 0.009979	8622
85.01079559 0.010811	8631
85.0116272 0.011642	8638
85.0124588 0.012474	8643
85.01329041 0.013306	8647
85.01412201 0.014137	8651
85.01495361 0.014969	8654
85.01578522 0.015800	8657
85.01661682 0.016632	8659
85.01744843 0.017464	8820
85.01828003 0.018295	8838
85.01911163 0.019127	8848
85.01994324 0.019959	8856
85.02077484 0.020790	8861
85.02160645 0.021622	8866
85.02243805 0.022453	8870
85.02326965 0.023285	8874
85.02410126 0.024117	8878
85.02493286 0.024948	8881
85.02576447 0.025780	9042
85.02659607 0.026611	9061
85.02742767 0.027443	9071



85.02825928	0.028275	9079
85.02909088	0.029106	9085
85.02992249	0.029938	9091
85.03075409	0.030769	9095
85.03158569	0.031601	9100
85.0324173	0.032433	9103
85.0332489	0.033264	9107
85.03408051	0.034096	9269
85.03491211	0.034927	9288
85.03574371	0.035759	9299
85.03657532	0.036591	9307
85.03740692	0.037422	9313
85.03823853	0.038254	9319
85.03907013	0.039085	9324
85.03990173	0.039917	9329
85.04073334	0.040749	9333
85.04156494	0.041580	9337
85.04158783	0.041603	9438
85.04161072	0.041626	9455
85.04164124	0.041657	9465
85.04167938	0.041695	9472
85.04172516	0.041740	9478
85.04177856	0.041794	9483
85.04184723	0.041862	9487
85.04192352	0.041939	9492
85.04201508	0.042030	9496
85.04212952	0.042145	9500
85.04226685	0.042282	9504
85.04242706	0.042442	9508
85.04262543	0.042641	9512
85.04286194	0.042877	9516
85.04314423	0.043159	9521
85.04347992	0.043495	9525
85.04388428	0.043900	9530
85.04437256	0.044388	9535
85.04496002	0.044975	9540
85.04566193	0.045677	9545
85.04650116	0.046516	9551
85.04751587	0.047531	9557
85.04872894	0.048744	9564
85.05018616	0.050201	9571
85.05193329	0.051949	9578
85.05403137	0.054047	9586

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TREX 008639.0096

85.05654907	0.056564	9595
85.05957031	0.059586	9604
85.06319427	0.063210	9613
85.06754303	0.067558	9623
85.07276154	0.072777	9634
85.07902527	0.079041	9645
85.08654022	0.086555	9657
85.09555817	0.095573	9669
85.10637665	0.106392	9682
85.11936188	0.119377	9695
85.1349411	0.134956	9709
85.15363312	0.153648	9723
85.17606354	0.176079	9737
85.20298767	0.203003	9751
85.23529053	0.235306	9766
85.27405548	0.274071	9781
85.3205719	0.320587	9795
85.37639618	0.376411	9810
85.44338226	0.443398	9825
85.52376556	0.523781	9839
85.620224	0.620239	9854
85.73597717	0.735992	9868
85.87487793	0.874893	9881
86.04156494	1.041580	9894
86.09513092	1.095146	9898
86.15940857	1.159424	9903
86.23654175	1.236557	9907
86.32910156	1.329117	9912
86.44017792	1.440193	9918
86.57346344	1.573479	9923
86.73340607	1.733421	9929
86.92533875	1.925354	9935
87.15566254	2.155678	9941
87.43204498	2.432060	9946
87.76371002		9951
88.16170502		9956
88.63929749		9960
89.21240997		9963
89.90014648		9966
90.72542572		9968
91.71576691		9969
92.9041748		9970
94.33026123		9970

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TREX 008639.0097

96.04156494

9970

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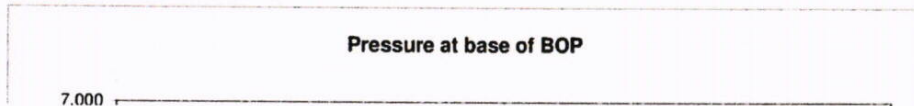
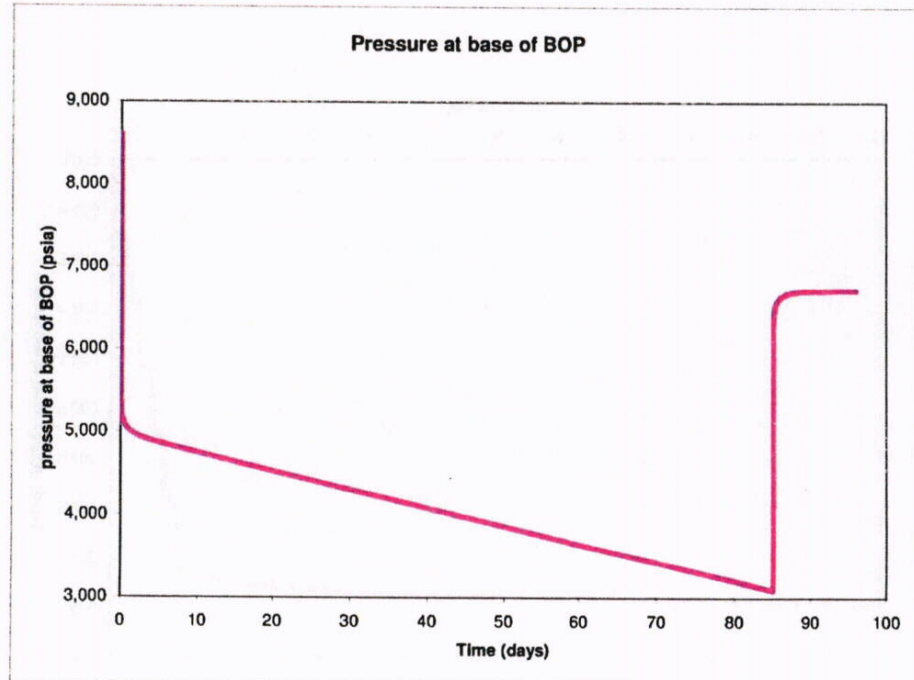
IGS075-018266

days	days	pressure at base of BOP aq = 0x	aq = 4x	aq = 14x
0	0		8600	-5150
0.00186824			5671	
0.00411014			5567	
0.00680041			5510	
0.01002873			5468	
0.01390272			5435	
0.01855151			5406	
0.02413006			5380	
0.03082432			5356	
0.03885743			5333	
0.04849716			5312	
0.06006484			5292	
0.07394605			5272	
0.09060351			5253	
0.11059245			5234	
0.1345792			5215	
0.16336329			5197	
0.1979042			5179	
0.23935328			5161	
0.28909218			5143	
0.34877887			5125	
0.42040291			5108	
0.50635177			5090	
0.60949039			5073	
0.73325676			5055	
0.88177639			5038	
1.05999994			5021	
1.2738682			5003	
1.53051019			4986	
1.83848059			4969	
2.20804501			4951	
2.6515224			4933	
3.18369508			4915	
3.82230258			4896	
4.58863163			4875	
5.50822639			4852	
6.61174011			4826	
7.93595648			4796	
9.52501678			4760	
11.43188858			4718	

rho_o = 568

dP = 3250

well loss = 1900

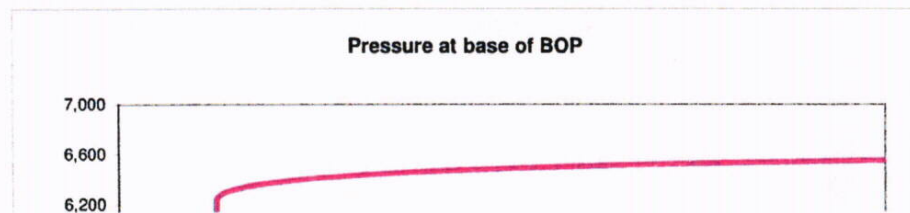
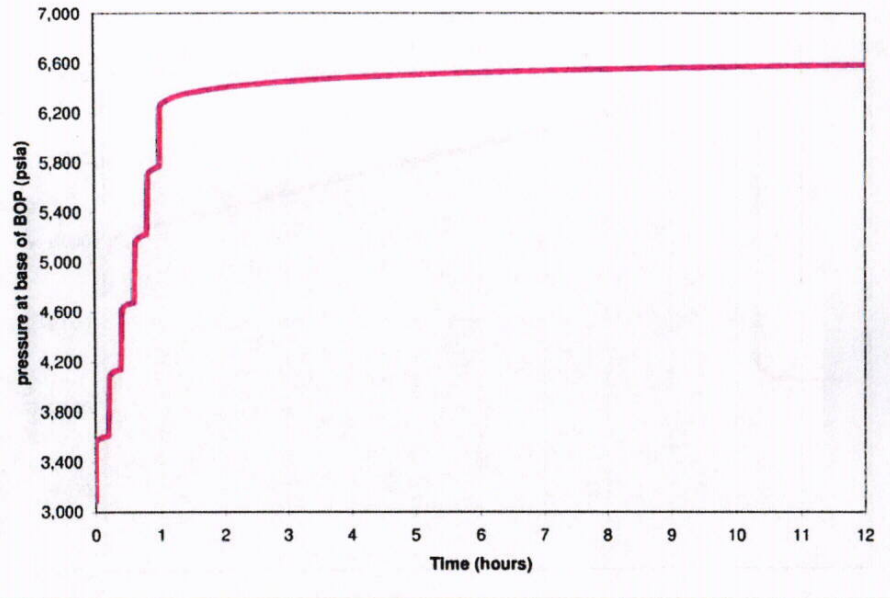


