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REVIEW OF THE PRODUCTION CASING DESIGN FOR THE MACONDO WELL

Prepared For
BP

Expert Report
by
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Summary of Opinions

I was asked to conduct an engineering review of the basis of design for the long string production casing installed at the Macondo well. I was also asked to review an alternative liner and tieback production casing design proposed for the Macondo well.

It is my opinion that there is no technical basis to challenge the design of the production casing for the Macondo well with regard to BP's decision to install a long string design option over a liner and tieback design option.

This report demonstrates that the use of a long string versus a liner and tieback will produce design results with very similar Factors of Safety and both are appropriate designs consistent with industry engineering standards and practices. While both designs are appropriate and reasonable for the application, in my opinion, the long string is the better design option with regard to loads placed on the production casing. My opinion is based on the fact that the liner and tieback design option guarantees there will be an Annular Pressure Buildup (APB) design issue in the B annulus; while a long string design option has a much lower probability of an APB design issue. The liner and tieback option APB pressure could be high enough to cause the production casing to collapse and compromise the integrity of the well bore once the well is producing. However because BP installed rupture disks in the 16" casing designed to mitigate the anticipated APB either a long string or a liner and tieback option would have been appropriate.

From a long term integrity standpoint the use of a long string design has benefits in a producing well as compared to a liner and tieback design, given the absence of a potential failure point at the liner and tieback interface (This is because the long string design does not have a seal assembly and a polished bore receptacle, while the liner and tieback does have this additional interface).

Designing production casing as a long string is a common and an acceptable practice in the Gulf of Mexico. BP has been criticized for using a long string in the Macondo well and allegedly putting cost before safety in its choice of the production casing design. In my opinion, BP's choice to use a production long string is consistent with good engineering practice, is consistent with industry practice, and is consistent with production casing strings installed in deepwater wells in the Gulf of Mexico. I hold that opinion based on my experience, this analysis and the statistics available in this case.

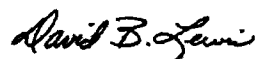
BP, in its Deepwater Horizon Accident Investigation report stated that a long string production design was far from abnormal in the area of the Gulf of Mexico around Block MC252 where BP was drilling. In fact, 57% of the 113 wells in a 10 by 10 lease block grid around MC252 used a production casing design similar to that employed by BP on the Macondo well [1]. Additionally, I have reviewed the testimony of MMS (now BOEMRE) regulators, who agree that a long string production casing is a common practice in the Gulf of Mexico. It is my understanding that the United States produced a chart showing more than 100 long string designs that Minerals Management Service approved in the Gulf of Mexico [2].

In addition, I reviewed Mr. Pritchard's expert report and his assertion that the installation of the rupture disks in the 16" casing could have compromised the post-incident well kill operation.

Installation of rupture disks is a common industry practice and is appropriate well design. It is my opinion that although individuals may have thought rupture disks would limit the kill operations, the rupture disks in fact had a higher burst rating than the 16" casing and the Hydril connections on the 16" casing. The rupture disks were not a weak link in the system.

This opinion is based on the information that has been provided to me for review. I reserve the right to adjust my opinion upon review of any additional documents or information previously unavailable to me.

Submitted 17 October 2011



David B. Lewis

Qualifications

I have over thirty years of domestic and international experience in oil & gas exploration and production. I have a management and a functional background in drilling, completions, offshore structures and a strong engineering background with experience in deepwater, big bore (mono bore) and high pressure-high temperature wells. I have specific expertise in technology management, deepwater drilling, High Pressure / High Temperature (HPHT) wells, reliability based design, tubulars, connections, marine drilling risers, conductors, pipelines, offshore structures, down-hole equipment, project management, training and finite element analysis. I am the CEO and President of Blade Energy Partners. I am a Registered Professional Engineer in the State of Texas, a member of the American Society of Civil Engineers (ASCE), a member of the Society of Petroleum Engineers (SPE), and serve on numerous American Petroleum Institute (API) and International Organization for Standardization (ISO) committees as summarized below:

API – American Petroleum Institute

- API Executive Board Member of Committee 5 – Tubular Goods
- Chairman API RP 5-EX Resource Group on Solid Expandable Development
- Chairman API Resource Group on Tubular Properties Software Development
- Technical Member of API 5CT - Specifications for Casing and Tubing
- Technical Member of API TR 5C3 - Bulletin on Formulas and Calculations for Casing, Tubing, Drill Pipe, and Line Pipe Properties

- API Executive Board Member of Committee 16 - Drilling Well Control Equipment
- Chairman 16Q - Recommended Practice for Design, Selection, Operation and Maintenance of Marine Drilling Riser Systems
- Chairman 16R - Specification for Marine Drilling Riser Couplings
- Technical Member of API 16F – Specification for Marine Drilling Riser Equipment
- Technical Member of API RP 6HP (PER 15K) - Greater than 15 ksi Equipment
- Technical Member API RP 96 – Deepwater Design Considerations

ISO – International Standardization Organization

- Technical Member WG2A and WG2B for ISO TR 10400 - Petroleum and natural gas industries — Equations and calculations for the properties of casing, tubing, drill pipe and line pipe used as casing or tubing

I have designed dozens of deepwater wells in multiple areas around the world and have been involved with numerous failure analysis and post well reviews. I have authored or co-authored over 20 industry papers. My education includes a BS degree and MS degree in Civil Engineering from University of Missouri-Rolla; and postgraduate doctoral work in finite element methods, continuum mechanics, vibrations, and structural dynamics. A copy of my resume is attached to this report as Exhibit A.

In the past five years I have been involved in three cases as an expert witness. They were:

1. Weatherford International, Inc., and Weatherford / Lamb, Inc., (Plaintiff) versus CaseTech International, Inc., (Defendant) in The United States District Court for the



Southern District of Texas, Houston Division, Civil Action No. H-03-5383. Served as expert witness for CaseTech. Settled out of court August 2008.

2. Testified to the Government of Colombia on the behalf of Tenaris with regard to tubular dumping by the Chinese in Colombia.
3. RoundTree and Associates, et.al., (Plaintiff) versus V&M Star (Defendant) in The United States District Court for the Southern District of Mississippi Jackson Division. Civil Action No. 3:08cv572 DPJ-JCS. Served as expert witness for V&M Star. Settled out of court November 2010.

Exhibit B details the rates, compensation and terms for my services. My compensation is in no way connected with the outcome of this suit.

Exhibit C contains the materials referenced in this report as well as consideration materials provided to Blade Energy Partners. References in this report text are denoted by a number in brackets [#].

Introduction - Problem Statement

This report addresses the design considerations of the Macondo well (Mississippi Canyon Block 252 – MC252) with production casing set as a “long string” versus a well with production casing set as a “liner and tieback”. I have seen both design options used in the Gulf of Mexico for deepwater and shallow water wells by numerous different operators.

In order to understand the engineering basis of a design review, there are a few fundamental points about well design that need to be explained.

At the most basic, the production casing is the inner-most casing string of pipe in any well. Figure 1 shows two typical wellbore schematics for deepwater subsea wells – one with a long string of production casing and one with a liner and tieback production casing. As one can see each string of casing is set inside of the previous casing string as the well gets deeper and deeper. Each string of casing has a name as detailed in the figure. Once a well is prepared for production, the operator installs the innermost pipe – the “production tubing.” The production tubing is the tubular through which the hydrocarbons flow up to the surface during production. For the Macondo well, production tubing would have been installed at some point in the future, after the temporary abandonment and before production. The well schematics in Figure 1 have some of the completion equipment installed (production tubing, packer, polished bore receptacle and perforations) for illustration.

The difference between a long string of production casing and a liner and tieback production casing is shown in Figure 1. A long string of production casing is a continuous pipe from the wellhead to the casing shoe (bottom of the casing). A production casing liner with a production casing tieback is casing which is installed into the well in two separate pipe sections with the liner being installed first and the tieback being installed second. The production casing tieback can be installed immediately after the production casing liner has been installed or installed at a later date.

As discussed in the next sections, the design analysis for both the long string and a liner with a tieback is the same – an operator must design production casing that can withstand the anticipated loads created during production. Those loads are complex and there are a number of different forces and pressures that must be analyzed. A production casing can fail in two different failure modes, both based on differential pressure in the annulus and in the interior of the casing. If the differential pressure from the interior to the annulus is sufficiently high, then the casing will “burst” and fail outward. If the differential pressure from the annulus to the interior is sufficiently high, then the casing will “collapse” and fail inward. Those differential pressures and how they are created and addressed during design are discussed further in the next sections. The annulus which is formed between the production tubing and production casing is called the ‘A’ annulus and the annulus which is formed between the production casing and drilling casing is the ‘B’ annulus. Each of these is labeled in Figure 1.

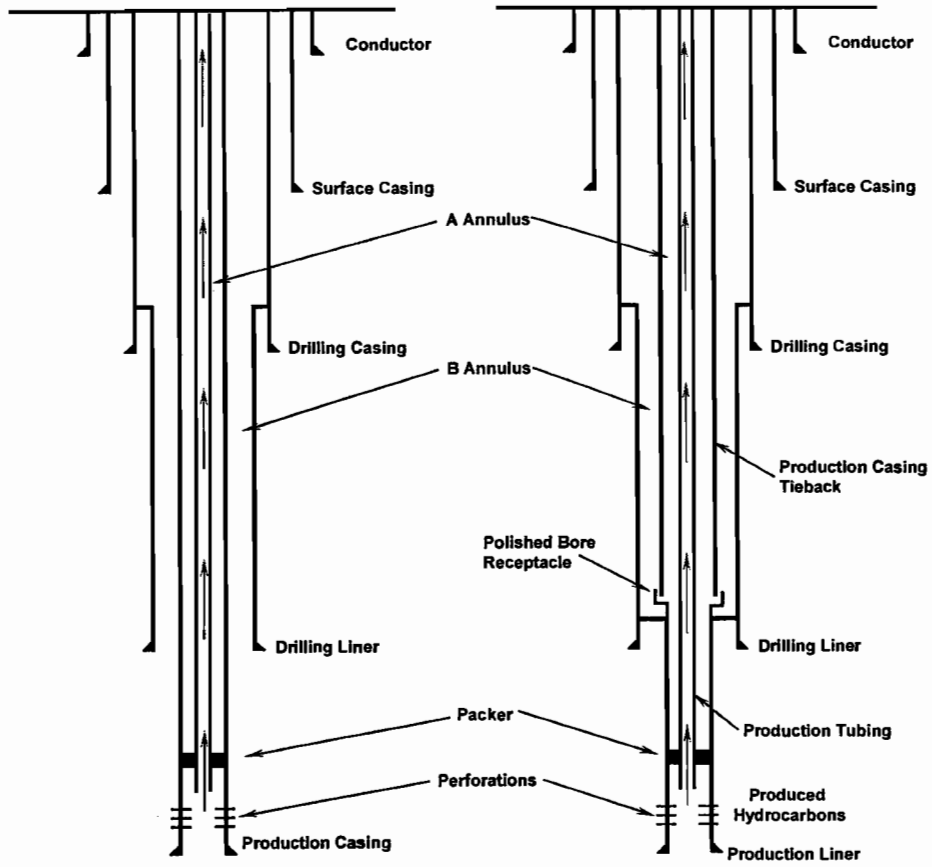


Figure 1. Long String (Left) and Liner and tieback (Right) Wellbore Schematics.

Design Requirements for Production Casing

The goal in production casing design is for the production casing to safely withstand all the anticipated loads that are likely to be placed on the production casing during its intended service life. The anticipated load placed on the production casing should not exceed the strength of the casing resisting that particular load type. This can be stated in a basic design formula as follows:

$$\text{Strength} \geq \text{Load} \quad (\text{Eq.1})$$

Design is really as simple as this equation. The challenge comes from appropriately analyzing the Load side of the equation. One can rewrite this equation so it can be used to determine the degree which Strength is greater than Load. This degree which Strength is greater than Load is the Factor of Safety and is defined by the following equation:

$$\text{Factor of Safety} = \text{Strength} / \text{Load} \quad (\text{Eq. 2})$$

Every design approach postulates a design check that ensures that the design strength exceeds the design load (or more specifically, the load effect) under various loading scenarios (kicks, lost returns, tubing leak, abandonment, etc.). In order to do this, of course, one needs a theory of strength, a design check based on an appropriate failure criterion and an estimate of the load itself.

Strength is calculated from strength-defining properties of the pipe which are dimensions and material properties. These coupled with an appropriate design model (i.e., equation) estimates the strength or resistance to a given type of load. Typical strength defining properties of casing are yield strength, pipe diameter, pipe wall thickness, ovality, eccentricity, tensile strength and material toughness.

Determining the proper value of the *Load* is more challenging. The Oil and Gas Industry has done an excellent job of defining and standardizing the Strength side of Equation 1 but has not standardized the Load definition of Equation 1 or the required Factor of Safety in Equation 2. There have been considerable post Macondo efforts to address these design issues but prior to the Macondo incident there was virtually no uniform Industry guidance on Load definitions or required Factors of Safety to be used in designs. Each oil and gas operator was (and still is) allowed to set his own Loads and Factor of Safety requirements.

For production casing, there are both burst and collapse loads that must be accounted for during the productive life of the well. There are three major different governing loads that operators consider when designing production casing. The loads on the production casing arise because of the differential pressures that can result from unanticipated equipment failure either early or late in the well's life and temperature and pressure changes resulting from producing hydrocarbons from the reservoir. These loads are modeled to calculate the most significant stresses that the production casing will reasonably see during its life. If these loads are properly evaluated, the Factor of Safety will be sufficiently high to predict a successful casing design.

Load 1 - Burst Load From Unanticipated Tubing Leak

For production casing the governing burst load condition is tubing leak. Tubing leak is an accidental load condition where a leak has formed in the production tubing string at the top of the well. The operator does everything it can to prevent this, but still include it in the design process as the differential pressures resulting from a tubing leak can be significant. If a leak occurs in the production tubing that means that one of the two mechanical barriers is assumed to have been lost for this load case (production tubing and production casing are the two mechanical barriers) and the well must be shut-in and repaired. When the well is shut-in this places pressure (called the Shut-In Tubing Pressure) on the A annulus, which is the annulus between the production tubing and production casing. The differential pressure between the production tubing and production casing creates a burst load on the production casing, meaning that the production casing may fail outward. The fluid in the A annulus is called packer fluid and its density is used to calculate the burst load on the production casing. This is the critical burst load the designer must consider in the design of production casing as the casing must be strong enough to withstand this load. See Figure 2.