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TREX 008639.0099

13.72013474		4667
16.46603012		4606
19.76110458		4533
23.7151947		4446
28.46010399		4341
34.15399551		4215
40.98666382		4064
49.18586731		3883
59.02490997		3665
70.83176422	shutin hr	3404
84.99998474	0	3091
85.00081635	0.00083	3566
85.00164795	0.040	3582
85.00247955	0.060	3590
85.00331116	0.080	3596
85.00414276	0.100	3599
85.00497437	0.120	3603
85.00580597	0.140	3605
85.00663757	0.160	3608
85.00746918	0.180	3610
85.00830078	0.200	3611
85.00913239	0.220	4088
85.00996399	0.240	4105
85.01079559	0.259	4114
85.0116272	0.279	4121
85.0124588	0.299	4126
85.01329041	0.319	4130
85.01412201	0.339	4134
85.01495361	0.359	4137
85.01578522	0.379	4140
85.01661682	0.399	4142
85.01744843	0.419	4620
85.01828003	0.439	4638
85.01911163	0.459	4648
85.01994324	0.479	4656
85.02077484	0.499	4661
85.02160645	0.519	4666
85.02243805	0.539	4670
85.02326965	0.559	4674
85.02410126	0.579	4678
85.02493286	0.599	4681
85.02576447	0.619	5159
		7/15/2010 12:30
		7/15/2010 12:31
		7/15/2010 12:32
		7/15/2010 12:33
		7/15/2010 12:34
		7/15/2010 12:35
		7/15/2010 12:37
		7/15/2010 12:38
		7/15/2010 12:39
		7/15/2010 12:40
		7/15/2010 12:41
		7/15/2010 12:43
		7/15/2010 12:44
		7/15/2010 12:45
		7/15/2010 12:46
		7/15/2010 12:47
		7/15/2010 12:49
		7/15/2010 12:50
		7/15/2010 12:51
		7/15/2010 12:52
		7/15/2010 12:53
		7/15/2010 12:55
		7/15/2010 12:56
		7/15/2010 12:57
		7/15/2010 12:58
		7/15/2010 12:59
		7/15/2010 13:01
		7/15/2010 13:02
		7/15/2010 13:03
		7/15/2010 13:04
		7/15/2010 13:05
		7/15/2010 13:07



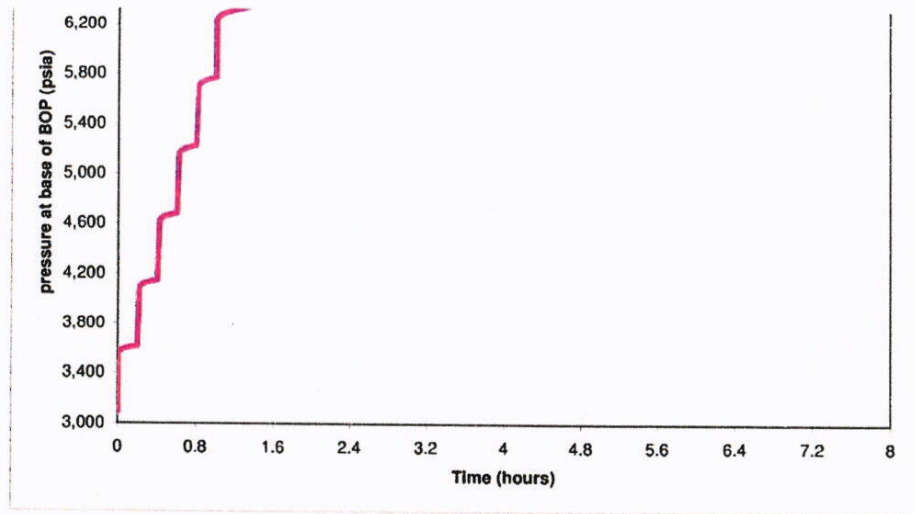
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IGS075-018268

TREX 008639.0100

85.02659607	0.639
85.02742767	0.659
85.02825928	0.679
85.02909088	0.699
85.02992249	0.719
85.03075409	0.738
85.03158569	0.758
85.0324173	0.778
85.0332489	0.798
85.03408051	0.818
85.03491211	0.838
85.03574371	0.858
85.03657532	0.878
85.03740692	0.898
85.03823853	0.918
85.03907013	0.938
85.03990173	0.958
85.04073334	0.978
85.04156494	0.998
85.04158783	0.998
85.04161072	0.999
85.04164124	1.000
85.04167938	1.001
85.04172516	1.002
85.04177856	1.003
85.04184723	1.005
85.04192352	1.007
85.04201508	1.009
85.04212952	1.011
85.04226685	1.015
85.04242706	1.019
85.04262543	1.023
85.04286194	1.029
85.04314423	1.036
85.04347992	1.044
85.04388428	1.054
85.04437256	1.065
85.04496002	1.079
85.04566193	1.096
85.04650116	1.116
85.04751587	1.141
85.04872894	1.170

5178	7/15/2010 13:08
5188	7/15/2010 13:09
5196	7/15/2010 13:10
5202	7/15/2010 13:11
5208	7/15/2010 13:13
5212	7/15/2010 13:14
5217	7/15/2010 13:15
5220	7/15/2010 13:16
5224	7/15/2010 13:17
5702	7/15/2010 13:19
5721	7/15/2010 13:20
5732	7/15/2010 13:21
5740	7/15/2010 13:22
5746	7/15/2010 13:23
5752	7/15/2010 13:25
5757	7/15/2010 13:26
5762	7/15/2010 13:27
5766	7/15/2010 13:28
5770	rate (psi/hr) 7/15/2010 13:29
6188	760279 7/15/2010 13:29
6205	30945 7/15/2010 13:29
6215	13652 7/15/2010 13:29
6222	7647 7/15/2010 13:30
6228	5461 7/15/2010 13:30
6233	3901 7/15/2010 13:30
6237	2427 7/15/2010 13:30
6242	2731 7/15/2010 13:30
6246	1820 7/15/2010 13:30
6250	1456 7/15/2010 13:30
6254	1214 7/15/2010 13:30
6258	1040 7/15/2010 13:31
6262	840 7/15/2010 13:31
6266	705 7/15/2010 13:31
6271	738 7/15/2010 13:32
6275	496 7/15/2010 13:32
6280	515 7/15/2010 13:33
6285	427 7/15/2010 13:33
6290	355 7/15/2010 13:34
6295	297 7/15/2010 13:35
6301	298 7/15/2010 13:36
6307	246 7/15/2010 13:38
6314	240 7/15/2010 13:40



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TREX 008639.0101

85.05018616	1.205	6321	200	7/15/2010	13:42
85.05193329	1.247	6328	167	7/15/2010	13:44
85.05403137	1.297	6336	159	7/15/2010	13:47
85.05654907	1.358	6345	149	7/15/2010	13:51
85.05957031	1.430	6354	124	7/15/2010	13:55
85.06319427	1.517	6363	103	7/15/2010	14:01
85.06754303	1.621	6373	96	7/15/2010	14:07
85.07276154	1.747	6384	88	7/15/2010	14:14
85.07902527	1.897	6395	73	7/15/2010	14:23
85.08654022	2.077	6407	67	7/15/2010	14:34
85.09555817	2.294	6419	55	7/15/2010	14:47
85.10637665	2.553	6432	50	7/15/2010	15:03
85.11936188	2.865	6445	42	7/15/2010	15:21
85.1349411	3.239	6459	37	7/15/2010	15:44
85.15363312	3.688	6473	31	7/15/2010	16:11
85.17606354	4.226	6487	26	7/15/2010	16:43
85.20298767	4.872	6501	22	7/15/2010	17:22
85.23529053	5.647	6516	19	7/15/2010	18:08
85.27405548	6.578	6531	16	7/15/2010	19:04
85.3205719	7.694	6545	13	7/15/2010	20:11
85.37639618	9.034	6560	11	7/15/2010	21:32
85.44338226	10.642	6575	9	7/15/2010	23:08
85.52376556	12.571	6589	7	7/16/2010	1:04
85.620224	14.886	6604	6	7/16/2010	3:23
85.73597717	17.664	6618	5	7/16/2010	6:09
85.87487793	20.997	6631	4	7/16/2010	9:29
86.04156494	24.998	6644	3	7/16/2010	13:29
86.09513092	26.284	6648			
86.15940857	27.826	6653			
86.23654175	29.677	6657			
86.32910156	31.899	6662			
86.44017792	34.565	6668			
86.57346344	37.763	6673			
86.73340607	41.602	6679			
86.92533875	46.208	6685			
87.15566254	51.736	6691			
87.43204498	58.369	6696			
87.76371002	66.329	6701			
88.16170502	75.881	6706			
88.63929749	87.344	6710			
89.21240997	101.098	6713			
89.90014648	117.604	6716			

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IGS075-018270

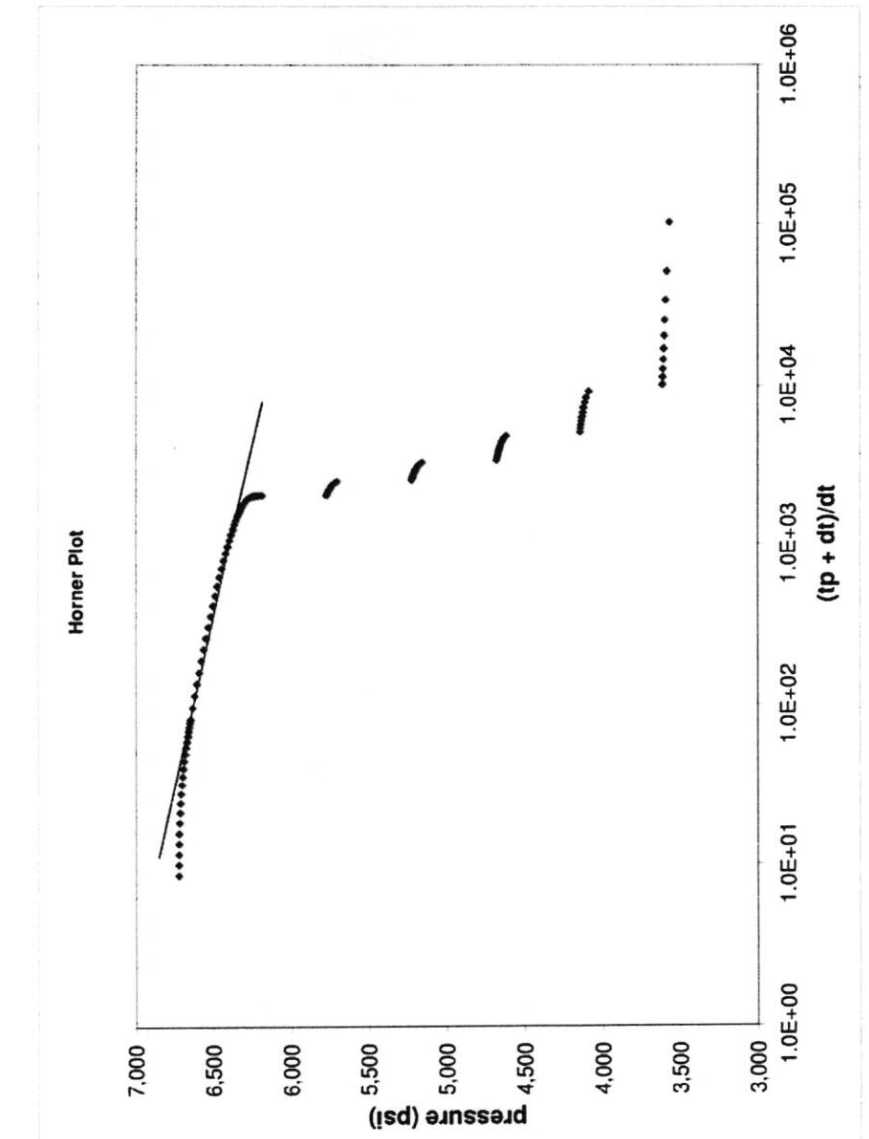
TREX 008639.0102

90.72542572	137.411	6718
91.71576691	161.179	6719
92.9041748	189.701	6720
94.33026123	223.927	6720
96.04156494	264.998	6720

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TREX 008639.0103



Time (h)	Pressure (psi)	Derivative (psi)
7.1520101230	40374.5208333333	3.091
7.1520101231	40374.5216649433	3.091
7.1520101232	0.0008316100	3.091
7.1520101233		3.091
7.1520101234		3.091
7.1520101235		3.091
7.1520101236		3.091
7.1520101237		3.091
7.1520101238		3.091
7.1520101239		3.091
7.1520101240		3.091
7.1520101241		3.091
7.1520101242		3.091
7.1520101243		3.091
7.1520101244		3.091
7.1520101245		3.091
7.1520101246		3.091
7.1520101247		3.091
7.1520101248		3.091
7.1520101249		3.091
7.1520101250		3.091
7.1520101251		3.091
7.1520101252		3.091
7.1520101253		3.091
7.1520101254		3.091
7.1520101255		3.091
7.1520101256		3.091
7.1520101257		3.091
7.1520101258		3.091
7.1520101259		3.091
7.1520101301		3.091
7.1520101302		3.091
7.1520101303		3.091
7.1520101304		3.091
7.1520101305		3.091
7.1520101307		3.091
7.1520101308		3.091
7.1520101309		3.091
7.1520101310		3.091
7.1520101311		3.091
7.1520101312		3.091
7.1520101313		3.091
7.1520101314		3.091
7.1520101315		3.091
7.1520101316		3.091
7.1520101317		3.091
7.1520101318		3.091
7.1520101319		3.091
7.1520101320		3.091
7.1520101321		3.091
7.1520101322		3.091
7.1520101323		3.091
7.1520101324		3.091
7.1520101325		3.091
7.1520101326		3.091
7.1520101327		3.091
7.1520101328		3.091
7.1520101329		3.091
7.1520101329		3.091
7.1520101329		3.091
7.1520101329		3.091
7.1520101329		3.091
7.1520101329		3.091
7.1520101330		3.091
7.1520101330		3.091
7.1520101330		3.091
7.1520101330		3.091

85.04192352 0.04193878 2027.763409 6242 7:15:2010 13.30
 85.04201508 0.04202034 2023.48255 6246 7:15:2010 13.30
 85.04212902 0.04214478 2017.85767 6250 7:15:2010 13.30
 85.04226685 0.04228311 2011.306126 6254 7:15:2010 13.30
 85.04242706 0.04244232 2003.717682 6258 7:15:2010 13.31
 85.04262543 0.04264069 1994.400781 6262 7:15:2010 13.31
 85.04286194 0.04287772 1983.405212 6266 7:15:2010 13.31
 85.04314423 0.04315949 1970.439844 6271 7:15:2010 13.32
 85.04347392 0.04349518 1955.239176 6275 7:15:2010 13.32
 85.04386828 0.04389954 1937.23862 6280 7:15:2010 13.33
 85.04437226 0.04439782 1915.038385 6285 7:15:2010 13.33
 85.04496602 0.04497328 1890.22675 6290 7:15:2010 13.34
 85.04564519 0.04565119 1861.884116 6295 7:15:2010 13.35
 85.04631175 0.04631642 1830.314694 6301 7:15:2010 13.36
 85.04707197 0.04707511 1799.301469 6307 7:15:2010 13.38
 85.04792884 0.04792442 1764.268698 6314 7:15:2010 13.40
 85.04887288 0.04887442 1724.268698 6321 7:15:2010 13.42
 85.05193329 0.05194855 1694.178893 6328 7:15:2010 13.44
 85.05440337 0.05440663 1657.24619 6336 7:15:2010 13.44
 85.05654807 0.05655643 1623.715722 6345 7:15:2010 13.47
 85.05957031 0.05958557 1427.518623 6354 7:15:2010 13.51
 85.06319427 0.06320953 1345.236693 6363 7:15:2010 14.01
 85.06784303 0.06785829 1259.172531 6373 7:15:2010 14.07
 85.07276154 0.07277668 1168.584413 6384 7:15:2010 14.14
 85.07902827 0.07904053 1076.374654 6395 7:15:2010 14.23
 85.08654022 0.08655548 983.0289223 6407 7:15:2010 14.34
 85.09555817 0.09557343 890.3663604 6419 7:15:2010 14.47
 85.10637665 0.10639191 799.532783 6432 7:15:2010 15.03
 85.11806188 0.11807714 713.0289227 6445 7:15:2010 15.21
 85.13094411 0.13095936 630.833116 6459 7:15:2010 15.44
 85.15083312 0.15084838 554.2110702 6473 7:15:2010 16.11
 85.17060354 0.17061880 483.7382296 6487 7:15:2010 16.43
 85.20298767 0.20299293 419.7130023 6501 7:15:2010 17.22
 85.23530653 0.23531179 362.2301153 6516 7:15:2010 18.08
 85.27406546 0.27407074 311.138823 6531 7:15:2010 19.04
 85.32059719 0.32060245 268.1394564 6545 7:15:2010 20.11
 85.37652114 0.37652640 228.8106881 6560 7:15:2010 21.32
 85.44318226 0.44318752 191.01354 6575 7:15:2010 23.06
 85.52316656 0.52317182 154.2103698 6594 7:16:2010 0.94
 85.620224 0.62022926 135.049839 6604 7:16:2010 3.23
 85.73597717 0.73598243 118.492926 6618 7:16:2010 6.99
 85.87467793 0.87468319 98.1549924 6631 0.13969076 7:16:2010 6.99
 86.04156484 1.0415802 82.60675936 6644 0.16668701 7:16:2010 13.20
 86.09513092 1.09514618 78.6159539 6648 0.055365598 7:16:2010 14.47
 86.15940857 1.15942383 74.31282699 6653 0.06427765 7:16:2010 16.19
 86.23654175 1.23655701 69.73923649 6657 0.07113318 7:16:2010 18.10
 86.32910156 1.32911682 64.58223013 6662 0.09255081 7:16:2010 20.23
 86.44017792 1.44019318 60.0198495 6668 0.11107636 7:16:2010 23.03
 86.57348344 1.57349874 55.02042286 6673 0.13328552 7:17:2010 2.15
 86.92333875 1.92335401 45.1471741 6679 0.15994263 7:17:2010 10.42
 87.15566254 2.1556778 40.43074644 6685 0.19193266 7:17:2010 16.14
 87.43204488 2.43206024 35.94978992 6691 0.23032379 7:17:2010 22.52
 87.76371002 2.76372528 31.75583391 6696 0.27638244 7:17:2010 22.52
 88.10110502 3.10112028 27.88609385 6701 0.33166504 7:18:2010 6.49
 88.63807049 3.63808575 24.3590539 6706 0.3977995 7:19:2010 16.22
 89.12426997 4.22428523 21.17839608 6713 0.47759247 7:19:2010 3.50
 89.66746944 4.86748470 18.34033059 6716 0.58739851 7:20:2010 17.35
 90.22542632 5.72544086 15.84601536 6718 0.82527924 7:21:2010 5.54