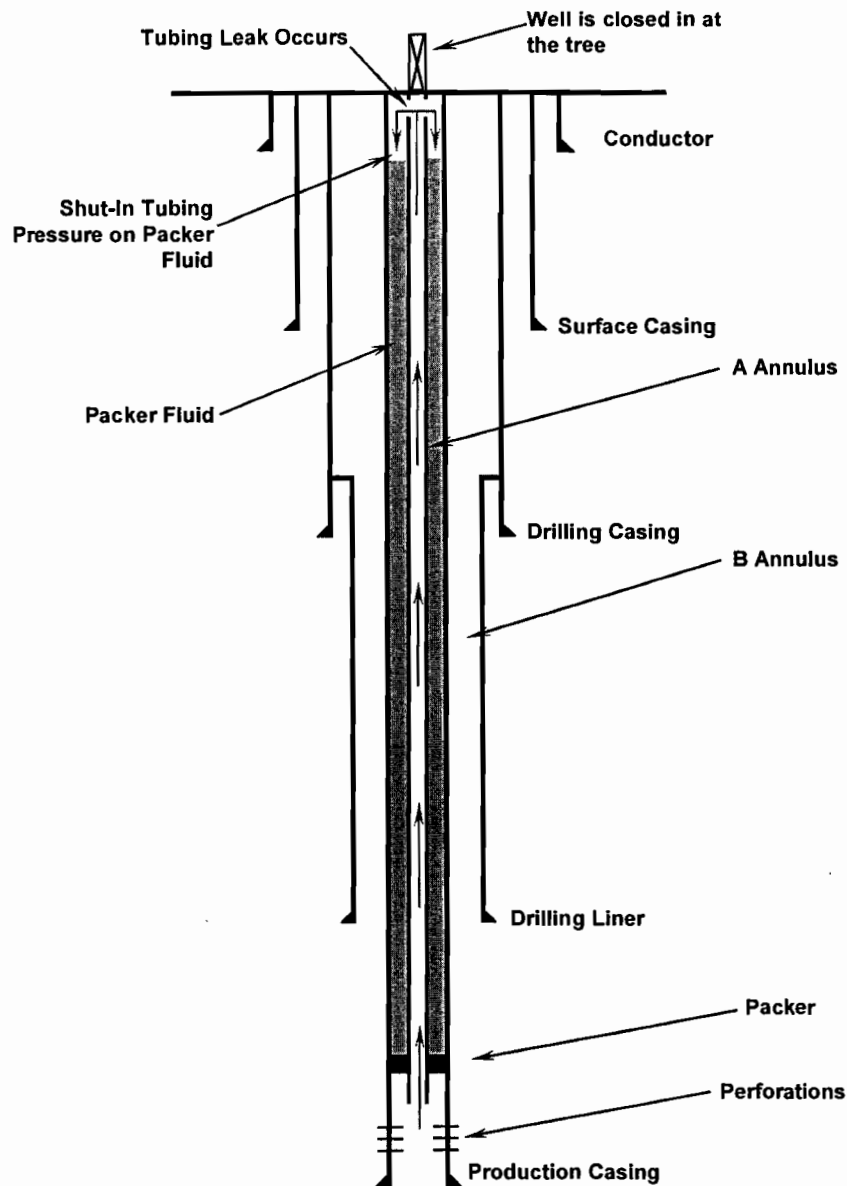


Figure 2. Tubing Leak Load Condition.

Load 2 – Loads During Production

One of the governing collapse load conditions for production casing is Annular Pressure Buildup (APB). This load condition occurs when the well starts producing hydrocarbons. The wellbore heats up due to high temperature hydrocarbons being produced through the production tubing. As the hot hydrocarbons are produced through the production tubing, they heat the surrounding casing strings as well as the fluids in the surrounding annuli (spaces between the casing strings). Any fluid trapped fluid in an annular space will try to expand and will exert significant pressure on the surrounding casing strings. Since the fluid is in a confined space there can be

a large pressure increase unless some type of APB mitigation (relief) is designed into the annulus.

The APB risks for the production casing is that fluid trapped in the B annulus heats and tries to expand. In a confined space the heating of the fluid will increase the pressure in the B annulus and may cause the production casing to collapse or may cause the outer string of drilling casing to burst. Therefore, the casing design needs to account for APB risks in two directions – either that the production casing will collapse (inward failure) or the exterior string will burst (outward failure).

APB risks of subsea wells are well known in the Gulf of Mexico and globally. There are a few methods of APB mitigation. Different operators have different mitigation methods, but the most common include design calibrated rupture disks, compressible fluids inserted in the annuli, vacuum insulated tubing, crushable foams, selecting stronger tubulars for the casing strings and designing to have open annuli (open shoes).

Load 3 – End of Life Loads

The final load condition which the well designer must address is an end of well life situation. This load condition is called abandonment collapse. In this load condition the well has been producing for many years and the reservoir pressure has decreased considerably since it was first completed. There is no longer a high pressure flow from the reservoir to the surface and pressures on the outside of the production casing can exceed the internal pressures. In this load case it is assumed the packer (completion equipment at the bottom of the production casing) fails and leaks the packer fluid into the reservoir. The abandonment reservoir pressure then balances the packer fluid hydrostatic height, placing more pressure outside the upper portion of the production casing than inside the production casing. This load condition places a collapse load on the production casing and, while it is only a concern late in the life of the well, it is accounted for in the initial design. See Figure 3.

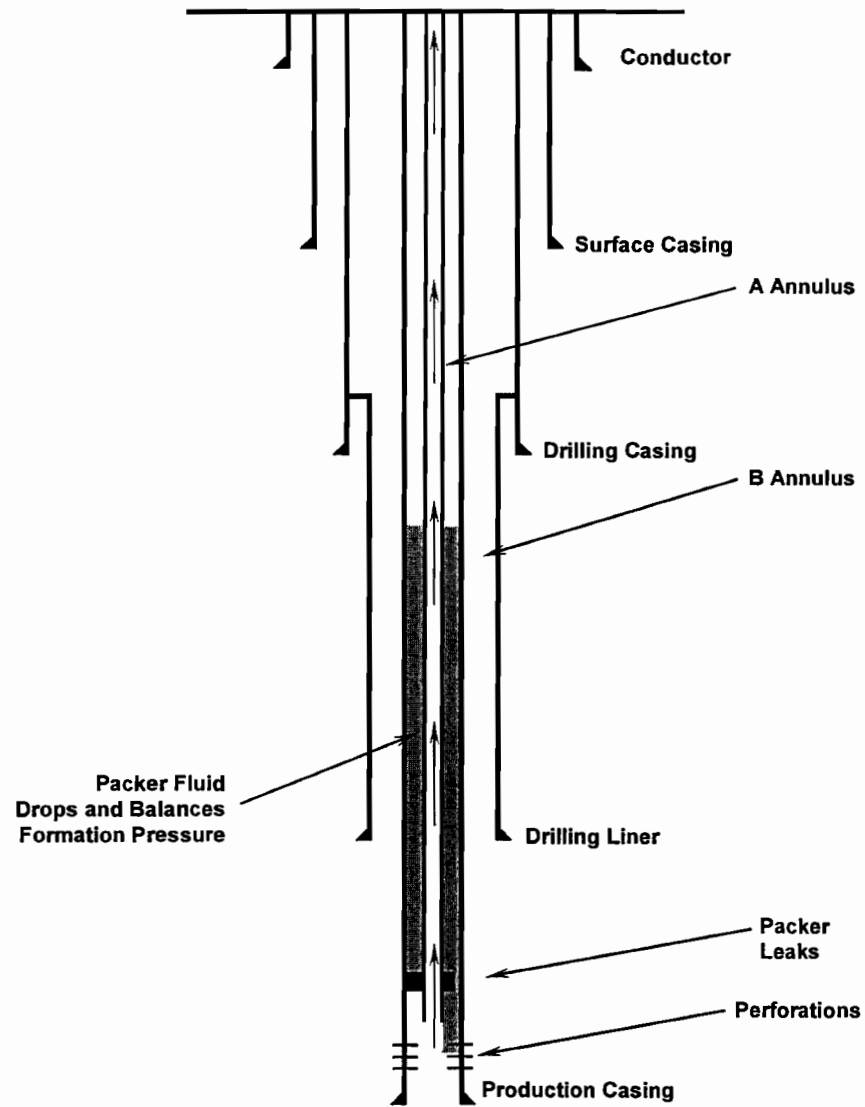


Figure 3. Abandonment Collapse Load Condition.

Macondo Production Casing Design

Following the above general background in the design criteria of production casing, I turn now to the Macondo production casing design.

Figure 4 is a sketch of the Macondo wellbore diagram from the Macondo Application for Revised Bypass [3]. This well schematic shows that the well has been side-tracked and details the various casing strings (size, weight and grade), pore pressures, fracture gradients, temperatures and cement tops along with the shoe depth at which each casing string is set.

I note that the original design for the Macondo well when it was originally proposed in 2009 involved seven casing strings [4]. However, as drilling operations occurred, the design was revised to account for the fact that BP had to set casing strings shallower than anticipated and as a result of a sidetrack that was required after the drill pipe and bottom hole assembly was stuck in the wellbore.

It is not surprising to me that the final, as run casing program utilized more casing strings than the original design proposal. It is common during deepwater drilling to encounter conditions that require changes to the casing program. In fact, a new technology has been developed over the past 10+ years to address the very issue of additional casing strings called Solid Expandables.

While a sidetrack is not desirable, it is not uncommon in the Gulf of Mexico. BP recognized the possibility of design changes from its earliest design, as BP always included a “contingency liner” in its plans [4]. As the casing design changed during drilling, BP’s casing design was subjected to repeated analysis and evaluation by its internal “EPT” team. I reviewed four of the BP EPT Evaluation of Casing Basis of Design reports, but my report focuses on the final version [5]. I agree with the conclusion of that report that the production casing run at the Macondo well had a sufficient Factor of Safety per Industry and BP practices and was an appropriate design.

In addition to the EPT team’s analysis of the casing design, BP submitted its casing designs to the MMS (now BOEMRE) for approval. It is my experience that the MMS uses the same design formula (Eq. 1) I analyzed here – whether the strength appropriately exceeds the load values. As I indicated above, prior to the Macondo incident (and in fact, still today), there are no industry accepted Factors of Safety or load definitions and the MMS had its own internal values for loads and Factors of Safety. The MMS will only approve casing designs if the design satisfies its independent review of the Strength > Load equation (Eq. 1). In this case, the MMS approved the production long string design proposed by BP [3].

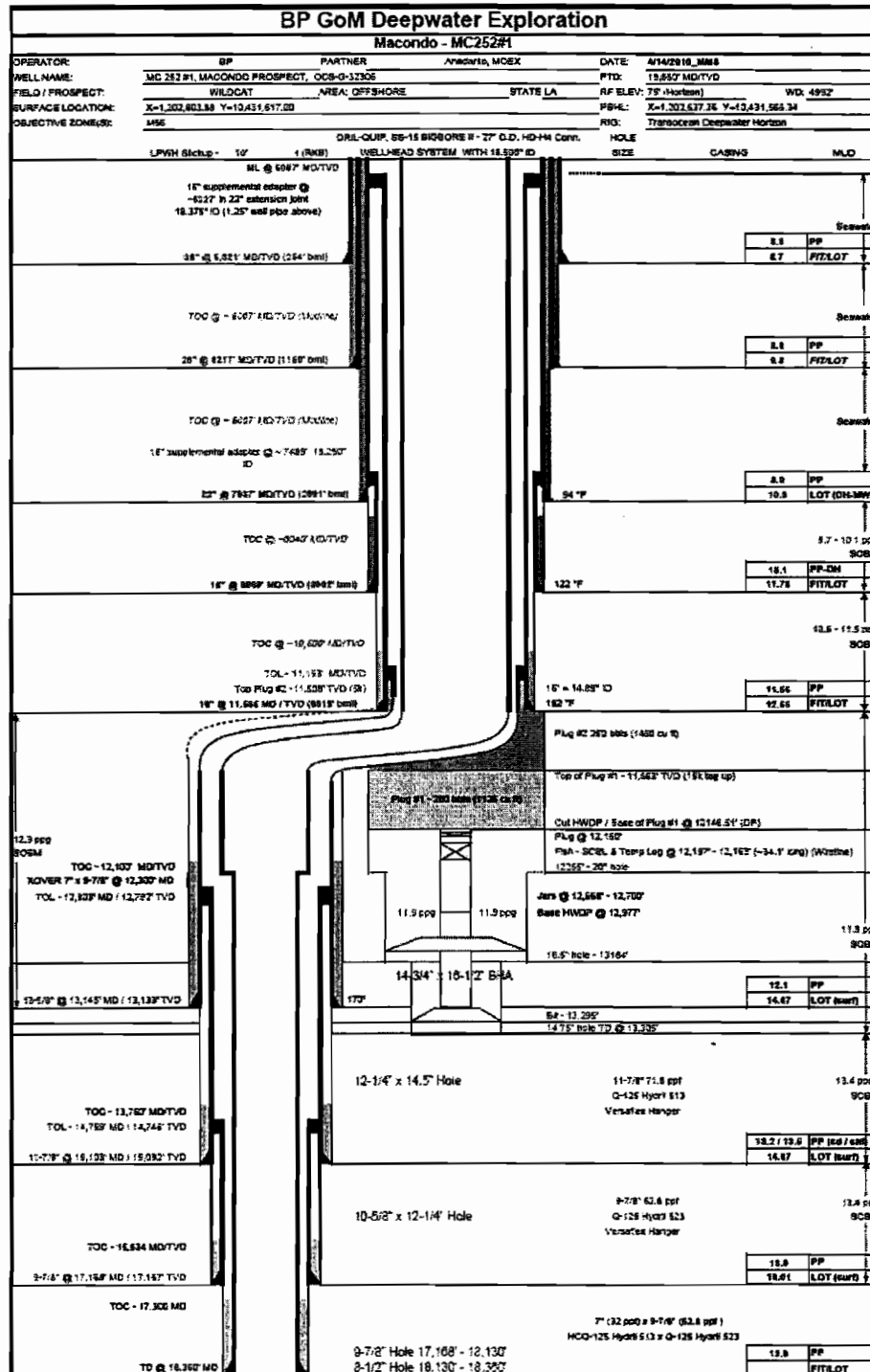


Figure 4. Macondo Wellbore Configuration from the APB.

Long String Design Results

My analysis of the Macondo long string production casing design shows that it was an appropriate design and had appropriate Factors of Safety for the governing anticipated loads. This discussion first outlines the conclusion of BP's EPT evaluation of casing design report [5] and then provides a summary of Blade's independent analysis.

Using BP's Macondo report [5] on the design of the production casing one can summarize the following Factors of Safety for the production casing for the long string design option. The production casing is a continuous string of pipe from the wellhead to the end of the well. It is comprised of 9-7/8" 62.80 lb/ft Q125 by 7" 32 lb/ft C110.¹

Table 1 details the minimum Factors of Safety from the BP design report.

	Factor Of Safety in 9-7/8" for Burst / Collapse	Factor Of Safety in 9-7/8" for VME ²	Factor of Safety in 7" for Burst / Collapse	Factor of Safety in 7" for VME
Tubing Leak (11060 psi shut-in tubing pressure) [6]	1.47	1.65	1.86	1.31
Abandonment Collapse (4955 psi abandonment pressure)	not reported	not reported	1.21	1.82

Table 1. BP's Minimum Factors of Safety Calculations for the Long String.

Blade modeled the Macondo well as detailed in the Application for Revised Bypass document [3] and shown in Figure 4. Blade used Landmark's (a Halliburton company) programs named WellCat and StressCheck to perform these calculations. These are the same programs used by BP. In addition Blade used its own in-house software tools to check the WellCat and StressCheck program results. Figure 5 shows the long string design modeled with WellCat. The model in Figure 5 is an output from the WellCat program and while it shows a rough schematic of the well design, the inputs and analysis conducted through WellCat are sophisticated.

Table 2 details the minimum Factors of Safety obtained by Blade from WellCat and Blade's own in-house program. The results are identical between the two computer programs. As one can see the results are comparable to Table 1.

¹ 62.80 lb/ft and 32 lb/ft is a measure of the weight of the casing and is a direct reflection of the wall thickness. Q125 and C110 are API grades and represent the material strengths.

² VME is Von Mises Equilivant and represents the state of stress in the casing.

	Factor Of Safety in 9-7/8" for Burst / Collapse	Factor Of Safety in 9-7/8" for VME	Factor of Safety in 7" for Burst / Collapse	Factor of Safety in 7" for VME
Tubing Leak (11060 psi shut-in tubing pressure burst load)	1.47	1.59	1.42	1.45
Abandonment Collapse (4955 psi abandonment pressure collapse load)	1.48	2.05	1.25	1.70

Table 2. Blade's Minimum Factors of Safety Calculations for the Long String.

It is my opinion that the long string production casing design had sufficient Factors of Safety and was an appropriate design. As mentioned in the Introduction there are no specific Industry standards that govern acceptable Factors of Safety for production casing design (or any other casing strings). "Typical" minimum Factors of Safety values I see in the Industry are the following:

- Burst 1.0 – 1.1
- Triaxial 1.25
- Collapse 1.0 – 1.1
- Tension 1.3 – 1.6
- Compression 1.3 – 1.6

Blade's most common recommendations for designing production casing are the following:

- Burst 1.1
- Triaxial 1.25
- Collapse 1.0
- Tension 1.3 for proprietary connections and 1.6 for API connections
- Compression 1.3 for proprietary connections and 1.6 for API connections

From BP's Casing Design Manual [7] the minimum Factors of Safety for production casing are:

- Burst 1.1
- Triaxial 1.25
- Collapse 1.0
- Tension 1.4
- Compression 1.4

First, I note that BP's internal Factors of Safety are consistent with what I regularly see in the industry.

Second, I note that the Factors of Safety for the production casing design as modeled by BP (Table 1) and modeled by Blade (Table 2) are greater than the minimum BP requirements and typical industry values. The long string production casing was an acceptable design.

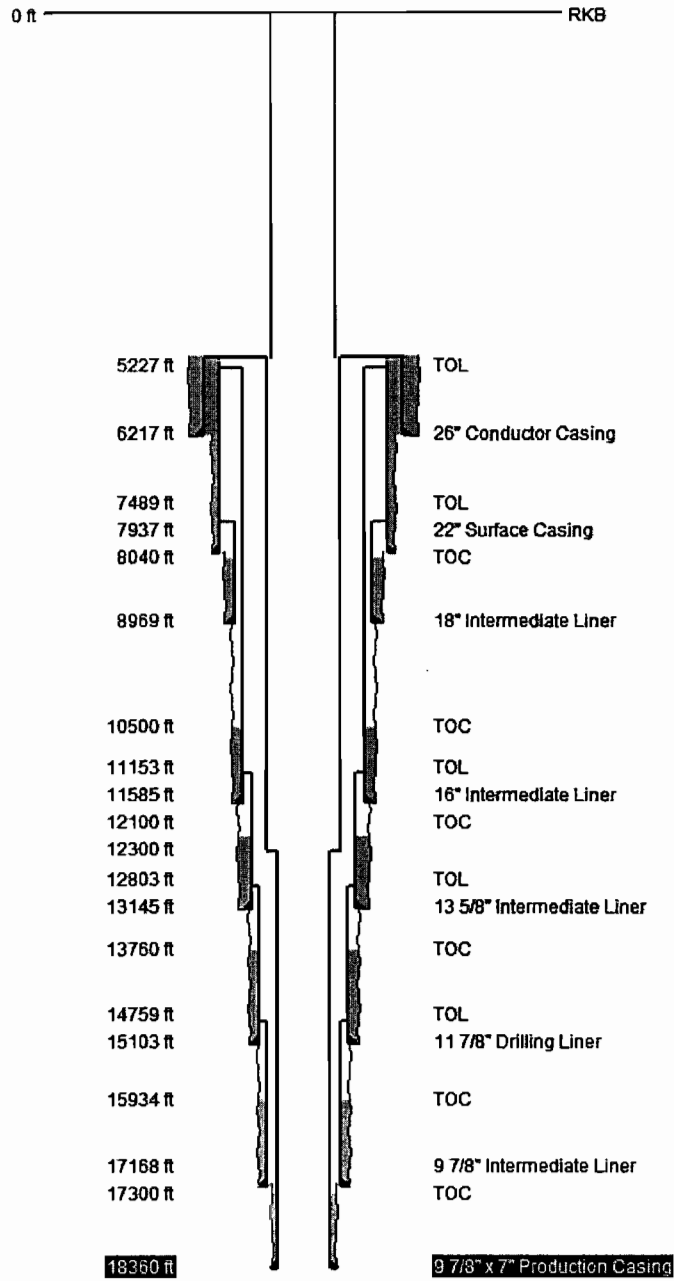


Figure 5. Macondo Long String Design.

Liner and Tieback Design Results

In addition to modeling of the long string production casing run in the Macondo well, Blade also modeled a liner and tieback design option. Figure 6 details the WellCat wellbore schematic of the liner and tieback WellCat model.

As with the long string production design, a liner and tieback is subject to burst and collapse loads that must be evaluated. Table 3 details the minimum Factors of Safety for the liner and tieback design.

	Factor Of Safety in 9-7/8" for Burst / Collapse	Factor Of Safety in 9-7/8" for VME	Factor of Safety in 7" for Burst / Collapse	Factor of Safety in 7" for VME
Tubing Leak (11060 psi shut-in tubing pressure)	1.44	1.54	1.50	1.55
Abandonment Collapse (4955 psi abandonment pressure)	1.33	1.86	1.25	1.70

Table 3. Blade's Minimum Factors of Safety Calculations for the Liner and Tieback.

As one can see the Factors of Safety are all acceptable and approximately the same as the long string design. However, the liner and tieback design inherently creates an APB issue for this design. In this configuration the B annulus has become trapped (sealed) between two casing strings. With this B annulus trapped there will be an APB load, as with all liner and tieback designs. Our analysis of a production scenario (10,000 bbl/day, 600 GOR, 32 API) in WellCat shows the APB load will be 9,340 psi (this load must be added to the existing hydrostatic loads) The additional 9,340 psi on the load side of the Factor of Safety equation (Eq. 2) causes the Factor of Safety for collapse on the production casing tieback to be 0.76. This Factor of Safety is not acceptable (less than 1.0) and failure of the tieback production casing will likely occur when the well is brought on production *unless* sufficient APB mitigation can be put in place which can reduce the APB loads to an acceptable design level. BP had APB mitigation in place to account for a trapped (sealed) B annulus possibility and the rupture disks in the 16" casing would mitigate this additional APB load for a liner and tieback production casing. In my opinion, even with the additional APB load a liner and tieback production casing would be an appropriate design, once BP's APB mitigation is taken into account. However, given the additional APB concerns, my opinion is that the long string production casing was the better of two acceptable options.

It is worth noting that the long string design option may also have an APB design issue even though it has an open casing shoe because the B annulus may or may not become trapped over the life of the well. Many operators will not solely rely on an open casing shoe to mitigate APB due to the potential problem of solids settling out of the drilling fluid in the B annulus and

plugging the casing shoe.³ Because of the solids settling problem many operators, including BP, will use an appropriate APB mitigation technique even with an open casing shoe.

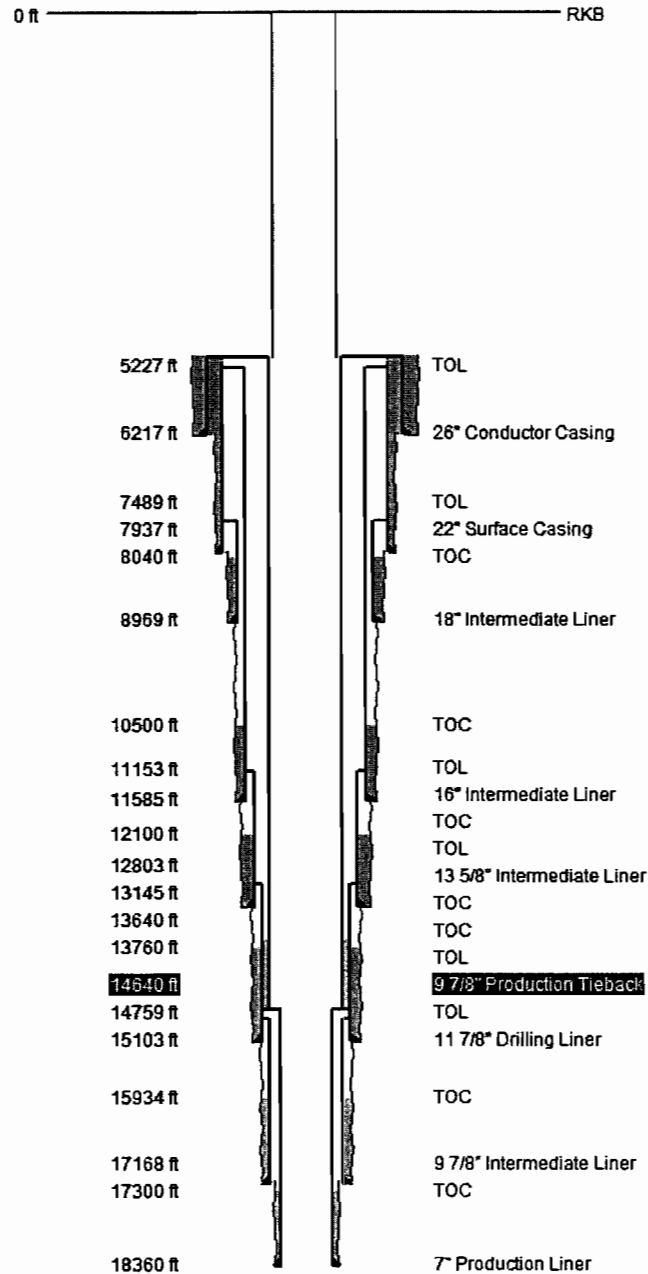


Figure 6. Macondo with Liner and Tieback Design.

³ BP's Tubular Casing Design Manual recommends treating all annuli as closed to account for this concern.

Review of David M. Pritchard's Report with Regard to Production Casing Design

In addition to my independent engineering review of the production casing for the Macondo well, I also reviewed the portions of Mr. Pritchard's BP Macondo MC 252 #1 Well Design, Planning and Execution Technical Report related to burst disks and APB mitigation. In reviewing Mr. Pritchard's report he makes several comments with regard to APB and the use of the long string versus a liner and tieback design option. I disagree with Mr. Pritchard's assertions for several reasons and do not believe that the use of rupture disks – which is an industry accepted APB mitigation technique – interfered with well kill operations.

On page 23, Section 12 Mr. Pritchard talks about the use of "Burst Plates". This term is not used by the industry and I assumed Mr. Pritchard is talking about rupture disks. Rupture disks are extensively used in the Gulf of Mexico by many operators. They are an extremely reliable method to mitigate APB which has caused wells to fail in the Gulf of Mexico and globally. Criticism of the use of rupture disks is inconsistent with common industry practice for deepwater wells in the Gulf of Mexico.

On pages 197 – 199, 242, 294, 335, 357 and 358 of his report, Mr. Pritchard discusses the limitations of using rupture disks and APB. As stated in Mr. Pritchard's report the rupture disks were rated to 7500 psi and installed in the 16" casing and he alleges that they caused the post-April 20 well control efforts to be compromised. One needs to realize that the API internal yield burst rating [8] for the 16" 97 lb/ft P110 casing used in the Macondo well is 6920 psi and the Hydril 511 connections used on the 16" casing has a burst rating of 6660 psi as shown in Figure 7 [9]. Rupture disks were not the weak link, it is typically the connection because flush or near flush connections are required to install one casing string inside of the previous casing string.

Premium Connections Performance Data

Choose pipe size, weight and grade to view connection options and performance data.

PRODUCT	PIPE SELECTION DATA			Options	
Wedge 511™	Unit	USC unit		<ul style="list-style-type: none"> > Printer friendly version > E-mail results > View list of grade codes > Tenarishydril Homepage 	
	Size	16.000	Wall (Weight:lbs/R)		0.575 (96.00)
PIN	Grade	API110	Connection		Wedge 511™
PIPE BODY DATA					
GEOMETRY					
Nominal OD	16.000 in.	Nominal Weight	96.00 lbs/R	Standard Drift Diameter	14.692 in.
Nominal ID	14.850 in.	Wall Thickness	0.575 in.	Special Drift Diameter	14.750 in.
PERFORMANCE					
Body Yield Strength	3065 x 1000 lbs	Internal Yield	6928 psi	Collapse	2340 psi
WEDGE 511™ CONNECTION DATA					
GEOMETRY					
Critical Section Area	17.416 sq. in.	Threads per in.	2.65		
PERFORMANCE					
Compression Efficiency	72.5 %	Compression Rating	2222 x 1000 lbs	Internal Yield	6660 psi
MAKE-UP TORQUES					
Yield Torque	450000 ft-lbs				
BLANKING DIMENSIONS					

BOX

Tenaris Steel Grade Designations

Figure 7. Tenaris Hydril 511 Connection Ratings.

Exhibit A – Resume of David B. Lewis



Last Name: Lewis
First Name: David
Current Position: President and CEO of Blade Energy Partners

WORK HISTORY SUMMARY

2003 - Present	Blade Energy Partners.
2000 - 2003	Independent Consultant.
1999 - 2000	ExxonMobil Upstream Research Company and Development Company – Drilling.
1992 - 1999	Mobil Exploration and Producing Technical Center (MEPTec) – Drilling Technology.
1988 - 1992	Mobil E&P Services Incorporated (MEPSI) - Drilling Technology.
1981 - 1988	Mobil R&D Corporation (MRDC) – Capital Projects - Offshore Engineering.