91.71578691	6.71578217	13.6567513	6719	0.99034119	7/22/2010 5:40
92.9041748	7.90419006	11.75378807	6720		7/23/2010 10:12
94.33026123	9.33027649	10.11012496	6720		7/24/2010 20:25
96.04156494	11.0415802	8.698172109	6720		7/26/2010 13:29

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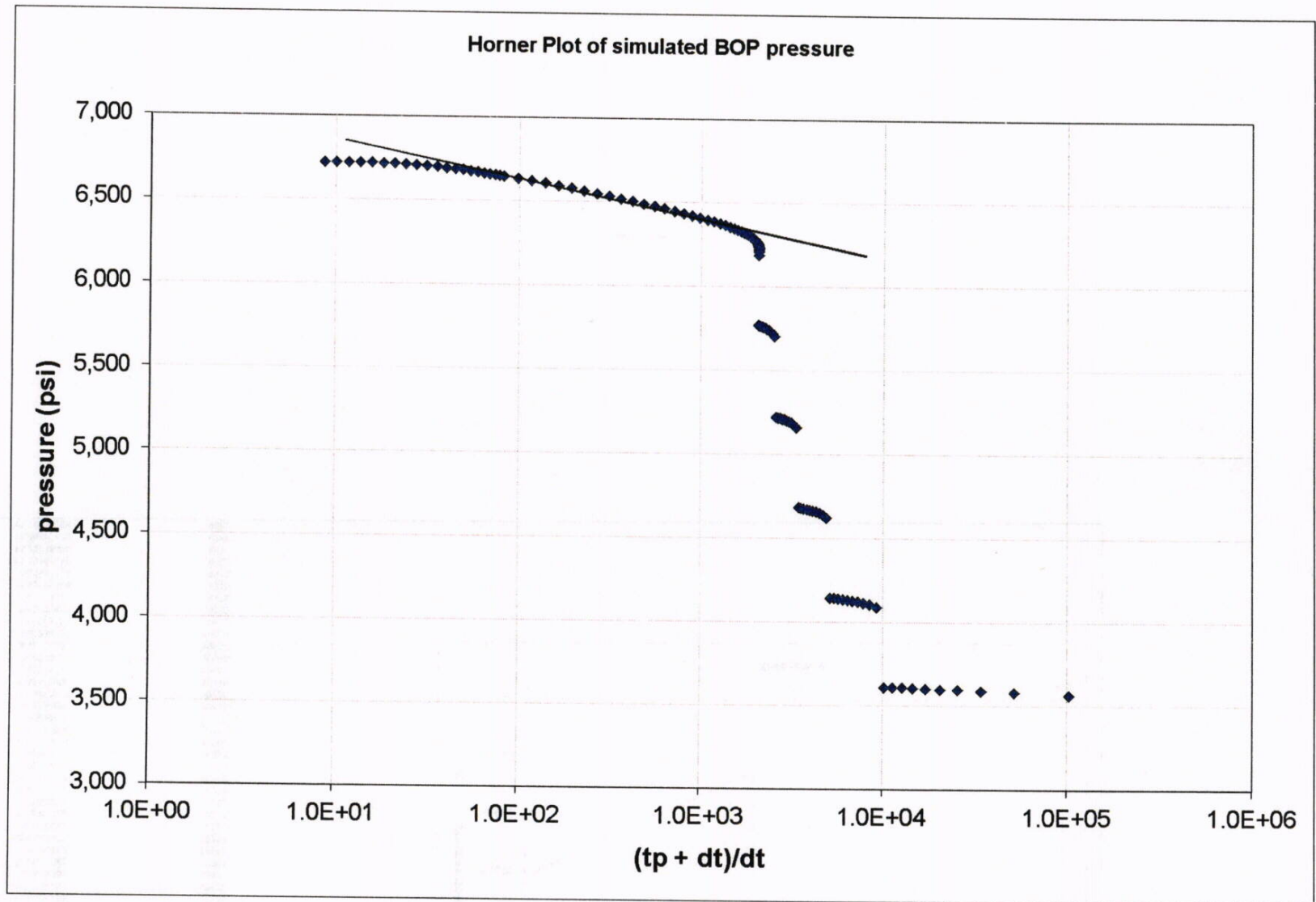
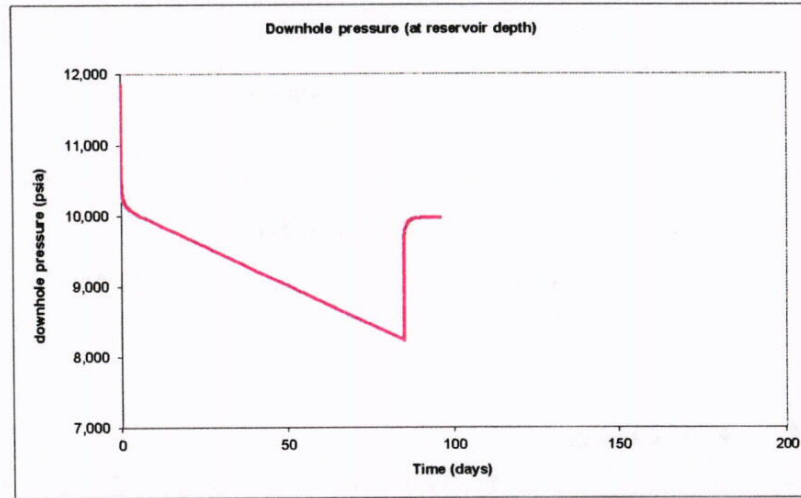


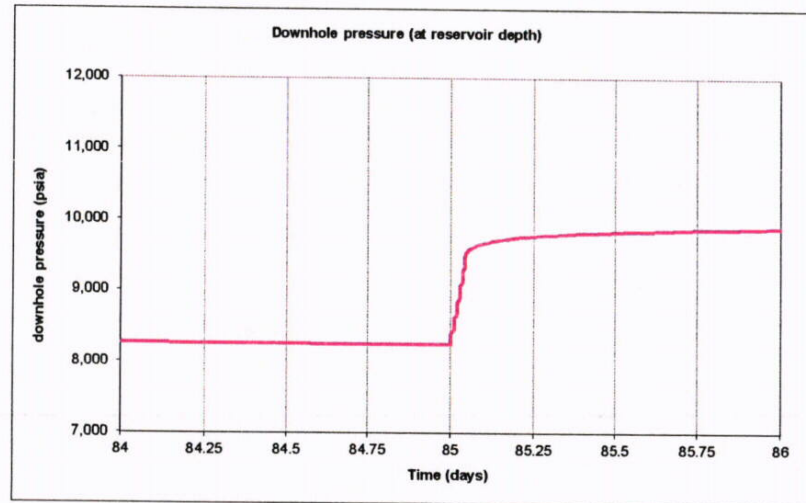
Chart1

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
1			down hole pressure																
2	days	days	aq = 0x																
3		0		11850															
4		0.00186824		10821															
5		0.00411014		10717															
6		0.00680041		10660															
7		0.01002873		10618															
8		0.01399272		10585															
9		0.01855151		10556															
10		0.02413006		10530															
11		0.03082432		10506															
12		0.03885743		10483															
13		0.04849716		10462															
14		0.06006484		10442															
15		0.07394605		10422															
16		0.09060351		10403															
17		0.11059245		10384															
18		0.1345792		10365															
19		0.16336329		10347															
20		0.1979042		10329															
21		0.23935328		10311															
22		0.28909218		10293															
23		0.34877887		10275															
24		0.42040291		10258															
25		0.50635177		10240															
26		0.60949039		10223															
27		0.73325676		10205															
28		0.88177639		10188															
29		1.05999994		10171															
30		1.2738682		10153															
31		1.53051019		10136															
32		1.83848059		10119															
33		2.20804501		10101															
34		2.6515224		10083															
35		3.18369508		10065															
36		3.82230258		10046															
37		4.58863163		10025															
38		5.50822839		10002															
39		6.61174811		9976															
40		7.93595648		9946															
41		9.52501678		9910															
42		11.43188858		9868															
43		13.72013474		9817															
44		16.46603012		9756															
45		19.76110458		9683															