SUMMARY

David has over thirty years of domestic and international experience in oil & gas exploration and production. He has a management and a functional background in drilling, completions, offshore structures and a strong engineering background with experience in deepwater, big bore (mono bore) and high pressure-high temperature wells. His experience includes developing a material and well design technology on reliability based design methods for wellbore tubulars. He also has specific expertise in technology management, deepwater drilling, HPHT wells, reliability based design, tubulars, connections, marine drilling risers, conductors, pipelines, offshore structures, down-hole equipment, project management, training and finite element analysis. David is the CEO of Blade Energy Partners. He is a Registered Professional Engineer in the State of Texas, member of ASCE, SPE, and serves on numerous API and ISO committees. He has authored or co-authored over 20 industry papers. Education includes a BS degree and MS degree in Civil Engineering from University of Missouri-Rolla; and postgraduate doctoral work in finite element methods, continuum mechanics, vibrations, and structural dynamics.

JOB EXPERIENCE

2007 - Present

President and CEO - Blade Energy Partners

Blade Energy Partners is an independent company that focuses on engineering and delivery of complex projects in the upstream energy industry. Blade provides operating companies with leading-edge expertise to solve drilling, completion, production, reservoir and pipeline challenges. Blade works from an operating perspective, with the sole objective to maximize a client's return on reserves and assets. Since its creation seven years ago, Blade has worked on a variety of engineering, research, and development projects in several sectors of the upstream oil and gas industry. Blade is a group of 85 engineers who tackle the most difficult engineering problems in the oil and gas industry. Blade had annual revenues of \$21 MM in 2008 and has grossed \$100 MM in sales from its conception in 2000. Offices are located in Dallas, Houston, Dubai, Aberdeen and Jakarta. Primary clients are BP, Shell, ExxonMobil, Chevron and Total.

In addition to being the CEO of Blade, active member in or chairman of several API and ISO committees. API Executive Board Member of Committee 5 (Tubular Goods Committee) and API Executive Board Member of Committee 16 (Drilling Well Control Equipment)

2003 - 2007

Director of Engineering - Blade Energy Partners

Responsible for the engineering division of Blade Energy Partners. Developed best drilling practices for HPHT wells in the Gulf of Mexico for ChevronTexaco. Performed QRA on BP's Holstein and Mad Dog spars due to fatigue limitations on the conductor connectors. Developed stochastic cost and time estimating program for ChevronTexaco's Gorgon big bore development. Developed extreme HPHT (x-HPHT) designs for Anadarko, Shell, BHP, and Newfield for their deep gas Gulf of Mexico plays. Continue to be active in API Committees.

Designed longest extended reach well (10 miles) in the world for Norsk Hydro in the North Sea. Used Mono Diameter Solid Expandable technology coupled with stochastic tubular design to optimize torque, drag, cuttings transport, etc.

2000 - 2003

Independent Consultant

Provided drilling and completion consulting services to the upstream oil and gas industry. Specializing in deepwater and high pressure - high temperature (HPHT) wells. Clients included BP, Diamond, Shell, AERA (Shell - Mobil joint venture), BHP and PanCanadian (now EnCana).

Contracted by PanCanadian to startup and support PanCanadian's deepwater drilling development (Weymouth, Torbrook, and Annieopsquotch wells) offshore Eastern Canada. Torbrook in 6000' of water was PanCanadian's first deepwater well in water depths greater than 400 feet. This challenge coupled with a new 10,000 foot dynamically positioned vessel, the Eirik Raude, which was under construction, and a relatively new drilling contractor, Ocean Rig, made the execution of the project quite exciting and challenging. PanCanadian had no deepwater experience in the company. Overall charge was to help PanCanadian

develop their first deepwater drilling and completion program. This included completion of the vessel construction, acceptance testing, sea trials, well bore design, conductor design, wellhead, BOP/LMRP certification, marine drilling riser analysis, specification and procedure development. Provided technical project support to Shell and AERA with their onshore high pressure - high temperature wells (Northwest Lost Hills – Southern California).

Performed casing and tubing design, developed material specifications and procedures. Provided technical project support to BP and BHP with their deepwater offshore wells in the Gulf of Mexico (Crazy Horse for BP and Gnome for BHP) by performing marine drilling riser designs and stochastic well bore designs.

Expert witness for Diamond Offshore. Case centered on the catastrophic failure of a new deepwater marine drilling riser in Southeast Asia.

Developed and offered to the oil and gas industry a material and well design training course on reliability based design methods for wellbore tubulars. The course deals with all aspects of material selection from low carbon steel to the high-end alloys coupled with reliability based, limit state design theory for wells. Presented the course in October and December 2001 to over 60 participants.

Active in API Committee 5 developing new limit state design formulations for burst, collapse, and brittle fracture of wellbore tubulars which will be incorporated into the new API and ISO specifications / standards (ISO TR 10400). These new limit state formulas will greatly expand the capability of well bore tubulars used in deepwater and HPHT wells. Chairman of the API Resource Group developing Solid Expandable Technology.

1999 - 2000

Manager – Well Construction Technology. ExxonMobil.

Managed the Well Construction Section (drilling and completions) and Senior Advisor to the ExxonMobil Global Drilling Organization. This was a dual reporting role. Managed 30+ engineers involved with drilling and completion technologies within the ExxonMobil Research Company and reported into the ExxonMobil Development Company as a Senior Advisor to the global drilling organization. Responsibilities were: 1.) to develop new drilling and completion technologies and transfer them into the Development Company; 2.) provide technical drilling and completion support to all operating affiliates; and 3.) provide technical drilling and completion support to large international capital projects. Technology transfer from Mobil to ExxonMobil and refining organizational structures for the new company were the primary objectives for this time period. Effectively transferred Mobil's QRA (Quantitative Risk Analysis), LRF (Load and Resistance Factor Design), and deepwater drilling technologies into ExxonMobil.

Developed technology plans for deepwater dual gradient drilling, ultra deepwater riser designs, slim wellbore designs, casing while drilling, variable density liquid buoyancy for deepwater marine drilling risers, underbalanced drilling, low-cost deepwater drilling vessels, and deepwater completions.

1997 - 1999

Section Manager – Drilling Technology. Mobil Technology Company.

Managed 22 seasoned engineers (over 600 years of experience) working high-tech drilling and completion technologies in the support of Mobil's capital projects. The section provides the technical support for complex drilling and completion designs/operations by supporting Mobil's global drilling efforts. The section was involved in the drilling of over 40 high-tech wells in 1999 and nine large international capital projects with a total Mobil spend of \$1.2 billion (drilling / completion component). The section specialized in deepwater, HPHT, big bore (10 inch tubing), mono bore, underbalanced, extended reach, multi-lateral, and horizontal wells. In addition, the section supports and becomes heavily involved with operated by others (OBO) properties through technology application and technical support. OBO wells account for \$550 million of Mobil's annual drilling and completion spend.

Projects whereby a significant amount of technical support was provided:

- Mobile Bay / Mary Anne Developments
- Qatar – Qatar Gas / Ras Laffan Trains 1 - 4
- North Sumatra Offshore (NSO 'A')
- Skene – North Sea
- Tranche – North Sea
- Sable Island Offshore Inc (SOEI)
- Kashagan / Tangiz
- Hibernia
- North Sumatra – Indonesia – ARUN, SLS, Pase

1992 - 1997

Senior Drilling Engineering Advisor - Mobil Drilling.

Responsible for the "heavy metal" aspects of critical wells (deepwater, big bore / monobore, HPHT, etc.) within Mobil on a global basis. This includes wellheads, trees (surface and subsea), OCTG, casing / tubing connections (proprietary and API), offshore conductors, marine drilling risers, production risers and overall well bore design.

Responsible for the development of Quantitative Risk Analysis (QRA) technologies for drilling and production operations within Mobil. This technology has been applied to compaction / subsidence, marine drilling risers, corrosion, wear, poor mechanical properties / poor dimensional properties, stress corrosion cracking, inadequate designs, marine drilling risers, and various operational scenarios within Mobil.

Responsible for the concept and lead the in-house development, global implementation, and certifying authority approvals of Load and Resistance Factor Design (LRFD) technology for casing and tubing within Mobil. LRFD not only includes a design aspect but in addition, material and quality systems were developed and implemented. Lead a team of 40+ engineers / technologists from multiple Mobil Corporations in this effort. Over 15 man-years of effort went into the development of this technology. Cost savings impact to Mobil due to LRFD and QRA technologies has surpassed \$200 million dollars.

Heavily involved in the drilling startup aspects of Mobil operated drilling operations for large capital projects and Mobil affiliates, Mobil North Sea Limited - HPHT, Mobile Bay, Ras Laffan, Qatar Gas, North Sumatra Offshore, Sable Offshore Exploration Inc., and Hibernia.

Taught and developed internal Mobil training courses on Tubular Mechanics / Well Loads, LRFD for Casing / Tubing Design, Quantitative Risk Analysis, Marine Drilling Riser Analysis and Design, and Deepwater Floating Drilling.

1988 - 1992

Senior Drilling Engineer - Mobil Drilling

Responsible for the development and application of Mobil's deepwater drilling technology. Including the design, and analysis of linear / nonlinear, frequency / time domain deepwater drilling risers (up to water depths of 10,500 feet). Developed technology (riser recoil systems, riser restraint systems, fairings for vortex induced vibrations, etc.) to drill in deepwater and high current areas (greater than 5 knots). Performed all marine drilling riser analyses and deepwater well bore designs during this period for Mobil. Developed technology to run conductor (30" - 48") and 20" casing in high-current, open deepwater conditions. This technology was the foundation and successfully used in the support of Mobil's deepwater capital projects in the Gulf of Mexico, North Sea, and Brazil. Was on the API Committee 2 and a key contributor to the re-write of API RP 2Q – Recommended Practice for Design, Selection, Operation and Maintenance of Marine Drilling Riser Systems (now called API RP 16Q).

Heavily involved with the development and application of slim hole, high rpm, and continuous coring drilling technology for Mobil's New Ventures Capital Projects Group. These capital projects targeted remote jungle locations whereby full size drilling rigs could not be moved into the location. Successfully applied the technology to projects in Bolivia.

1981 - 1988

Senior Structural Engineer - Mobil Technology Company

Provided technical on-site structural engineering support to Mobil's foreign affiliates (Mobil North Sea Limited, Mobil Producing Netherlands Inc., Mobil Producing Nigeria, Mobil Exploration Norway Inc., and Mobil Oil Canada) and Mobil Capital Project Task Forces.

Foreign affiliate overseas assignments whereby structural responsibility was under my control were:

- Reanalysis of the Beryl 'A' superstructure,
- Reanalysis of the Beryl 'B' structure for certification purposes,
- Analysis and repair of the transition cones of Beryl 'A',
- Development of a weight control program for Beryl 'A',
- Development of software interfaces for weight control databases and structural analysis packages for Mobil North Sea Limited,
- INIM platform analysis,
- Statfjord 'B' and 'C' Helideck / Quarters Study,
- Beryl 'A' ballast water leak repair,
- Statfjord 'A' ALP design review,
- Statfjord 'A' Polycrown Flotel design review,
- Selection of structural analysis packages for Mobil North Sea Limited and Mobil Producing Nigeria.

Senior Structural Engineer to the following Mobil Capital Project Task Forces:

- Statfjord 'C' - Norway',
- Beryl 'B' - UK,
- Beryl 'A' Additional Gas Compression Module - UK,
- Second ALP for Beryl Field - Norway,
- Camelot - UK,
- OSO - Nigeria,
- P6/A Gas Compression Module – The Netherlands,
- Beryl 'A' Riser Platform - UK
- NESS Subsea Protection Frames - UK.

Expertise utilized within Mobil was finite element capability. This expertise was used with various in-house finite element computer analyses using either SAPV, ICES STRUDL, FISTRUDL, MARCS, ASAS, INTRA, COSTAR, OCEANS (DAMS), RASM, FLEXCOM, FREECOM, SESAM, or ABAQUS on various Mobil in-house mainframes, IBM-VM/MVS/DOS; CDC-NOS BE, NOS; VAX-VMS, and CRAY.

SPECIFIC EXPERTISE

Deepwater Drilling, Extended Reach Wells, HPHT Wells, Capital Projects, Reliability Based Design, Optimization Technology, Tubulars, Connections, Marine Drilling Risers, Conductors, Pipelines, Offshore Structures, Down-Hole Equipment, Project Management, Training and Finite Element Analysis.

PROFESSIONAL SOCIETIES AND ORGANIZATIONS

Registered Professional Engineer – Texas #59664

ASCE – American Society of Civil Engineers – Member

Academy of Civil Engineers – University of Missouri – Rolla Chapter. Board Member 2009 – 2012, President 2010

SPE – Society of Petroleum Engineers – Member. Distinguished Lecturer for 2009 – 2010. Lecture topic is: "Reliability Based Design – The Inevitable Evolution in Complex Wellbore Tubular Design"

API – American Petroleum Institute

- API Executive Board Member of Committee 5 – Tubular Goods
- Chairman API RP 5-EX Resource Group on Solid Expandable Development
- Chairman API Resource Group on Tubular Properties Software Development
- Technical Member of API 5CT - Specifications for Casing and Tubing
- Technical Member of API TR 5C3 - Bulletin on Formulas and Calculations for Casing, Tubing, Drill Pipe, and Line Pipe Properties

- API Executive Board Member of Committee 16 - Drilling Well Control Equipment
- Chairman 16Q - Recommended Practice for Design, Selection, Operation and Maintenance of Marine Drilling Riser Systems
- Chairman 16R - Specification for Marine Drilling Riser Couplings
- Technical Member of API 16F – Specification for Marine Drilling Riser Equipment
- Technical Member of API RP 6HP (PER 15K) - Greater than 15 ksi Equipment

- Technical Member API RP 96 – Deepwater Design Considerations

ISO – International Standardization Organization

- Technical Member WG2A and WG2B for ISO TR 10400 - Petroleum and natural gas industries — Equations and calculations for the properties of casing, tubing, drill pipe and line pipe used as casing or tubing

Structural Engineering Institute – Member

Tau Beta Pi – Engineering Honor Society

Chi Epsilon – Civil Engineering Honor Society Member and National Honor Member

Sigma Xi – Research Society

PUBLICATIONS

Contributing Author to SPE Textbook on Advanced Drilling and Well Technology, SPE 2009.

Gao, M., Krishnamurthy, K., **Lewis, D.B.**, "A Study of Pressure Limits of Double Q&T P110 in Low H₂S Environments", NACE Corrosion 2008 Annual Conference and Exposition, 16 – 20 March 2008, New Orleans, Louisiana.

Lewis, D. B., Sathuvalli, U.B., and Culen, M., "Designing Deep Wells: The Promise and the Challenge", Drilling and Exploration World, February 2008.

Lewis, D.B., Suryanarayana P.V., Bell, Robert, McKee, Robert, Zwald, Edwin, "ERD with Single-Diameter Expandables", Harts E&P, August 2006, pp 43 – 45.

Bell, Robert, McKee, Robert, Zwald, Edwin, **Lewis D.B.**, Suryanarayana, P.V., "Single-Diameter Technology Capable of Increasing Extended-Reach Drilling by 50%", Offshore Technology Conference OTC 17828, May 2006.

Lewis, D.B., "Quantitative Risk Analysis Optimizes Well Design in Deep, HPHT Projects", The American Oil and Gas Reporter, October 2004, pp103-109.

Maes, M.A., Sinclair, J., **Lewis, D.B.**, "Risk Analysis of Running A Deepwater Production Test from a Dynamically Positioned Vessel in the North-Atlantic", 22nd International Conference on Offshore Mechanics and Arctic Engineering - OMAE 37009, Cancun, Mexico, June 8 – 13, 2003.

Sathuvalli, U., Suryanarayana, P., **Lewis, D.B.**, "Limit Analysis of Coiled Tubing with Bending Moment, Internal Pressure and Axial Load", SPE/ICoTA Conference, SPE 68422, March 2001, Houston.

Schwind, B., Brand, P.R., **Lewis, D.B.**, Klementich, E.F., "Implementing and Benchmarking of Reliability Methods in Well Design 11-7/8 71.80 (0.582" wall) Q125 T1 S BTC-L Tin Drilling Casing", Offshore Technology Conference OTC 13052, May 2001.

Shanks, F.E., Adams, J.B., **Lewis, D.B.**, Gean, J.B., "Dynamically Positioned Drilling Vessel – Acceptability Analysis", IMCA Station Keeping Seminar, Rio de Janeiro, Brazil, 5-7 November, 1998.

Lewis, D.B., Brand, P.B., Maes, M.A., "Use of QRA Technology in Drilling and Well Operations", SPE Applied Technology Workshop - Risk Based Design of Well Casing and Tubing, SPE 48323, Houston, May 1998.

Maes, M.A., **Lewis, D.B.**, et. al., "Reliability Based Tubing and Casing Design: Principles and Approach", Journal of Offshore Mechanics and Arctic Engineering, JOMAE/362, May 1997.

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Raney, J.B., Lewis, D.B., "Implementing a Reliability-Based Design Procedure for Production Tubing", OMC 97 #1897, March 1997.

Brand, P.R., Lewis, D.B., "Reliability-Based Design of Oil Country Tubular Goods", 7th ASCE Specialty Conference on Probabilistic Mechanics and Structural Reliability, August 1996.

Maes, M.A., Lewis, D.B., "Reliability-Based Casing Design", Journal of Energy Resources Technology, June 1995, Vol. 117.

Lewis, D.B., et. al., "Load and Resistance Factor Design for Oil Country Tubular Goods", Offshore Technology Conference OTC 7936, May 1995.

Brand, P.R., Whitney, W.S., and Lewis, D.B., "Load and Resistance Factor Design Case Histories", Offshore Technology Conference OTC 7937, May 1995.

Quigley, M.S., Lewis, D.B., "Brief: Field Measurements of Casing Tension Forces", JPT Journal, February 1995.

Gulati, K.C., Lewis, D.B., et. al., "Reliability Based Design and Application of Drilling Tubulars", Offshore Technology Conference OTC 7557, May 1994.

Maes, M.A., Lewis, D.B., et. al., "Reliability Based Tubing and Casing Design", Journal of Offshore Mechanics and Arctic Engineering, JOMAE/94-1217, May 1994.

Lewis, D.B., et. al., "Effect of Makeup and Internal Pressure on the Structural Strength of API Buttress and 8 Round Threaded Connections", Offshore Technology Conference OTC 7558, May 1994.

Lewis, D.B., et. al., "The Loop Current Experience - Ewing Bank 871," Society of Petroleum Engineers, JPT Journal, September 1991.

Sheppard, D.M., and Lewis, D.B., "Weight and Cost Sensitivity of Fixed Platform Jacket Structures to Design Wave Parameters," ASME Tenth Annual Energy Sources Conference, February 1987.

Emanuel, J.H., and Lewis, D.B., "Abutment-Thermal Interaction of a Composite Bridge," Journal of the Structural Division, ASCE, Vol. 107, No. ST11, November 1981, pp 2111-2126.

EDUCATION

MS degree in Civil Engineering - Structures / Engineering Mechanics – 1980 - University of Missouri-Rolla

BS degree in Civil Engineering - Structures / Engineering Mechanics – 1978 - University of Missouri-Rolla

Professional / Honorary Degree in Civil Engineering – 2008 – University of Missouri-Rolla

Exhibit B – Statement of Compensation

Standard Rates for Legal Support Services

	<u>Consultation Hourly Rates</u>	<u>Proceedings / Testifying Hourly Rates</u>
Blade Senior Engineers:	\$338.00	\$450.00
Blade Principals	\$368.00	\$540.00
Blade Administrative Assistance:	\$55.00	

These rates are Blade's standard billing rates for its consulting work. Blade's reasonable costs including travel are paid by BP as well.

David B. Lewis will be invoiced at \$368 / hour for consultation work and \$540 / hour for proceedings and testifying.

Exhibit C – References In Report And Consideration Materials

Materials referenced in the report are:

1. MDL Ex. 1, BP Deepwater Horizon Accident Investigation Report at App. O
2. MDL Ex. 5347; 13 July 2011 F. Patton Deposition Transcript at 238-39; 23 September 2011 D. Trocquet Deposition Transcript at 35-36, 62-64. 198-199
3. MDL Ex. 3527
4. BP-HZN-MBI 00140193-201; 00140211-13; 216-233; 234-250; 251-270; 300-317; 318-335; 336-353; 354-379; 447-460; and 475-492 (2009 Drilling Program)
5. Evaluation of Casing Design Basis for Macondo Prospect Mississippi Canyon Block 252 OCS-G-32306 Well No.1 Revision 4, 22 March 2010, BP-HZN-2179MDL01327814-828
6. BP-HZN-2179MDL03291883, Macondo (MC252#1) scm Mar10.sck
7. Tubular Design Manual BPA-D-003, Revision 2.0, December 2008, BP-HZN-2179MDL02241291-1731
8. API TR 5C3 Technical Report on Equations and Calculations for Casing, Tubing, and Line Pipe Used as Casing or Tubing; and Performance Properties Tables for Casing and Tubing, December 2008
9. Tenaris website www.tenaris.com

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Additional consideration materials follow.

BEGBATES	ENDBATES	FILENAME/DESCRIPTION
BP-HZN-2179MDL03184020	BP-HZN-2179MDL03184020	Prod Csg match slides.wcd
BP-HZN-2179MDL03184021	BP-HZN-2179MDL03184021	Macondo APB updated 5-19-09.wcd
BP-HZN-2179MDL03184022	BP-HZN-2179MDL03184022	Macondo original well -- flow scenarios for Tony.wcd
BP-HZN-2179MDL03184023	BP-HZN-2179MDL03184023	Macondo APB.wcd
BP-HZN-2179MDL03184024	BP-HZN-2179MDL03184024	actual wellbore (in process).wcd
BP-HZN-2179MDL03184025	BP-HZN-2179MDL03184025	Macondo APB backup.wcd
BP-HZN-2179MDL03184026	BP-HZN-2179MDL03184026	Macondo sidetrack April'10.wcd
BP-HZN-2179MDL03184027	BP-HZN-2179MDL03184027	kill capped well 7-23-10.wcd
BP-HZN-2179MDL03184028	BP-HZN-2179MDL03184028	kill capped well.wcd
BP-HZN-2179MDL03184029	BP-HZN-2179MDL03184029	packer fluid investigation.wcd
BP-HZN-2179MDL03184030	BP-HZN-2179MDL03184030	Tubulars - 2 (Pat).wcd
BP-HZN-2179MDL03184031	BP-HZN-2179MDL03184031	flow up annulus.wcd
BP-HZN-2179MDL03184032	BP-HZN-2179MDL03184032	pump in.wcd
BP-HZN-2179MDL03305111	BP-HZN-2179MDL03305111	17 Hands injection well.wcd
BP-HZN-2179MDL03291883	BP-HZN-2179MDL03291883	Macondo (MC252#1) scm Mar10.sck
n/a	n/a	2011-09-23 Expert Report of Calvin Barnhill (Transocean).pdf
n/a	n/a	2011-07-13 Patton, Frank (Deposition Transcripts & Exhibits)
n/a	n/a	2011-03-21 Sprague, John (Deposition Transcripts & Exhibits)
n/a	n/a	2011-09-23 Trocquet, David (Deposition Transcripts & Exhibits)
BP-HZN-2179MDL00161597	BP-HZN-2179MDL00161607	TD casing and T.A. plan forward.ppt
BP-HZN-2179MDL0010506	BP-HZN-2179MDL0010507	Email from Hafle to Miller er Macondo APB
BP-HZN-BLY00000001	BP-HZN-BLY00000760	BP Internal Investigation Report
n/a	n/a	Presidential Commission Report
n/a	n/a	2011-08-26 Expert Report of Pritchard (PSC)
n/a	n/a	Macondo Incident - Transocean Investigation Report
BP-HZN-2179MDL02241291	BP-HZN-2179MDL02241731	Tubular Design Manual
BP-HZN-2179MDL03858684	BP-HZN-2179MDL03859253	SRP 5.2-0005
BP-HZN-MBI00130799	BP-HZN-MBI00130910	Drilling and Well Operating Procedure
BP-HZN-CEC020494	BP-HZN-CEC020510	2010-03 Drilling Pieces
BP-HZN-CEC028826	BP-HZN-CEC028840	2010-04 Drilling Pieces
BP-HZN-MBI00099088	BP-HZN-MBI00099102	2010-01 Drilling Plan Pieces
BP-HZN-MBI00116697	BP-HZN-MBI00116706	2010-03 Drilling Pieces
BP-HZN-MBI00126181	BP-HZN-MBI00126200	2010-04 Drilling Pieces
BP-HZN-MBI00140193	BP-HZN-MBI00140201	2009-09 Drilling Plan Pieces
BP-HZN-MBI00140211	BP-HZN-MBI00140213	2009-09 Drilling Plan Pieces
BP-HZN-MBI00140216	BP-HZN-MBI00140233	2009-09 Drilling Plan Pieces
BP-HZN-MBI00140234	BP-HZN-MBI00140250	2009-09 Drilling Plan Pieces

BEGBATES	ENDBATES	FILENAME/DESCRIPTION
BP-HZN-MB100140251	BP-HZN-MB100140270	2009-09 Drilling Plan Pieces
BP-HZN-MB100140300	BP-HZN-MB100140317	2009-09 Drilling Plan Pieces
BP-HZN-MB100140318	BP-HZN-MB100140335	2009-09 Drilling Plan Pieces
BP-HZN-MB100140336	BP-HZN-MB100140353	2009-09 Drilling Plan Pieces
BP-HZN-MB100140354	BP-HZN-MB100140379	2009-09 Drilling Plan Pieces
BP-HZN-MB100140447	BP-HZN-MB100140460	2009-09 Drilling Plan Pieces
BP-HZN-MB100140461	BP-HZN-MB100140473	2010-01 Drilling Plan Pieces
BP-HZN-MB100140475	BP-HZN-MB100140492	2009-09 Drilling Plan Pieces
BP-HZN-MB100140493	BP-HZN-MB100140509	2010-01 Drilling Plan Pieces
BP-HZN-MB100140522	BP-HZN-MB100140530	2010-01 Drilling Plan Pieces
BP-HZN-MB100140564	BP-HZN-MB100140598	2010-01 Drilling Plan Pieces
BP-HZN-MB100140599	BP-HZN-MB100140600	2010-01 Drilling Plan Pieces
BP-HZN-MB100140601	BP-HZN-MB100140617	2010-01 Drilling Plan Pieces
BP-HZN-MB100141096	BP-HZN-MB100141118	2010-03 Drilling Pieces
BP-HZN-MB100141119	BP-HZN-MB100141137	2010-03 Drilling Pieces
BP-HZN-MB100141205	BP-HZN-MB100141221	2010-03 Drilling Pieces
BP-HZN-MB100141257	BP-HZN-MB100141276	2010-03 Drilling Pieces
BP-HZN-MB100141297	BP-HZN-MB100141316	2010-03 Drilling Pieces
BP-HZN-MB100141317	BP-HZN-MB100141336	2010-03 Drilling Pieces
BP-HZN-MB100141400	BP-HZN-MB100141411	2010-03 Drilling Pieces
BP-HZN-MB100141493	BP-HZN-MB100141512	2010-03 Drilling Pieces
BP-HZN-MB100141737	BP-HZN-MB100141746	2010-03 Drilling Pieces
BP-HZN-MB100142014	BP-HZN-MB100142034	2010-04 Drilling Pieces
BP-HZN-2179MDL00539685	BP-HZN-2179MDL00539696	Evaluation of Casing Basis of Design - Rev 0
BP-HZN-2179MDL00470489	BP-HZN-2179MDL00470501	Evaluation of Casing Basis of Design - Rev 1
BP-HZN-2179MDL03074329	BP-HZN-2179MDL03074252	Evaluation of Casing Basis of Design - Rev 2
BP-HZN-2179MDL01578858	BP-HZN-2179MDL01578862	Evaluation of Casing Basis of Design - Rev 3
BP-HZN-2179MDL0132814	BP-HZN-2179MDL01327828	Evaluation of Casing Basis of Design - Rev 4
BP-HZN-BLY00165387	BP-HZN-BLY00165397	Macondo Prospect APB Mitigation - Rev 0
BP-HZN-2179MDL00236767	BP-HZN-2179MDL00236779	Macondo Prospect APB Mitigation - Rev 1
BP-HZN-2179MDL00010506	BP-HZN-2179MDL00010507	April 14, 2010 Miller to Morel email re APB mitigation
n/a	n/a	Trocquet Deposition Transcript and Exhibits
n/a	n/a	MDL Exhibit 5347 - Long String designs produced during Trocquet Deposition
BP-HZN-2179MDL00048527	BP-HZN-2179MDL00048531	Macondo APB dated April 15, 2010
n/a	n/a	Materials from www.tennaris.com re crossover joint