downhole pressure

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
46	23.7151947			9596															
47	28.46010399			9491															
48	34.15399551			9365															
49	40.98666382			9214															
50	49.18586731			9033															
51	59.02490997			8815															
52	70.83176422			8554	dP (psia)	dT (day)													
53	84.39998474	0		8241	815	35.81411743													
54	85.00061635	0.000832		8399															
55	85.00164795	0.001663		8415															
56	85.00247955	0.002495		8423															
57	85.00331116	0.003326		8429															
58	85.00414276	0.004158		8432															
59	85.00497437	0.004990		8436															
60	85.00580597	0.005821		8438															
61	85.00663757	0.006653		8441															
62	85.00746918	0.007484		8443															
63	85.00830078	0.008316		8444															
64	85.00913239	0.009148		8605															
65	85.00996399	0.009979		8622															
66	85.01079559	0.010811		8631															
67	85.0116272	0.011642		8638															
68	85.0124588	0.012474		8643															
69	85.01329041	0.013306		8647															
70	85.01412201	0.014137		8651															
71	85.01495361	0.014969		8654															
72	85.01578522	0.015800		8657															
73	85.01661682	0.016632		8659															
74	85.01744843	0.017464		8920															
75	85.01828003	0.018295		8938															
76	85.01911163	0.019127		8948															
77	85.01994324	0.019959		8956															
78	85.02077484	0.020790		8961															
79	85.02160645	0.021622		8966															
80	85.02243805	0.022453		8970															
81	85.02326965	0.023285		8974															
82	85.02410126	0.024117		8978															
83	85.02493286	0.024948		8981															
84	85.02576447	0.025780		9042															
85	85.02659607	0.026611		9061															
86	85.02742767	0.027443		9071															
87	85.02825928	0.028275		9079															
88	85.02909088	0.029106		9085															
89	85.02992249	0.029938		9091															
90	85.03075409	0.030769		9095															
91	85.03158569	0.031601		9100															
92	85.0324173	0.032433		9103															
93	85.0332489	0.033264		9107															
94	85.03408051	0.034096		9269															
95	85.03491211	0.034927		9288															
96	85.03574371	0.035759		9299															
97	85.03657532	0.036591		9307															
98	85.03740692	0.037422		9313															
99	85.03823853	0.038254		9319															
100	85.03907013	0.039085		9324															
101	85.03990173	0.039917		9329															
102	85.04073334	0.040749		9333															
103	85.04156494	0.041580		9337															
104	85.04159783	0.041603		9438															
105	85.04161072	0.041626		9455															
106	85.04164124	0.041657		9465															
107	85.04167938	0.041695		9472															
108	85.04172516	0.041740		9478															
109	85.04177856	0.041794		9483															
110	85.04184723	0.041862		9487															

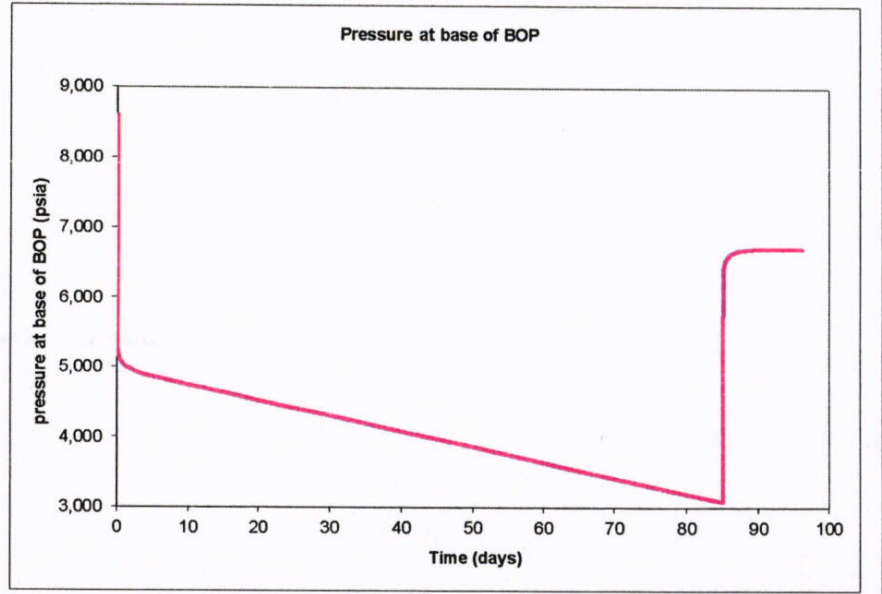


downhole pressure

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
111	85.04192352	0.041939		9492															
112	85.04201508	0.042030		9496															
113	85.04212952	0.042145		9500															
114	85.04226685	0.042282		9504															
115	85.04242706	0.042442		9508															
116	85.04262543	0.042641		9512															
117	85.04286194	0.042877		9516															
118	85.04314423	0.043159		9521															
119	85.04347992	0.043495		9525															
120	85.04388428	0.043900		9530															
121	85.04437256	0.044388		9535															
122	85.04496002	0.044975		9540															
123	85.04566193	0.045677		9545															
124	85.04650116	0.046516		9551															
125	85.04751587	0.047531		9557															
126	85.04872894	0.048744		9564															
127	85.05018616	0.050201		9571															
128	85.05193329	0.051949		9578															
129	85.05403137	0.054047		9586															
130	85.05654907	0.056564		9595															
131	85.05957031	0.059586		9604															
132	85.06319427	0.063210		9613															
133	85.06754303	0.067558		9623															
134	85.07276154	0.072777		9634															
135	85.07902527	0.079041		9645															
136	85.08654022	0.086555		9657															
137	85.09555817	0.095573		9669															
138	85.10637665	0.106392		9682															
139	85.11936188	0.119377		9695															
140	85.1349411	0.134956		9709															
141	85.15363312	0.153648		9723															
142	85.17606354	0.176079		9737															
143	85.20298767	0.203003		9751															
144	85.23529053	0.235306		9766															
145	85.27405548	0.274071		9781															
146	85.3205719	0.320587		9795															
147	85.37639618	0.376411		9810															
148	85.44338226	0.443398		9825															
149	85.52376556	0.523781		9839															
150	85.620224	0.620239		9854															
151	85.73597717	0.735992		9868															
152	85.87487793	0.874893		9881															
153	86.04156494	1.041580		9894															
154	86.09513092	1.095146		9898															
155	86.15940857	1.159424		9903															
156	86.23654175	1.236557		9907															
157	86.32910156	1.329117		9912															
158	86.44017792	1.440193		9918															
159	86.57346344	1.573479		9923															
160	86.73340607	1.733421		9929															
161	86.92533875	1.925354		9935															
162	87.15566254	2.155678		9941															
163	87.43204498	2.432060		9946															
164	87.76371002			9951															
165	88.16170502			9956															
166	88.63929749			9960															
167	89.21240997			9963															
168	89.90014648			9966															
169	90.72542572			9968															
170	91.71576691			9969															
171	92.9041748			9970															
172	94.33028123			9970															
173	95.04156494			9970															

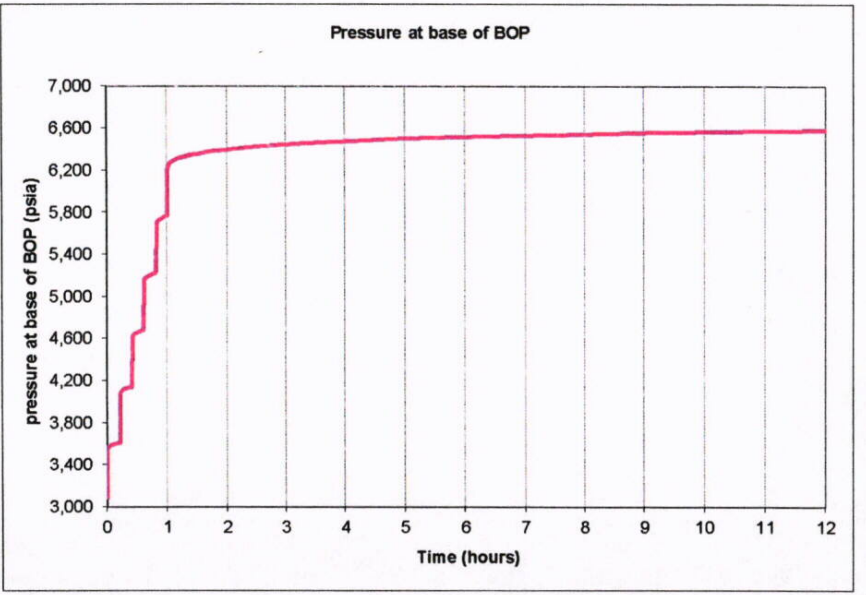
downhole pressure

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
1			pressure at base of BOP					rho_o =	568		dP =	3250		well loss =	1900				
2	days	days	aq = 0x	aq = 4x	aq = 14x														
3		0		8600		-5150													
4		0.00186824		5671															
5		0.00411014		5567															
6		0.00680041		5510															
7		0.01002873		5468															
8		0.01390272		5435															
9		0.01855151		5406															
10		0.02413006		5380															
11		0.03082432		5356															
12		0.03885743		5333															
13		0.04849716		5312															
14		0.06006484		5292															
15		0.07394605		5272															
16		0.09060351		5253															
17		0.11059245		5234															
18		0.1345792		5215															
19		0.16336329		5197															
20		0.1979042		5179															
21		0.23935328		5161															
22		0.28909218		5143															
23		0.34877887		5125															
24		0.42040291		5108															
25		0.50635177		5090															
26		0.60949039		5073															
27		0.73325676		5055															
28		0.88177639		5038															
29		1.05999994		5021															
30		1.2738882		5003															
31		1.53051019		4986															
32		1.83848059		4969															
33		2.20804501		4951															
34		2.6515224		4933															
35		3.18369508		4915															
36		3.82230258		4896															
37		4.58863163		4875															



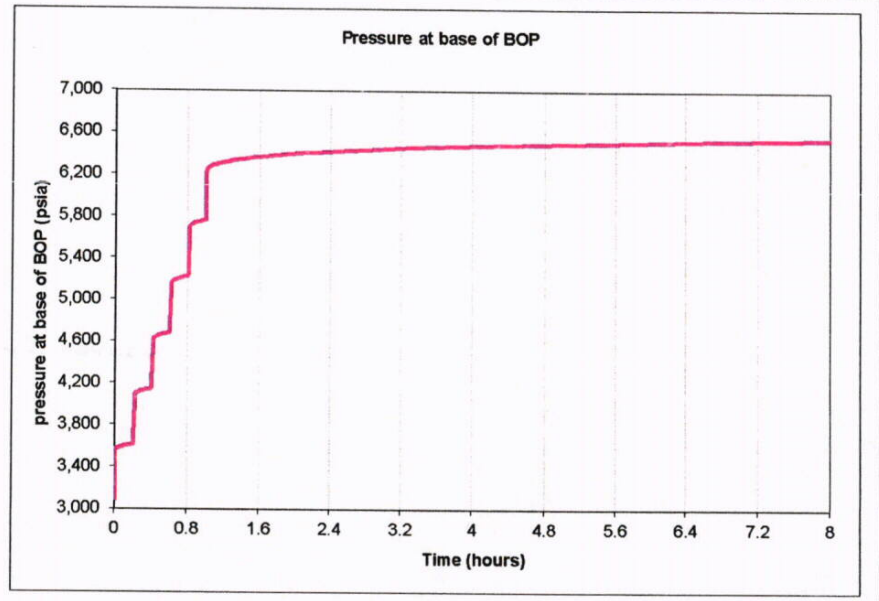
pressure at base of BOP

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
38	5.50822639			4852															
39	6.61174011			4826															
40	7.93595648			4796															
41	9.52501678			4760															
42	11.43188858			4718															
43	13.72013474			4667															
44	16.46603012			4606															
45	19.76110458			4533															
46	23.7151947			4446															
47	28.46010399			4341															
48	34.15399551			4215															
49	40.98666382			4064															
50	49.18586731			3883															
51	59.02490997			3665															
52	70.83176422	shutin hr		3404															
53	84.99998474	0		3081		7/15/2010 12:30													
54	85.00081635	0.00083		3566		7/15/2010 12:31													
55	85.00164795	0.040		3582		7/15/2010 12:32													
56	85.00247955	0.060		3590		7/15/2010 12:33													
57	85.00331116	0.080		3596		7/15/2010 12:34													
58	85.00414276	0.100		3599		7/15/2010 12:35													
59	85.00497437	0.120		3603		7/15/2010 12:37													
60	85.00580597	0.140		3605		7/15/2010 12:38													
61	85.00663757	0.160		3608		7/15/2010 12:39													
62	85.00746918	0.180		3610		7/15/2010 12:40													
63	85.00830078	0.200		3611		7/15/2010 12:41													
64	85.00913239	0.220		4088		7/15/2010 12:43													
65	85.00996399	0.240		4105		7/15/2010 12:44													
66	85.01079559	0.259		4114		7/15/2010 12:45													
67	85.0116272	0.279		4121		7/15/2010 12:46													
68	85.0124588	0.299		4126		7/15/2010 12:47													
69	85.01329041	0.319		4130		7/15/2010 12:49													
70	85.01412201	0.339		4134		7/15/2010 12:50													
71	85.01495361	0.359		4137		7/15/2010 12:51													
72	85.01578522	0.379		4140		7/15/2010 12:52													
73	85.01661682	0.399		4142		7/15/2010 12:53													
74	85.01744843	0.419		4620		7/15/2010 12:55													



pressure at base of BOP

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
75	85.01828003	0.439		4638		7/15/2010 12:56													
76	85.01911163	0.459		4648		7/15/2010 12:57													
77	85.01994324	0.479		4656		7/15/2010 12:58													
78	85.02077484	0.499		4661		7/15/2010 12:59													
79	85.02160645	0.519		4666		7/15/2010 13:01													
80	85.02243805	0.539		4670		7/15/2010 13:02													
81	85.02326965	0.559		4674		7/15/2010 13:03													
82	85.02410126	0.579		4678		7/15/2010 13:04													
83	85.02493286	0.599		4681		7/15/2010 13:05													
84	85.02576447	0.619		5159		7/15/2010 13:07													
85	85.02659607	0.639		5178		7/15/2010 13:08													
86	85.02742767	0.659		5188		7/15/2010 13:09													
87	85.02825928	0.679		5196		7/15/2010 13:10													
88	85.02909088	0.699		5202		7/15/2010 13:11													
89	85.02992249	0.719		5208		7/15/2010 13:13													
90	85.03075409	0.738		5212		7/15/2010 13:14													
91	85.03158569	0.758		5217		7/15/2010 13:15													
92	85.0324173	0.778		5220		7/15/2010 13:16													
93	85.0332489	0.798		5224		7/15/2010 13:17													
94	85.03408051	0.818		5702		7/15/2010 13:19													
95	85.03491211	0.838		5721		7/15/2010 13:20													
96	85.03574371	0.858		5732		7/15/2010 13:21													
97	85.03657532	0.878		5740		7/15/2010 13:22													
98	85.03740692	0.898		5746		7/15/2010 13:23													
99	85.03823853	0.918		5752		7/15/2010 13:25													
100	85.03907013	0.938		5757		7/15/2010 13:26													
101	85.03990173	0.958		5762		7/15/2010 13:27													
102	85.04073334	0.978		5766		7/15/2010 13:28													
103	85.04156494	0.998		5770 rate (psi/hr)		7/15/2010 13:29													
104	85.04158783	0.998		6188	760279	7/15/2010 13:29													
105	85.04161072	0.999		6205	30945	7/15/2010 13:29													
106	85.04164124	1.000		6215	13652	7/15/2010 13:29													
107	85.04167938	1.001		6222	7647	7/15/2010 13:30													
108	85.04172516	1.002		6228	5461	7/15/2010 13:30													
109	85.04177856	1.003		6233	3901	7/15/2010 13:30													
110	85.04184723	1.005		6237	2427	7/15/2010 13:30													
111	85.04192352	1.007		6242	2731	7/15/2010 13:30													