BEGBATES	ENDBATES	FILENAME/DESCRIPTION
n/a	n/a	API TR 5C3 Technical Report on Equations and Calculations for Casing, Tubing, and Line Pipe Used as Casing or Tubing; and Performance Properties Tables for Casing and Tubing, December 2008
TBD		Macondo MC252#1 (Long String Final).wcd (Blade created file)
TBD		Macondo MC 252#1 (Lnr+Tbk Final).wcd (Blade created file)
BP-HZN-2179MDL00236767	BP-HZN-2179MDL00236779	Macondo Prospect APB Mitigation Post Incident Report
BP-HZN-BL Y00173321	BP-HZN-BL Y00173326	Macondo: Integrity of the 9-7/8" x 7" Production Casing Post Incident Report
BP-HZN-2179MDL03154695	BP-HZN-2179MDL03154702	Macondo: Axial Movement/Forces Prior to Surface Event Post Incident Report
BP-HZN-2179MDL03369432	BP-HZN-2179MDL03369436	Macondo Pressure Limits for Kill Operations Post Incident Report
BP-HZN-2179MDL01598746	BP-HZN-2179MDL01598750	Macondo 16" x 9-7/8" Annulus Pressure Integrity Post Incident Report
BP-HZN-2179MDL00644093	BP-HZN-2179MDL00644110	Evaluation of Casing Design Basis for MC 252 Relief Wells 1 & 2 Post Incident Report
BP-HZN-2179MDL02316516	BP-HZN-2179MDL02316535	MC 252 Post-Event Flow Scenarios Post Incident Report
BP-HZN-2179MDL01597128	BP-HZN-2179MDL0157147	MC 252 Post-Event Flow Scenarios Post Incident Report
BP-HZN-2179MDL03305112	BP-HZN-2179MDL03305119	Macondo Containment Alternatives Post Incident Report
BP-HZN-2179MDL00001265	BP-HZN-2179MDL00001274	MC252 BP01 RPB 7addition approval.pdf
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BP-HZN-2179MDL00003290	BP-HZN-2179MDL00003295	BP-3296 JS WO-10445 Offshore Energy Services Macondo MC252-1 Horizon.pdf
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BP-HZN-2179MDL00003889	BP-HZN-2179MDL00003899	BP-3319 JS WO-10537 Weatherford TRS Macondo MC 252 1 Horizon.pdf
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BP-HZN-2179MDL00007421	BP-HZN-2179MDL00007422	CRF NCR 0310 574 WO-10489 Alliamon Tool Macondo MC252-1 Horizon.pdf
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BP-HZN-2179MDL00009773	BP-HZN-2179MDL00009781	BP-3282 JS WO-10408 Halliburton Sperry Sun Macondo MC 252 1 Horizon.pdf
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BP-HZN-2179MDL00010561	BP-HZN-2179MDL00010568	BP-008 SC WO-10506 Halliburton Service Tools Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL00010571	BP-HZN-2179MDL00010571	kv2414.mail
BP-HZN-2179MDL00010572	BP-HZN-2179MDL00010583	BP-012-PT WO-10532 Blackhawk Specialty Tools Houma-Macondo-MC252#1-Horizon.pdf
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BP-HZN-2179MDL00011127	BP-HZN-2179MDL00011132	BP-081-AH WO-10389 Mud Tool Subs Offshore Energy Services Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL00011207	BP-HZN-2179MDL00011207	Macondo 7" ID caliper
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BP-HZN-2179MDL00011304	BP-HZN-2179MDL00011310	BP-222 CD WO-10397 9600 Geo Pilots DD Halliburton-Sperry Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL00011329	BP-HZN-2179MDL00011329	Macondo 11-7/8" Updated Procedure
BP-HZN-2179MDL00011534	BP-HZN-2179MDL00011537	Mud Report 3-1-2010.pdf
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BP-HZN-2179MDL00262930	BP-HZN-2179MDL00262934	016_OCS-G32306 MC252 #1 - BP Daily Operations-Partners Report - Report Number 15 - (10-20-2009).PDF
BP-HZN-2179MDL00262966	BP-HZN-2179MDL00262970	023_OCS-G32306 MC252 #1 - BP Daily Operations-Partners Report - Report Number 22 - (10-27-2009).pdf
BP-HZN-2179MDL00262971	BP-HZN-2179MDL00262975	024_OCS-G32306 MC252 #1 - BP Daily Operations-Partners Report - Report Number 23 - (10-28-2009).PDF
BP-HZN-2179MDL00262993	BP-HZN-2179MDL00262995	028_OCS-G32306 MC252 #1 - BP Daily Operations-Partners Report - Report Number 27 - (11-1-2009).pdf

BEGBATES	ENDBATES	FILENAME/DESCRIPTION
BP-HZN-2179MDL00265152	BP-HZN-2179MDL00265156	MC 252 #1 Daily Report 10-26-09.pdf
BP-HZN-2179MDL00268277	BP-HZN-2179MDL00268318	Puma 4 End of Well report
BP-HZN-2179MDL00269994	BP-HZN-2179MDL00269994	kv249.mail
BP-HZN-2179MDL00269995	BP-HZN-2179MDL00269996	RA-10145 WB WO-10145 Repair Authorization Allis Chalmers Amelia Maconda MC 252 #1 Marianas.pdf
BP-HZN-2179MDL00270555	BP-HZN-2179MDL00270556	RE: Macondo - 16" Casing
BP-HZN-2179MDL00270557	BP-HZN-2179MDL00270557	BP-1176-AB 16" ID CALIPER 20 JTS TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL00270558	BP-HZN-2179MDL00270558	BP-270-KJK 16 97# BP-135 PE (182-JTS TS insp) TB #3.XLS
BP-HZN-2179MDL00270591	BP-HZN-2179MDL00270591	Macondo - 9-7/8" ID Caliper
BP-HZN-2179MDL00270592	BP-HZN-2179MDL00270592	BP-1180-AB 9 7-8 REPAIRS RIG PREP INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL00270593	BP-HZN-2179MDL00270593	BP-1147-AB 9 7-8 62 8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL00270716	BP-HZN-2179MDL00270716	Macondo - 9-7/8" ID Caliper
BP-HZN-2179MDL00270717	BP-HZN-2179MDL00270717	BP-1180-AB 9 7-8 REPAIRS RIG PREP INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL00270718	BP-HZN-2179MDL00270718	BP-1147-AB 9 7-8 62 8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL00273878	BP-HZN-2179MDL00273882	MC252 #1 COF 20100418.PDF
BP-HZN-2179MDL00273913	BP-HZN-2179MDL00273919	MC252 #1 COF 20100419.PDF
BP-HZN-2179MDL00286556	BP-HZN-2179MDL00286556	Emailing: Macondo_Drilling_Sec04_16_Liner_Interval_NSC_DP.doc, Macondo_Drilling_Sec05_13_58_Casing_Interval.doc
BP-HZN-2179MDL00287111	BP-HZN-2179MDL00287111	kv4332.mail
BP-HZN-2179MDL00287548	BP-HZN-2179MDL00287562	Approval.pdf
BP-HZN-2179MDL00287718	BP-HZN-2179MDL00287718	FW: 13-5/8" Drilling Procedure
BP-HZN-2179MDL00287906	BP-HZN-2179MDL00287923	Macondo Drilling_Sec09_13_58_Casing_Interval BP01.doc
BP-HZN-2179MDL00288416	BP-HZN-2179MDL00288416	Macondo kv1390.mail
BP-HZN-2179MDL00289961	BP-HZN-2179MDL00289961	FW: 11-7/8" Procedure
BP-HZN-2179MDL00289962	BP-HZN-2179MDL00289973	Macondo Drilling_Sec 10 11 875 Liner Interval Rev2.doc
BP-HZN-2179MDL00292210	BP-HZN-2179MDL00292210	Macondo Drilling_Sec 10 9 875 Liner Interval_Rev0.doc
BP-HZN-2179MDL00297108	BP-HZN-2179MDL00297108	11-7/8" and 9-7/8" liner procedures
BP-HZN-2179MDL00300865	BP-HZN-2179MDL00300874	Macondo Drilling production Interval_rev2.doc
BP-HZN-2179MDL00300919	BP-HZN-2179MDL00300920	RE: Rev 1 Procedure
BP-HZN-2179MDL00310022	BP-HZN-2179MDL00310023	FW: Rev 1 Procedure
BP-HZN-2179MDL00335261	BP-HZN-2179MDL00335261	RE: Macondo Drilling_Sec 10 9 875 Liner Interval_Rev0.doc
BP-HZN-2179MDL00338047	BP-HZN-2179MDL00338047	kv3634.mail
BP-HZN-2179MDL00339877	BP-HZN-2179MDL00339877	RE: Thoughts
BP-HZN-2179MDL00339885	BP-HZN-2179MDL00339885	BP_173_CD_WO-09775_WFTD_Gemoco_Macondo_MC_252_1_Marianas.pdf - Adobe Acrobat Standard
BP-HZN-2179MDL00339886	BP-HZN-2179MDL00339894	BP 173_CD_WO-09775 WFTD Gemoco Macondo MC 252 1 Marianas.pdf
BP-HZN-2179MDL00343242	BP-HZN-2179MDL00343242	FW BP-80 kv4784.mail

BEGBATES	ENDBATES	FILENAME/DESCRIPTION
BP-HZN-2179MDL00343243	BP-HZN-2179MDL00343249	BP-806 BJT WO 09466 Workstrings Macondo MC 252 1 Marianas.pdf
BP-HZN-2179MDL00343250	BP-HZN-2179MDL00343251	CRF NCR 0809 356 WO-09466 Workstrings Macondo MC252-1 Marianas.pdf
BP-HZN-2179MDL00355731	BP-HZN-2179MDL00355740	11-7/8" Casing Interval
BP-HZN-2179MDL00356009	BP-HZN-2179MDL00356009	Re: Thoughts
BP-HZN-2179MDL00360303	BP-HZN-2179MDL00360312	Macondo Drilling production Interval rev2.doc
BP-HZN-2179MDL00379981	BP-HZN-2179MDL00379993	BP-001 SC WO-10441 Halliburton Sperry Drilling Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL00398350	BP-HZN-2179MDL00398350	CRF NCR 0310 574 WO-10489 Allamton Tool Macondo MC252-1 Horizon.xls
BP-HZN-2179MDL00398774	BP-HZN-2179MDL00398776	MOCGomPrint[1].pdf
BP-HZN-2179MDL00398869	BP-HZN-2179MDL00398869	kv2169.mail
BP-HZN-2179MDL00398870	BP-HZN-2179MDL00398879	BP 132 PC WO 0414 Sii 34928 Allis Chalmers Macondo MC 252 #1 Marianas.pdf
BP-HZN-2179MDL00413598	BP-HZN-2179MDL00413598	Macondo Schematic 14 8 2 4142010.xls
BP-HZN-2179MDL00413690	BP-HZN-2179MDL00413691	FW: BP-1284-AB 9 7-8 X 7" X-OVER INSP K&B MACONDO MC252-1.XLS
BP-HZN-2179MDL00413692	BP-HZN-2179MDL00413692	BP-1284-AB 9 7-8 X 7" X-OVER INSP K&B MACONDO MC252-1.XLS
BP-HZN-2179MDL00443132	BP-HZN-2179MDL00443160	APD approval.pdf
BP-HZN-2179MDL00477014	BP-HZN-2179MDL00477014	Macondo MC 252 1 Schematic Rev14.0 SET 03072010.xls
BP-HZN-2179MDL00477039	BP-HZN-2179MDL00477039	Macondo MC 252 1 Schematic 062209 Rev6 DEFINE.xls
BP-HZN-2179MDL00477050	BP-HZN-2179MDL00477050	Macondo MC 252 #1 Schematic 040609 RevC.xls
BP-HZN-2179MDL00477063	BP-HZN-2179MDL00477063	Macondo MC 252 1 Schematic 110609 Rev12.2 EXECUTE.xls
BP-HZN-2179MDL00477066	BP-HZN-2179MDL00477066	Macondo MC 252 #1 Schematic 050209 Rev0 DEFINE.xls
BP-HZN-2179MDL00477068	BP-HZN-2179MDL00477068	Macondo MC 252 1 Schematic 051609 Rev5 DEFINE.xls
BP-HZN-2179MDL00477074	BP-HZN-2179MDL00477074	Macondo MC 252 1 Schematic 070809 Rev7 DEFINE.xls
BP-HZN-2179MDL00477116	BP-HZN-2179MDL00477116	Macondo
BP-HZN-2179MDL00501777	BP-HZN-2179MDL00501777	Macondo MC 252 #1 Schematic 040609 RevC.xls
BP-HZN-2179MDL00514445	BP-HZN-2179MDL00514508	Morel - LeBleu Reviewed Macondo Drilling Program.pdf
BP-HZN-2179MDL00520608	BP-HZN-2179MDL00520608	Macondo MC 252 1 Schematic 1610 Horizon Rev13.2 EXECUTE.xls
BP-HZN-2179MDL00524558	BP-HZN-2179MDL00524566	Macondo RBP 7addition correction.pdf
BP-HZN-2179MDL00529930	BP-HZN-2179MDL00529938	APD approval.pdf
BP-HZN-2179MDL00572911	BP-HZN-2179MDL00572937	MC 252 Macondo BoD 22 in Casing Post Job Report.pdf
BP-HZN-2179MDL00572938	BP-HZN-2179MDL00572938	MC 252 Macondo BoD 16 in Liner Post Job Report.pdf
BP-HZN-2179MDL00573894	BP-HZN-2179MDL00574126	WSL Handbook.pdf
BP-HZN-2179MDL00870350	BP-HZN-2179MDL00870364	GP 10-01 - Casing and Tubing Design.doc
BP-HZN-2179MDL01743223	BP-HZN-2179MDL01743746	TDM 2010.pdf
BP-HZN-2179MDL01765527	BP-HZN-2179MDL01765527	BP-1261-AB 11 7-8 71.8 HCQ125 513 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01765528	BP-HZN-2179MDL01765528	BP-1261-AB 11 7-8 71.8 HCQ125 513 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01768794	BP-HZN-2179MDL01768794	BP-1266-AB 9 5-8 53.5 Q125 513 BOX X 9 7-8 62.8 513 PIN X-OVER MACONDO MC252-1.XLS