pressure at base of BOP

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
112	85.04201508	1.009	6246	1820	7/15/2010 13:30														
113	85.04212952	1.011	6250	1456	7/15/2010 13:30														
114	85.04226685	1.015	6254	1214	7/15/2010 13:30														
115	85.04242706	1.019	6258	1040	7/15/2010 13:31														
116	85.04262543	1.023	6262	840	7/15/2010 13:31														
117	85.04286194	1.029	6266	705	7/15/2010 13:31														
118	85.04314423	1.036	6271	738	7/15/2010 13:32														
119	85.04347992	1.044	6275	496	7/15/2010 13:32														
120	85.04388428	1.054	6280	515	7/15/2010 13:33														
121	85.04437256	1.065	6285	427	7/15/2010 13:33														
122	85.04496002	1.079	6290	355	7/15/2010 13:34														
123	85.04566193	1.096	6295	297	7/15/2010 13:35														
124	85.04650116	1.116	6301	298	7/15/2010 13:36														
125	85.04751587	1.141	6307	246	7/15/2010 13:38														
126	85.04872894	1.170	6314	240	7/15/2010 13:40														
127	85.05018616	1.205	6321	200	7/15/2010 13:42														
128	85.05193329	1.247	6328	167	7/15/2010 13:44														
129	85.05403137	1.297	6336	159	7/15/2010 13:47														
130	85.056854907	1.358	6345	149	7/15/2010 13:51														
131	85.05957031	1.430	6354	124	7/15/2010 13:55														
132	85.06319427	1.517	6363	103	7/15/2010 14:01														
133	85.06754303	1.621	6373	96	7/15/2010 14:07														
134	85.07276154	1.747	6384	88	7/15/2010 14:14														
135	85.07902527	1.897	6395	73	7/15/2010 14:23														
136	85.08654022	2.077	6407	67	7/15/2010 14:34														
137	85.09555817	2.294	6419	55	7/15/2010 14:47														
138	85.10637665	2.553	6432	50	7/15/2010 15:03														
139	85.11936188	2.865	6445	42	7/15/2010 15:21														
140	85.1349411	3.239	6459	37	7/15/2010 15:44														
141	85.15363312	3.688	6473	31	7/15/2010 16:11														
142	85.17606354	4.226	6487	26	7/15/2010 16:43														
143	85.20298767	4.872	6501	22	7/15/2010 17:22														
144	85.23529053	5.647	6516	19	7/15/2010 18:08														
145	85.27405548	6.578	6531	16	7/15/2010 19:04														
146	85.3205719	7.694	6545	13	7/15/2010 20:11														
147	85.37639618	9.034	6560	11	7/15/2010 21:32														
148	85.44338226	10.642	6575	9	7/15/2010 23:08														
149	85.52376556	12.571	6589	7	7/16/2010 1:04														
150	85.620224	14.886	6604	6	7/16/2010 3:23														
151	85.73597717	17.664	6618	5	7/16/2010 6:09														
152	85.87487793	20.997	6631	4	7/16/2010 9:29														
153	86.04156494	24.998	6644	3	7/16/2010 13:29														

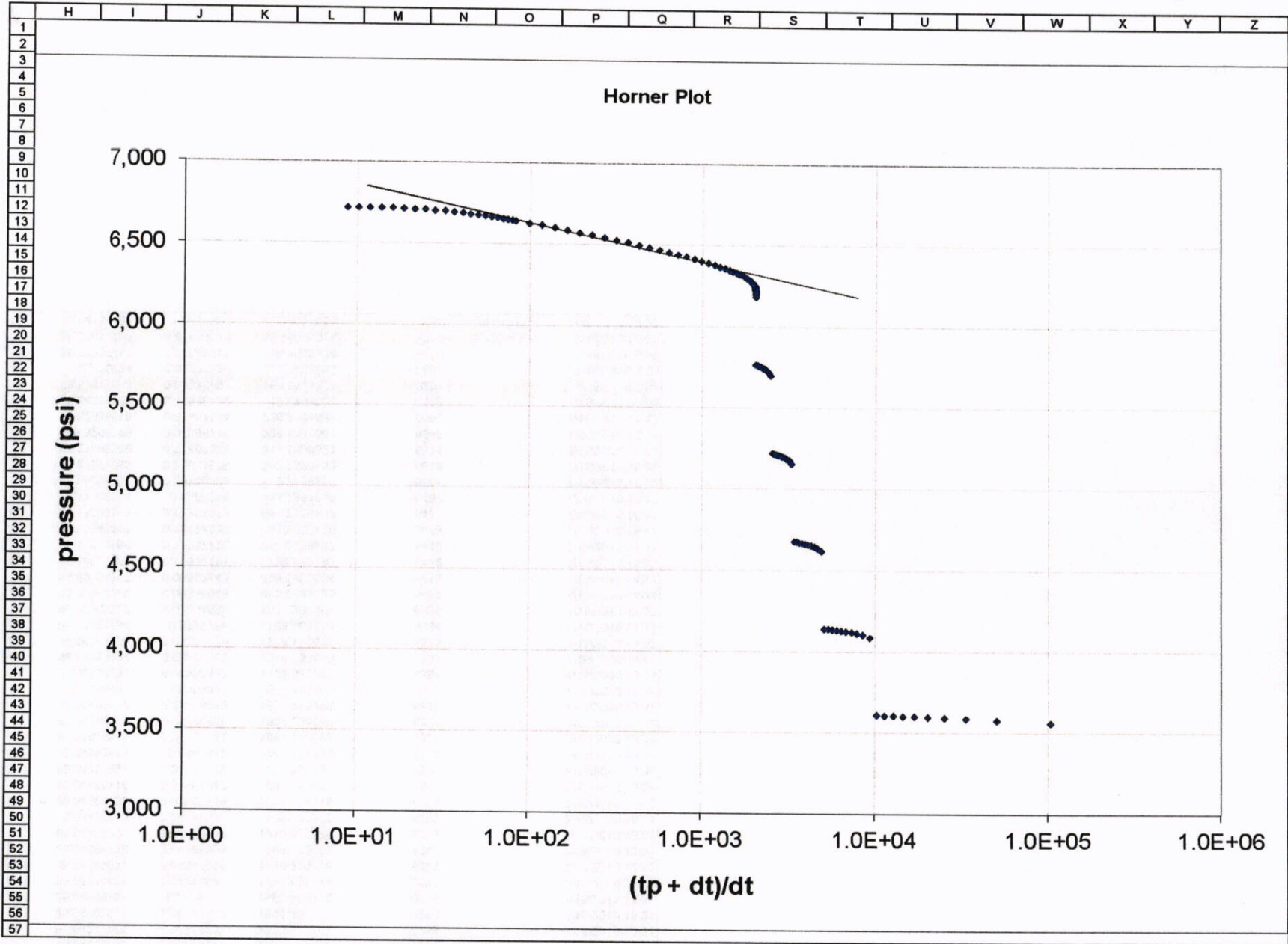
pressure at base of BOP

	A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S
154	86.09513092	28.284		6648															
155	86.15940857	27.828		6653															
156	86.23654175	29.677		6657															
157	86.32910156	31.899		6662															
158	86.44017792	34.585		6668															
159	86.57346344	37.763		6673															
160	86.73340607	41.802		6679															
161	86.92533875	46.208		6685															
162	87.15566254	51.736		6691															
163	87.43204498	58.369		6696															
164	87.76371002	66.329		6701															
165	88.16170502	75.881		6706															
166	88.63929749	87.344		6710															
167	89.21240997	101.098		6713															
168	89.90014648	117.604		6716															
169	90.72542572	137.411		6718															
170	91.71576891	161.179		6719															
171	92.9041748	189.701		6720															
172	94.33026123	223.927		6720															
173	96.04156494	264.998		6720															