BEGBATES	ENDBATES	FILENAME/DESCRIPTION
BP-HZN-2179MDL01768795	BP-HZN-2179MDL01768795	BP-1266-AB 9 5-8 53.5 Q125 513 BOX X 9 7-8 62.8 513 PIN X-OVER MACONDO MC252-1.XLS
BP-HZN-2179MDL01774971	BP-HZN-2179MDL01774971	BP-1261-AB 11 7-8 71.8 HCQ125 513 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01774972	BP-HZN-2179MDL01774972	BP-1261-AB 11 7-8 71.8 HCQ125 513 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01789618	BP-HZN-2179MDL01789619	RE: 7" 32# drifting
BP-HZN-2179MDL01789620	BP-HZN-2179MDL01789620	BP-1282-AB 7" 32 HCQ125 513 RIG PREP EXPERT RISER SOLUTION FOURCHON MACONDO MC252-1.XLS
BP-HZN-2179MDL01790235	BP-HZN-2179MDL01790235	BP-1282-AB 7" 32 HCQ125 513 RIG PREP EXPERT RISER SOLUTION FOURCHON MACONDO MC252-1.XLS
BP-HZN-2179MDL01790236	BP-HZN-2179MDL01790236	BP-1282-AB 7" 32 HCQ125 513 RIG PREP EXPERT RISER SOLUTION FOURCHON MACONDO MC252-1.XLS
BP-HZN-2179MDL01843753	BP-HZN-2179MDL01843753	BP-1147-AB 9 7-8 82.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01896142	BP-HZN-2179MDL01896142	FW: BP-164 CD WO-09574 Allis Chalmers Broussard Macondo MC252-1 Transocean Marianas.pdf - Adobe Acrobat Standard
BP-HZN-2179MDL01896143	BP-HZN-2179MDL01896150	BP-164 CD WO-09574 Allis Chalmers Broussard Macondo MC252-1 Transocean Marianas.pdf
BP-HZN-2179MDL01896208	BP-HZN-2179MDL01896208	Macondo - Float Equipment Order - PO 4540072082 Rev 1 dated 09-24-2009 - Need Approval
BP-HZN-2179MDL01896209	BP-HZN-2179MDL01896217	PO 4540072082 Rev 1 dated 09-24-2009.pdf
BP-HZN-2179MDL01898052	BP-HZN-2179MDL01898052	Macondo - 13-5/8" Pup Joint to Hydril for Split & Re-thread
BP-HZN-2179MDL01898053	BP-HZN-2179MDL01898053	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01898545	BP-HZN-2179MDL01898545	Macondo kv4671.mail
BP-HZN-2179MDL01898546	BP-HZN-2179MDL01898554	PO 4540072082 Rev 1 dated 09-24-2009 - Approved.pdf
BP-HZN-2179MDL01898871	BP-HZN-2179MDL01898872	FW BP Ma kv5877.mail
BP-HZN-2179MDL01898873	BP-HZN-2179MDL01898873	FW: BP-164 CD WO-09574 Allis Chalmers Broussard Macondo MC252-1 Transocean Marianas.xls
BP-HZN-2179MDL01898874	BP-HZN-2179MDL01898874	BP-164 CD WO-09574 Allis Chalmers Broussard Macondo MC252-1 Transocean Marianas.xls
BP-HZN-2179MDL01903806	BP-HZN-2179MDL01903807	Macondo - 9-7/8" Re-threads - Post-thread Inspection adh Rig Prep
BP-HZN-2179MDL01903808	BP-HZN-2179MDL01903808	TUBULAR GOODS RELEASE
BP-HZN-2179MDL01903809	BP-HZN-2179MDL01903809	BP-1147-AB 9 7-8 62.8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01903810	BP-HZN-2179MDL01903810	BP-1124-AB 9 7-8 62.8 Q125 THRD INSP TUBO S MACONDO MC252-1.XLS
BP-HZN-2179MDL01904597	BP-HZN-2179MDL01904597	BP-1194- kv31333.mail
BP-HZN-2179MDL01904598	BP-HZN-2179MDL01904598	BP-1194-AB 16" CLEAN AND REDOPE TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01904631	BP-HZN-2179MDL01904631	BP-1173-AB 18" PUP JT INSP HYDRIL MACONDO MC252-1.XLS
BP-HZN-2179MDL01904632	BP-HZN-2179MDL01904632	BP-1173-AB 18" PUP JT INSP HYDRIL MACONDO MC252-1.XLS
BP-HZN-2179MDL01904688	BP-HZN-2179MDL01904688	BP-1144-AB 18" 117 P110 511 RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01904689	BP-HZN-2179MDL01904689	BP-1144-AB 18" 117 P110 511 RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01904690	BP-HZN-2179MDL01904690	BP-1185-AB 13 5-8 PUP JT RIG PREP MACONDO MC252-1.XLS

BEGBATES	ENDBATES	FILENAME/DESCRIPTION
BP-HZN-2179MDL01904691	BP-HZN-2179MDL01904691	BP-1185-AB 13 5-8 PUP JT RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01906144	BP-HZN-2179MDL01906144	BP-1184-AB 18" 117 P110 511 MACONDO MC252-1.XLS
BP-HZN-2179MDL01906145	BP-HZN-2179MDL01906145	BP-1184-AB 18" 117 P110 511 MACONDO MC252-1.XLS
BP-HZN-2179MDL01907303	BP-HZN-2179MDL01907303	BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01907304	BP-HZN-2179MDL01907304	BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01913574	BP-HZN-2179MDL01913575	FW: Macondo - 13-5/8" Pup Joint to Hydril for Split & Re-thread
BP-HZN-2179MDL01913576	BP-HZN-2179MDL01913576	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01913653	BP-HZN-2179MDL01913653	JS100332 kv3545.mail
BP-HZN-2179MDL01913654	BP-HZN-2179MDL01913654	JS100332-WR-089-SM.xls
BP-HZN-2179MDL01914613	BP-HZN-2179MDL01914613	Macondo - Float EquipmentPO 4540072082 Rev 2 dated 10-13-2009 (2).pdf - Adobe Acrobat Standard
BP-HZN-2179MDL01914614	BP-HZN-2179MDL01914624	PO 4540072082 Rev 2 dated 10-13-2009 (2).pdf
BP-HZN-2179MDL01917717	BP-HZN-2179MDL01917717	RE: 9 5/8 Csg. Pups BP Macondo#1 MC-252
BP-HZN-2179MDL01917718	BP-HZN-2179MDL01917718	BP-1266-AB 9 5-8 53 5 Q125 513 BOX X 9 7-8 62 8 513 PIN X-OVER MACONDO MC252-1 (2).XLS
BP-HZN-2179MDL01917719	BP-HZN-2179MDL01917719	BP-1264-AB 9 5-8 X 9 7-8 X-OVER INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL01919954	BP-HZN-2179MDL01919954	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01919955	BP-HZN-2179MDL01919955	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01922352	BP-HZN-2179MDL01922352	BP-1182-AB 16" PUP JT RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01922353	BP-HZN-2179MDL01922353	BP-1182-AB 16" PUP JT RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01922500	BP-HZN-2179MDL01922500	18" RIG PREP & BUCK-ON AT TUBO SOUTH
BP-HZN-2179MDL01922501	BP-HZN-2179MDL01922501	BP Integrity Assurance Insp. Workbook v4.8
BP-HZN-2179MDL01922502	BP-HZN-2179MDL01922502	BP Integrity Assurance Insp. Workbook v4.8
BP-HZN-2179MDL01925752	BP-HZN-2179MDL01925752	RA-9576 BJT WO-09576 Repair Authorization DT L313941 Workstrings Nakika Herschel SS
BP-HZN-2179MDL01925753	BP-HZN-2179MDL01925755	MC520-H2 Marianas.pdf - Adobe Acrobat Standard
BP-HZN-2179MDL01926317	BP-HZN-2179MDL01926317	RA-9576 BJT WO-09576 Repair Authorization DT L313941 Workstrings Nakika Herschel SS
BP-HZN-2179MDL01926318	BP-HZN-2179MDL01926318	MC520-H2 Marianas.pdf
BP-HZN-2179MDL01926451	BP-HZN-2179MDL01926451	RA-9576 BJT WO-09576 Repair Authorization DT L313941 Workstrings Nakika Herschel SS
BP-HZN-2179MDL01926452	BP-HZN-2179MDL01926452	MC520-H2 Marianas.pdf
BP-HZN-2179MDL01928379	BP-HZN-2179MDL01928379	BP-1261-AB 11 7-8 71.8 HCQ125 513 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01928380	BP-HZN-2179MDL01928380	BP-1261-AB 11 7-8 71.8 HCQ125 513 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01932130	BP-HZN-2179MDL01932130	BP-1125-AB 9 7-8 62.8 Q125 THRD INSP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01932131	BP-HZN-2179MDL01932131	BP-1125-AB 9 7-8 62.8 Q125 THRD INSP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01941429	BP-HZN-2179MDL01941429	BP-1264-AB 9 5-8 X 9 7-8 X-OVER INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL01941430	BP-HZN-2179MDL01941430	BP-1264-AB 9 5-8 X 9 7-8 X-OVER INSP MACONDO MC252-1.XLS
		BP-1101-AB 16" 97 P110 511 BURST SUB STENCILING MACONDO MC252-1.XLS
		BP-1101-AB 16" 97 P110 511 BURST SUB STENCILING MACONDO MC252-1.XLS
		BP-1177-AB 16" TMT BUCKON TUBO S. MACONDO MC252-1.XLS
		BP-1177-AB 16" TMT BUCKON TUBO S. MACONDO MC252-1.XLS

BEGBATES	ENDBATES	FILENAME/DESCRIPTION
BP-HZN-2179MDL01942794	BP-HZN-2179MDL01942795	FW: Macondo - 9-7/8" Re-threads - Post-thread Inspection adn Rig Prep
BP-HZN-2179MDL01942796	BP-HZN-2179MDL01942796	Hydril PA-09-6955-AV.doc
BP-HZN-2179MDL01942797	BP-HZN-2179MDL01942797	BP-1147-AB 9 7-8 62.8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01942798	BP-HZN-2179MDL01942798	BP-1124-AB 9 7-8 62.8 Q125 THRD INSP TUBO S MACONDO MC252-1.XLS
BP-HZN-2179MDL01943218	BP-HZN-2179MDL01943218	BP-1180- kv3841.mail
BP-HZN-2179MDL01943219	BP-HZN-2179MDL01943219	BP-1180-AB 9 7-8 REPAIRS RIG PREP INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL01948962	BP-HZN-2179MDL01948962	Macondo - 16" Casing Back to Storage
BP-HZN-2179MDL01948963	BP-HZN-2179MDL01948963	BP-1182-AB 16" PUP JT RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01948964	BP-HZN-2179MDL01948964	BP-1182-AB 16" PUP JT RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01948965	BP-HZN-2179MDL01948965	BP-1171-AB 16" RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01948966	BP-HZN-2179MDL01948966	BP-1171-AB 16" RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01948967	BP-HZN-2179MDL01948967	BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01948968	BP-HZN-2179MDL01948968	BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01956781	BP-HZN-2179MDL01956782	FW: BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01956783	BP-HZN-2179MDL01956783	BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01957649	BP-HZN-2179MDL01957649	BP-1186-AB 18" 117 P110 511 WR INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL01957650	BP-HZN-2179MDL01957650	BP-1186-AB 18" 117 P110 511 WR INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL01960125	BP-HZN-2179MDL01960125	FW: Macondo - Float Equipment Order - Weatherford PO 4540072082 Rev 2 - Need Approval
BP-HZN-2179MDL01960126	BP-HZN-2179MDL01960126	PO 4540072082 Rev 2 dated 10-13-2009.pdf
BP-HZN-2179MDL01960137	BP-HZN-2179MDL01960137	PO 4540072082 Rev 2 dated 10-13-2009 (2).pdf
BP-HZN-2179MDL01960473	BP-HZN-2179MDL01960473	FW: Macondo - Float Equipment Order - PO 4540072082 Rev 1 dated 09-24-2009 - Need Approval
BP-HZN-2179MDL01960474	BP-HZN-2179MDL01960482	PO 4540072082 Rev 1 dated 09-24-2009.pdf
BP-HZN-2179MDL01960483	BP-HZN-2179MDL01960491	PO 4540072082 Rev 1 dated 09-24-2009 (2).pdf
BP-HZN-2179MDL01961550	BP-HZN-2179MDL01961550	BP-1147-AB 9 7-8 62.8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01961551	BP-HZN-2179MDL01961551	BP-1147-AB 9 7-8 62.8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01962010	BP-HZN-2179MDL01962010	BP-1227-AB 16" 109 P110EC 511 RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01962011	BP-HZN-2179MDL01962011	BP-1227-AB 16" 109 P110EC 511 RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01965469	BP-HZN-2179MDL01965469	BP-1252-AB 13 5-8 88.2 HCQ125 523 APPLY KENDEX MACONDO MC252-1.XLS
BP-HZN-2179MDL01965470	BP-HZN-2179MDL01965470	BP-1252-AB 13 5-8 88.2 HCQ125 523 APPLY KENDEX MACONDO MC252-1.XLS
BP-HZN-2179MDL01969228	BP-HZN-2179MDL01969228	BP-1226-AB 16" 109 P110EC 511 RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01969229	BP-HZN-2179MDL01969229	BP-1226-AB 16" 109 P110EC 511 RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01970844	BP-HZN-2179MDL01970844	BP-1183-AB 16" PUP JT RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01970845	BP-HZN-2179MDL01970845	BP-1183-AB 16" PUP JT RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01982761	BP-HZN-2179MDL01982761	BP-1265-AB 9 7-8 62.8 Q125 513 BOX END CUTOFF MACONDO MC252-1.XLS
BP-HZN-2179MDL01982762	BP-HZN-2179MDL01982762	BP-1265-AB 9 7-8 62.8 Q125 513 BOX END CUTOFF MACONDO MC252-1.XLS
BP-HZN-2179MDL01982986	BP-HZN-2179MDL01982986	BP-1262-AB 11 7-8 71.8 HCQ125 513 BUCKON MACONDO MC252-1.XLS

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BP-HZN-2179MDL01982987	BP-HZN-2179MDL01982987	BP-1262-AB 11 7-8 71.8 HCQ125 513 BUCKON MACONDO MC252-1.XLS
BP-HZN-2179MDL01983279	BP-HZN-2179MDL01983280	Macondo kv3465.mail
BP-HZN-2179MDL01983281	BP-HZN-2179MDL01983281	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01983282	BP-HZN-2179MDL01983282	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL01984237	BP-HZN-2179MDL01984237	BP-1145-AB 18" 117 P110 511 TMT BUCKON MACONDO MC252-1.XLS
BP-HZN-2179MDL01984238	BP-HZN-2179MDL01984238	BP-1145-AB 18" 117 P110 511 TMT BUCKON MACONDO MC252-1.XLS
BP-HZN-2179MDL01986592	BP-HZN-2179MDL01986592	BP-1176-AB 16" ID CALIPER 20 JTS TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01986593	BP-HZN-2179MDL01986593	BP-1176-AB 16" ID CALIPER 20 JTS TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL01989288	BP-HZN-2179MDL01989288	BP-1263-AB 9 7-8 62.8 Q125 523 BUCKON MACONDO MC252-1.XLS
BP-HZN-2179MDL01989289	BP-HZN-2179MDL01989289	BP-1263-AB 9 7-8 62.8 Q125 523 BUCKON MACONDO MC252-1.XLS
BP-HZN-2179MDL01990494	BP-HZN-2179MDL01990494	BP-1277-AB 11 7-8 71.8 HCQ125 513 WR INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL01990495	BP-HZN-2179MDL01990495	BP-1277-AB 11 7-8 71.8 HCQ125 513 WR INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL01990809	BP-HZN-2179MDL01990809	Macondo kv654.mail
BP-HZN-2179MDL01990810	BP-HZN-2179MDL01990810	BP-1170-AB 16" RIG PREP TUBO N MACONDO MC252-1.XLS
BP-HZN-2179MDL01992560	BP-HZN-2179MDL01992560	Macondo - 16" Casing Back to Storage
BP-HZN-2179MDL01992561	BP-HZN-2179MDL01992561	BP-1182-AB 16" PUP JT RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01992562	BP-HZN-2179MDL01992562	BP-1182-AB 16" PUP JT RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01992563	BP-HZN-2179MDL01992563	BP-1171-AB 16" RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL01992564	BP-HZN-2179MDL01992564	BP-1171-AB 16" RIG PREP TUBO S. MACONDO MC252-1.XLS
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BP-HZN-2179MDL01993153	BP-HZN-2179MDL01993153	v - BP-1555 WB WO-10278 Weatherford Liner Hangers NI Macondo MC 252-1 Marianas (2).xls
BP-HZN-2179MDL02172066	BP-HZN-2179MDL02172087	D&C Recommended Practice.doc
BP-HZN-2179MDL02241291	BP-HZN-2179MDL02241731	TDM 2008.pdf
BP-HZN-2179MDL02437271	BP-HZN-2179MDL02437273	RE: BP Macondo crossover sub question
BP-HZN-2179MDL02437274	BP-HZN-2179MDL02437274	FW: BP-164 CD WO-09574 Allis Chalmers Broussard Macondo MC252-1 Transocean Marianas.xls
BP-HZN-2179MDL02437275	BP-HZN-2179MDL02437275	BP-164 CD WO-09574 Allis Chalmers Broussard Macondo MC252-1 Transocean Marianas.xls
BP-HZN-2179MDL02464363	BP-HZN-2179MDL02464364	FW: Macondo - 9-7/8" Re-threads - Post-thread Inspection adn Rig Prep
BP-HZN-2179MDL02464365	BP-HZN-2179MDL02464365	TUBULAR GOODS RELEASE
BP-HZN-2179MDL02464366	BP-HZN-2179MDL02464366	BP-1147-AB 9 7-8 62.8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02464367	BP-HZN-2179MDL02464367	BP-1124-AB 9 7-8 62.8 Q125 THRD INSP TUBO S MACONDO MC252-1.XLS
BP-HZN-2179MDL02516507	BP-HZN-2179MDL02516507	BP-1279- kv5434.mail
BP-HZN-2179MDL02516508	BP-HZN-2179MDL02516508	BP-1279-AB 7" 32 HCQ125 513 RIG PREP TUBO AMELIA MACONDO MC252-1.XLS
BP-HZN-2179MDL02516522	BP-HZN-2179MDL02516522	Macondo kv4660.mail
BP-HZN-2179MDL02516523	BP-HZN-2179MDL02516533	PO 4540072082 Rev 2 dated 10-13-2009 (2).pdf

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BP-HZN-2179MDL02518626	BP-HZN-2179MDL02518626	BP-1228- kv3459.mail
BP-HZN-2179MDL02518627	BP-HZN-2179MDL02518627	BP-1228-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02518954	BP-HZN-2179MDL02518954	Macondo - 16" ID Caliper
BP-HZN-2179MDL02518955	BP-HZN-2179MDL02518955	BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL02534091	BP-HZN-2179MDL02534091	Macondo - Float Equipment Order - PO 4540072082 Rev 1 dated 09-24-2009 - Need Approval
BP-HZN-2179MDL02534092	BP-HZN-2179MDL02534100	PO 4540072082 Rev 1 dated 09-24-2009.pdf
BP-HZN-2179MDL02542708	BP-HZN-2179MDL02542709	FW: BP Macondo crossover sub question
BP-HZN-2179MDL02542710	BP-HZN-2179MDL02542710	FW: BP-164 CD WO-09574 Allis Chalmers Broussard Macondo MC252-1 Transocean Marianas.xls
BP-HZN-2179MDL02542711	BP-HZN-2179MDL02542711	BP-164 CD WO-09574 Allis Chalmers Broussard Macondo MC252-1 Transocean Marianas.xls
BP-HZN-2179MDL02545993	BP-HZN-2179MDL02545993	Macondo - 13-5/8" Pup Joint to Hydril for Split & Re-thread
BP-HZN-2179MDL02545994	BP-HZN-2179MDL02545994	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02550241	BP-HZN-2179MDL02550241	RE: BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL02550242	BP-HZN-2179MDL02550242	BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL02550278	BP-HZN-2179MDL02550279	FW: Macondo - 13-5/8" Pup Joint to Hydril for Split & Re-thread
BP-HZN-2179MDL02550280	BP-HZN-2179MDL02550280	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02562224	BP-HZN-2179MDL02562224	BP-1171-AB 16" RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL02562225	BP-HZN-2179MDL02562225	BP-1171-AB 16" RIG PREP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL02566919	BP-HZN-2179MDL02566919	Macondo - 9-7/8" Float Equipment Order - PO 4540072082 Rev 1 dated 09-24-2009
BP-HZN-2179MDL02566920	BP-HZN-2179MDL02566928	PO 4540072082 Rev 1 dated 09-24-2009 - Approved.pdf
BP-HZN-2179MDL02575587	BP-HZN-2179MDL02575588	FW: BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL02575589	BP-HZN-2179MDL02575589	BP-1170-AB 16" RIG PREP TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL02604020	BP-HZN-2179MDL02604021	BP-1176-AB 16" ID CALIPER 20 JTS TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL02604022	BP-HZN-2179MDL02604022	BP-1176-AB 16" ID CALIPER 20 JTS TUBO N. MACONDO MC252-1.XLS
BP-HZN-2179MDL02604797	BP-HZN-2179MDL02604798	Macondo - 13-5/8" Casing - Un-rig Prep
BP-HZN-2179MDL02604799	BP-HZN-2179MDL02604799	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02604800	BP-HZN-2179MDL02604800	BP-1162-AB 13 5-8 88.2 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02605896	BP-HZN-2179MDL02605896	Macondo - Float Equipment Order - PO 4540072082 Rev 1 dated 09-24-2009 - Need Approval
BP-HZN-2179MDL02605897	BP-HZN-2179MDL02605905	PO 4540072082 Rev 1 dated 09-24-2009.pdf
BP-HZN-2179MDL02607352	BP-HZN-2179MDL02607352	BP-1260- kv354.mail
BP-HZN-2179MDL02607353	BP-HZN-2179MDL02607353	BP-1260-AB 13 5-8 88.2 HCQ125 X-OVER INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL02616703	BP-HZN-2179MDL02616703	BP-1262-AB 11 7-8 71.8 HCQ125 513 BUCKON MACONDO MC252-1.XLS
BP-HZN-2179MDL02616704	BP-HZN-2179MDL02616704	BP-1262-AB 11 7-8 71.8 HCQ125 513 BUCKON MACONDO MC252-1.XLS
BP-HZN-2179MDL02631105	BP-HZN-2179MDL02631106	Macondo - 9-7/8" Re-threads - Post-thread Inspection adh Rig Prep
BP-HZN-2179MDL02631107	BP-HZN-2179MDL02631107	TUBULAR GOODS RELEASE
BP-HZN-2179MDL02631108	BP-HZN-2179MDL02631108	BP-1147-AB 9 7-8 62.8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02631109	BP-HZN-2179MDL02631109	BP-1124-AB 9 7-8 62.8 Q125 THRD INSP TUBO S. MACONDO MC252-1.XLS

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BP-HZN-2179MDL02635553	BP-HZN-2179MDL02635553	BP-1280-AB 7" 32 HCQ125 513 TMT BUCK-ON MACONDO MC252-1.XLS
BP-HZN-2179MDL02635554	BP-HZN-2179MDL02635554	BP-1280-AB 7" 32 HCQ125 513 TMT BUCK-ON MACONDO MC252-1.XLS
BP-HZN-2179MDL02635857	BP-HZN-2179MDL02635857	BP-1231-AB 13 5-8 88.2 HCQ125 523 BUCKON MACONDO MC252-1.XLS
BP-HZN-2179MDL02635858	BP-HZN-2179MDL02635858	BP-1231-AB 13 5-8 88.2 HCQ125 523 BUCKON MACONDO MC252-1.XLS
BP-HZN-2179MDL02659011	BP-HZN-2179MDL02659011	BP-1237-AB 9 7-8 62.8 Q125 PE X VTOP PJ INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL02659012	BP-HZN-2179MDL02659012	BP-1237-AB 9 7-8 62.8 Q125 PE X VTOP PJ INSP MACONDO MC252-1.XLS
BP-HZN-2179MDL02693970	BP-HZN-2179MDL02693970	BP-1147-AB 9 7-8 62.8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02693971	BP-HZN-2179MDL02693971	BP-1147-AB 9 7-8 62.8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02696255	BP-HZN-2179MDL02696255	BP-1124- kv3640.mail
BP-HZN-2179MDL02696256	BP-HZN-2179MDL02696256	BP-1124-AB 9 7-8 62.8 Q125 THRD INSP TUBO S. MACONDO MC252-1.XLS
BP-HZN-2179MDL02698104	BP-HZN-2179MDL02698105	RE Macon kv3832.mail
BP-HZN-2179MDL02698106	BP-HZN-2179MDL02698106	BP-1147-AB 9 7-8 62.8 HCQ125 523 RIG PREP MACONDO MC252-1.XLS
BP-HZN-2179MDL02703257	BP-HZN-2179MDL02703257	Macondo kv312.mail
BP-HZN-2179MDL02703258	BP-HZN-2179MDL02703268	PO 4540072082 Rev 2 dated 10-13-2009.pdf
BP-HZN-2179MDL02727487	BP-HZN-2179MDL02727487	JS100310-WR-086-SM.xls
BP-HZN-2179MDL02727488	BP-HZN-2179MDL02727488	BP Integrity Assurance Insp. Workbook v4.8
BP-HZN-2179MDL02750110	BP-HZN-2179MDL02750110	BP-1196-AB 9 7-8 CLEAN AND REDOPE MACONDO MC252-1.XLS
BP-HZN-2179MDL02750111	BP-HZN-2179MDL02750111	BP-1196-AB 9 7-8 CLEAN AND REDOPE MACONDO MC252-1.XLS
BP-HZN-2179MDL02759843	BP-HZN-2179MDL02759848	BP-3259 JS WO-10333 BA Rentals Gulf Coast Machine Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02761059	BP-HZN-2179MDL02761066	BP-3275 JS WO-10388 Smith HE Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02768265	BP-HZN-2179MDL02768273	BP-205 CD WO-10223 Blackhawk Specialty Tools Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL02773555	BP-HZN-2179MDL02773560	BP-3272 JS WO-10379 Halliburton Sperry Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL02784126	BP-HZN-2179MDL02784135	BP-3269 JS WO-10374 Baker Hughes Inteq Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02786680	BP-HZN-2179MDL02786685	BP-3257 JS WO-10331 Halliburton Sperry Drilling Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02797017	BP-HZN-2179MDL02797048	Weatherford DT 5436925-5 for 13.625 inch.pdf
BP-HZN-2179MDL02800859	BP-HZN-2179MDL02800896	Blackhawk - Inspection Papers - 16 inch.pdf
BP-HZN-2179MDL02801163	BP-HZN-2179MDL02801168	BHA Inspection Release Workbook
BP-HZN-2179MDL02801438	BP-HZN-2179MDL02801441	BP-3227 JS WO-10236 NOV Downhole Gammaloy Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02802211	BP-HZN-2179MDL02802215	BP-203 CD WO-10217 Alilis Chalmers Amelia Macondo MC 252-1 Horizon.pdf
BP-HZN-2179MDL02805524	BP-HZN-2179MDL02805533	BP-221 CD WO-10393 8 0 MWD Halliburton-Sperry Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL02810657	BP-HZN-2179MDL02810668	Smith HE DT - ST643278.pdf
BP-HZN-2179MDL02815092	BP-HZN-2179MDL02815095	BP-028 JKL WO-10230 Mashburn Machine Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL02815404	BP-HZN-2179MDL02815444	Halliburton DT-310101305 - 13.625 fast drills.pdf
BP-HZN-2179MDL02818854	BP-HZN-2179MDL02818861	Smith He -DT-ST644195 - w-certs.pdf
BP-HZN-2179MDL02830019	BP-HZN-2179MDL02830024	BP-3260 JS WO-10337 Halliburton Sperry Drilling Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02833446	BP-HZN-2179MDL02833453	BP-069 AH WO-10231 Alilis Chalmers Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02839274	BP-HZN-2179MDL02839280	BP-222 CD WO-10397 9600 Geo Pilots DD Halliburton-Sperry Macondo MC252-1 Horizon.pdf

BEGBATES	ENDBATES	FILENAME/DESCRIPTION
BP-HZN-2179MDL02839940	BP-HZN-2179MDL02839945	BP-3222 JS WO-10224 Smith HE Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL02842113	BP-HZN-2179MDL02842122	BP-215 CD WO-10350 8 0 MWD Equip Halliburton-Sperry Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL02842123	BP-HZN-2179MDL02842130	BP-3228 JS WO-10238 NOV Downhole Gammalay Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02842894	BP-HZN-2179MDL02842901	BP-3278 JS WO-10396 BA Rental Tools Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02842907	BP-HZN-2179MDL02842913	BP-223 CD WO-10399 Crossover Sub Allis Chalmers Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL02845203	BP-HZN-2179MDL02845208	BP-3265 JS WO-10348 Allis Chalmers Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL02846343	BP-HZN-2179MDL02846350	BP-3279 JS WO-10400 Halliburton Service Tools Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02853986	BP-HZN-2179MDL02853990	BP-068-AH WO-10219 9 625 Mud Motor Halliburton Sperry Sun Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02865046	BP-HZN-2179MDL02865052	BP-3226 JS WO-10235 Halliburton Sperry Drilling Macondo MC 252-1 Horizon.pdf
BP-HZN-2179MDL02865849	BP-HZN-2179MDL02865853	BP-901 BIT WO 10392 Mashburn Machine Macondo MC252 1 Horizon.pdf
BP-HZN-2179MDL02866289	BP-HZN-2179MDL02866294	BP-081-AH WO-10389 Mud Tool Subs Offshore Energy Services Macondo MC252-1 Horizon.pdf
BP-HZN-2179MDL02866409	BP-HZN-2179MDL02866416	BP-3119 JS WO-10207 Baker Hughes Inteq Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02874879	BP-HZN-2179MDL02874887	BP-3282 JS WO-10408 Halliburton Sperry Sun Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02876818	BP-HZN-2179MDL02876827	BP 225 CD WO-10405 6 625 HWDP Allis Chalmers Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02881882	BP-HZN-2179MDL02881886	BP-3224 JS WO-10227 Sperry Drilling Geo Pilot Macondo MC 252 1 Horizon.pdf
BP-HZN-2179MDL02989874	BP-HZN-2179MDL02989886	RPD-Horizon approval.pdf
BP-HZN-2179MDL03022665	BP-HZN-2179MDL03022666	RA-9594 BIT WO-09594 Repair Authorization Form Workstrings Macondo MC 252 1 Marianas.pdf
BP-HZN-2179MDL03023062	BP-HZN-2179MDL03023066	BP-3076 JS WO-09579 962 Powerpak 7-8 GT Anadrill Macondo MC 252 1 Marianas.pdf
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