pressure at base of BOP

	A	B	C	D	E	F	G
1	TP+dT	dT	(TP+dT)/dT	psi			
2	84.99998474			3091		7/15/2010 12:30	40374.5208333333
3	85.00081635	0.00083161	102212.3548	3565.666667		7/15/2010 12:31	40374.5216649433
4	85.00164795	0.00166321	51106.98466	3581.666667		7/15/2010 12:32	0.0008316100
5	85.00247955	0.00249481	34071.72472	3589.666667		7/15/2010 12:33	
6	85.00331116	0.00332642	25553.99233	3595.666667		7/15/2010 12:34	
7	85.00414276	0.00415802	20443.41844	3598.666667		7/15/2010 12:35	
8	85.00497437	0.00498963	17036.32822	3602.666667		7/15/2010 12:37	
9	85.00580597	0.00582123	14602.72244	3604.666667		7/15/2010 12:38	
10	85.00663757	0.00665283	12777.51537	3607.666667		7/15/2010 12:39	
11	85.00746918	0.00748444	11357.89307	3609.666667		7/15/2010 12:40	
12	85.00830078	0.00831604	10222.20922	3610.666667		7/15/2010 12:41	
13	85.00913239	0.00914765	9293.002289	4088.333333		7/15/2010 12:43	
14	85.00996399	0.00997925	8518.672645	4105.333333		7/15/2010 12:44	
15	85.01079559	0.01081085	7863.470087	4114.333333		7/15/2010 12:45	
16	85.0116272	0.01164246	7301.861222	4121.333333		7/15/2010 12:46	
17	85.0124588	0.01247406	6815.139481	4126.333333		7/15/2010 12:47	
18	85.01329041	0.01330567	6389.252883	4130.333333		7/15/2010 12:49	
19	85.01412201	0.01413727	6013.475162	4134.333333		7/15/2010 12:50	
20	85.01495361	0.01496887	5679.450327	4137.333333		7/15/2010 12:51	
21	85.01578522	0.01580048	5380.582439	4140.333333		7/15/2010 12:52	
22	85.01661682	0.01663208	5111.604611	4142.333333		7/15/2010 12:53	
23	85.01744843	0.01746369	4868.240815	4620		7/15/2010 12:55	
24	85.01828003	0.01829529	4647.003684	4638		7/15/2010 12:56	
25	85.01911163	0.01912689	4445.004474	4648		7/15/2010 12:57	
26	85.01994324	0.0199585	4259.836322	4656		7/15/2010 12:58	
27	85.02077484	0.0207901	4089.483689	4661		7/15/2010 12:59	
28	85.02160645	0.02162171	3932.233225	4666		7/15/2010 13:01	
29	85.02243805	0.02245331	3786.632708	4670		7/15/2010 13:02	
30	85.02326965	0.02328491	3651.432179	4674		7/15/2010 13:03	
31	85.02410126	0.02411652	3525.55432	4678		7/15/2010 13:04	
32	85.02493286	0.02494812	3408.069741	4681		7/15/2010 13:05	
33	85.02576447	0.02577973	3298.163498	5158.666667		7/15/2010 13:07	
34	85.02659607	0.02661133	3195.127642	5177.666667		7/15/2010 13:08	
35	85.02742767	0.02744293	3098.336354	5187.666667		7/15/2010 13:09	
36	85.02825928	0.02827454	3007.237581	5195.666667		7/15/2010 13:10	
37	85.02909088	0.02910614	2921.345492	5201.666667		7/15/2010 13:11	
38	85.02992249	0.02993775	2840.224215	5207.666667		7/15/2010 13:13	
39	85.03075409	0.03076935	2763.488799	5211.666667		7/15/2010 13:14	
40	85.03158569	0.03160095	2690.792071	5216.666667		7/15/2010 13:15	
41	85.0324173	0.03243256	2621.822554	5219.666667		7/15/2010 13:16	
42	85.0332489	0.03326416	2556.302306	5223.666667		7/15/2010 13:17	
43	85.03408051	0.03409577	2493.97742	5702.333333		7/15/2010 13:19	
44	85.03491211	0.03492737	2434.621104	5721.333333		7/15/2010 13:20	
45	85.03574371	0.03575897	2378.025533	5732.333333		7/15/2010 13:21	
46	85.03657532	0.03659058	2324.001842	5740.333333		7/15/2010 13:22	
47	85.03740692	0.03742218	2272.379827	5746.333333		7/15/2010 13:23	
48	85.03823853	0.03825379	2223.001656	5752.333333		7/15/2010 13:25	
49	85.03907013	0.03908539	2175.725255	5757.333333		7/15/2010 13:26	
50	85.03990173	0.03991699	2130.418695	5762.333333		7/15/2010 13:27	
51	85.04073334	0.0407486	2086.960861	5766.333333		7/15/2010 13:28	
52	85.04156494	0.0415802	2045.241844	5770.333333		7/15/2010 13:29	
53	85.04158783	0.04160309	2044.117104	6188		7/15/2010 13:29	
54	85.04161072	0.04162598	2042.9936	6205		7/15/2010 13:29	
55	85.04164124	0.0416565	2041.497515	6215		7/15/2010 13:29	
56	85.04167938	0.04169464	2039.630978	6222		7/15/2010 13:30	
57	85.04172516	0.04174042	2037.395052	6228		7/15/2010 13:30	

er Plot



Horner Plot

	A	B	C	D	E	F
58	85.04177856	0.04179382	2034.793148	6233		7/15/2010 13:30
59	85.04184723	0.04186249	2031.456973	6237		7/15/2010 13:30
60	85.04192352	0.04193878	2027.763409	6242		7/15/2010 13:30
61	85.04201508	0.04203034	2023.348255	6246		7/15/2010 13:30
62	85.04212952	0.04214478	2017.856767	6250		7/15/2010 13:30
63	85.04226685	0.04228211	2011.306126	6254		7/15/2010 13:30
64	85.04242706	0.04244232	2003.717682	6258		7/15/2010 13:31
65	85.04262543	0.04264069	1994.400781	6262		7/15/2010 13:31
66	85.04286194	0.0428772	1983.405212	6266		7/15/2010 13:31
67	85.04314423	0.04315949	1970.439044	6271		7/15/2010 13:32
68	85.04347992	0.04349518	1955.239176	6275		7/15/2010 13:32
69	85.04388428	0.04389954	1937.23862	6280		7/15/2010 13:33
70	85.04437256	0.04438782	1915.939385	6285		7/15/2010 13:33
71	85.04496002	0.04497528	1890.92675	6290		7/15/2010 13:34
72	85.04566193	0.04567719	1861.884716	6295		7/15/2010 13:35
73	85.04650116	0.04651642	1828.311404	6301		7/15/2010 13:36
74	85.04751587	0.04753113	1789.301367	6307		7/15/2010 13:38
75	85.04872894	0.0487442	1744.796898	6314		7/15/2010 13:40
76	85.05018616	0.05020142	1694.178893	6321		7/15/2010 13:42
77	85.05193329	0.05194855	1637.234019	6328		7/15/2010 13:44
78	85.05403137	0.05404663	1573.715722	6336		7/15/2010 13:47
79	85.05654907	0.05656433	1503.713543	6345		7/15/2010 13:51
80	85.05957031	0.05958557	1427.519621	6354		7/15/2010 13:55
81	85.06319427	0.06320953	1345.733693	6363		7/15/2010 14:01
82	85.06754303	0.06755829	1259.172531	6373		7/15/2010 14:07
83	85.07276154	0.07277768	1168.954413	6384		7/15/2010 14:14
84	85.07902527	0.07904053	1076.397454	6395		7/15/2010 14:23
85	85.08654022	0.08655548	983.0289223	6407		7/15/2010 14:34
86	85.09555817	0.09557343	890.3683604	6419		7/15/2010 14:47
87	85.10637665	0.10639191	799.932783	6432		7/15/2010 15:03
88	85.11936188	0.11937714	713.0289927	6445		7/15/2010 15:21
89	85.1349411	0.13495636	630.833116	6459		7/15/2010 15:44
90	85.15363312	0.15364838	554.2110702	6473		7/15/2010 16:11
91	85.17606354	0.1760788	483.7383236	6487		7/15/2010 16:43
92	85.20298767	0.20300293	419.7130932	6501		7/15/2010 17:22
93	85.23529053	0.23530579	362.2320153	6516		7/15/2010 18:08
94	85.27405548	0.27407074	311.1388523	6531		7/15/2010 19:04
95	85.3205719	0.32058716	266.1384564	6545		7/15/2010 20:11
96	85.37639618	0.37641144	226.8166881	6560		7/15/2010 21:32
97	85.44338226	0.44339752	192.701534	6575		7/15/2010 23:08
98	85.52376556	0.52378082	163.2815909	6589		7/16/2010 1:04
99	85.620224	0.62023926	138.0438639	6604		7/16/2010 3:23
100	85.73597717	0.73599243	116.4902976	6618		7/16/2010 6:09
101	85.87487793	0.87489319	98.15469924	6631	0.13890076	7/16/2010 9:29
102	86.04156494	1.0415802	82.60675936	6644	0.16668701	7/16/2010 13:29

er Plot

	A	B	C	D	E	F
103	86.09513092	1.09514618	78.61519539	6648	0.05356598	7/16/2010 14:47
104	86.15940857	1.15942383	74.31226299	6653	0.06427765	7/16/2010 16:19
105	86.23654175	1.23655701	69.73923649	6657	0.07713318	7/16/2010 18:10
106	86.32910156	1.32911682	64.95223013	6662	0.09255981	7/16/2010 20:23
107	86.44017792	1.44019318	60.0198495	6668	0.11107636	7/16/2010 23:03
108	86.57346344	1.5734787	55.02042286	6673	0.13328552	7/17/2010 2:15
109	86.73340607	1.73342133	50.03596331	6679	0.15994263	7/17/2010 6:06
110	86.92533875	1.92535401	45.14771741	6685	0.19193268	7/17/2010 10:42
111	87.15566254	2.1556778	40.43074644	6691	0.23032379	7/17/2010 16:14
112	87.43204498	2.43206024	35.94978592	6696	0.27638244	7/17/2010 22:52
113	87.76371002	2.76372528	31.75558391	6701	0.33166504	7/18/2010 6:49
114	88.16170502	3.16172028	27.88409385	6706	0.397995	7/18/2010 16:22
115	88.63929749	3.63931275	24.3560539	6710	0.47759247	7/19/2010 3:50
116	89.21240997	4.21242523	21.17839608	6713	0.57311248	7/19/2010 17:35
117	89.90014648	4.90016174	18.34636309	6716	0.68773651	7/20/2010 10:06
118	90.72542572	5.72544098	15.84601536	6718	0.82527924	7/21/2010 5:54
119	91.71576691	6.71578217	13.6567513	6719	0.99034119	7/22/2010 5:40
120	92.9041748	7.90419006	11.75378807	6720		7/23/2010 10:12
121	94.33026123	9.33027649	10.11012496	6720		7/24/2010 20:25
122	96.04156494	11.0415802	8.698172109	6720		7/26/2010 13:29

